

**From inflow to interflow, through plunging and lofting:
*uncovering the dominant flow processes of a sediment-rich negatively
buoyant river inflow into a stratified lake***

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Motivation

River inflows...

...are an important input of sediment, oxygen, contaminants, nutrients, heat, and momentum for lakes and reservoirs

→ influence on water quality, reservoir storage capacity & hazards

→ hydrodynamic processes at the river-lake/reservoir interface control the fate of these components

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51

Eutrophication processes regulated by a plunging river inflow

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157

Loss of reservoir volume by sediment deposition and its impact on water availability in semiarid Brazil

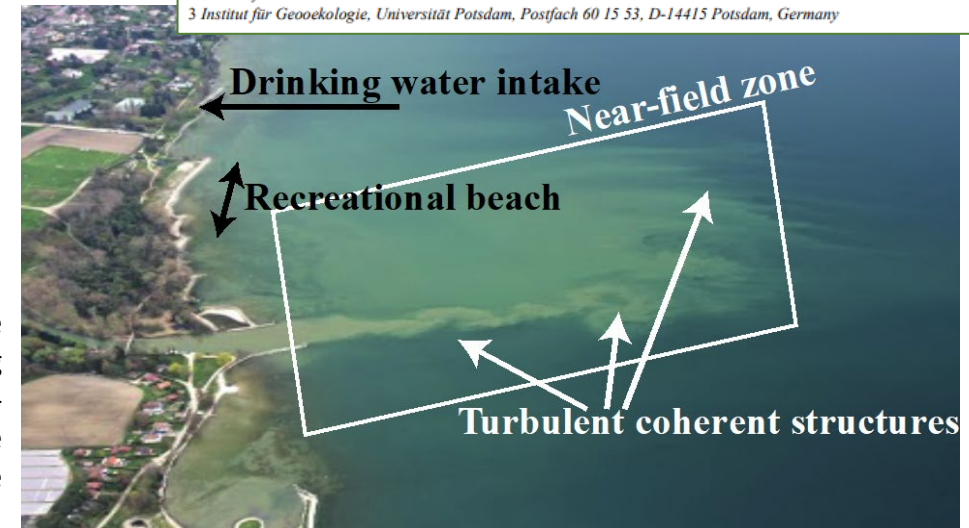
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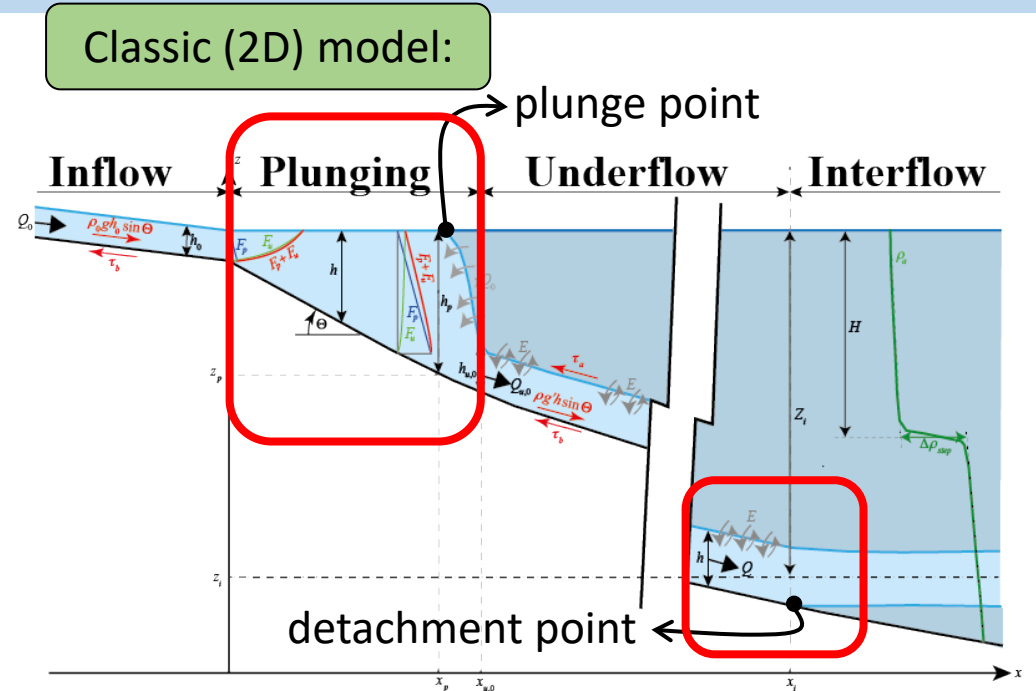
Inflow of the River Venoge into Lake Geneva (Switzerland). An intake of drinking water for the highly urbanized Lausanne-Geneva region is situated at 1 km from the inflow, and recreational beach areas are situated at both sides of the inflow. →

Motivation

River inflows...

...will plunge and form a gravity-driven density current near the bed (underflow, UF) and/or intermediate current (interflow, IF) when they are negatively buoyant w.r.t. lake surface water

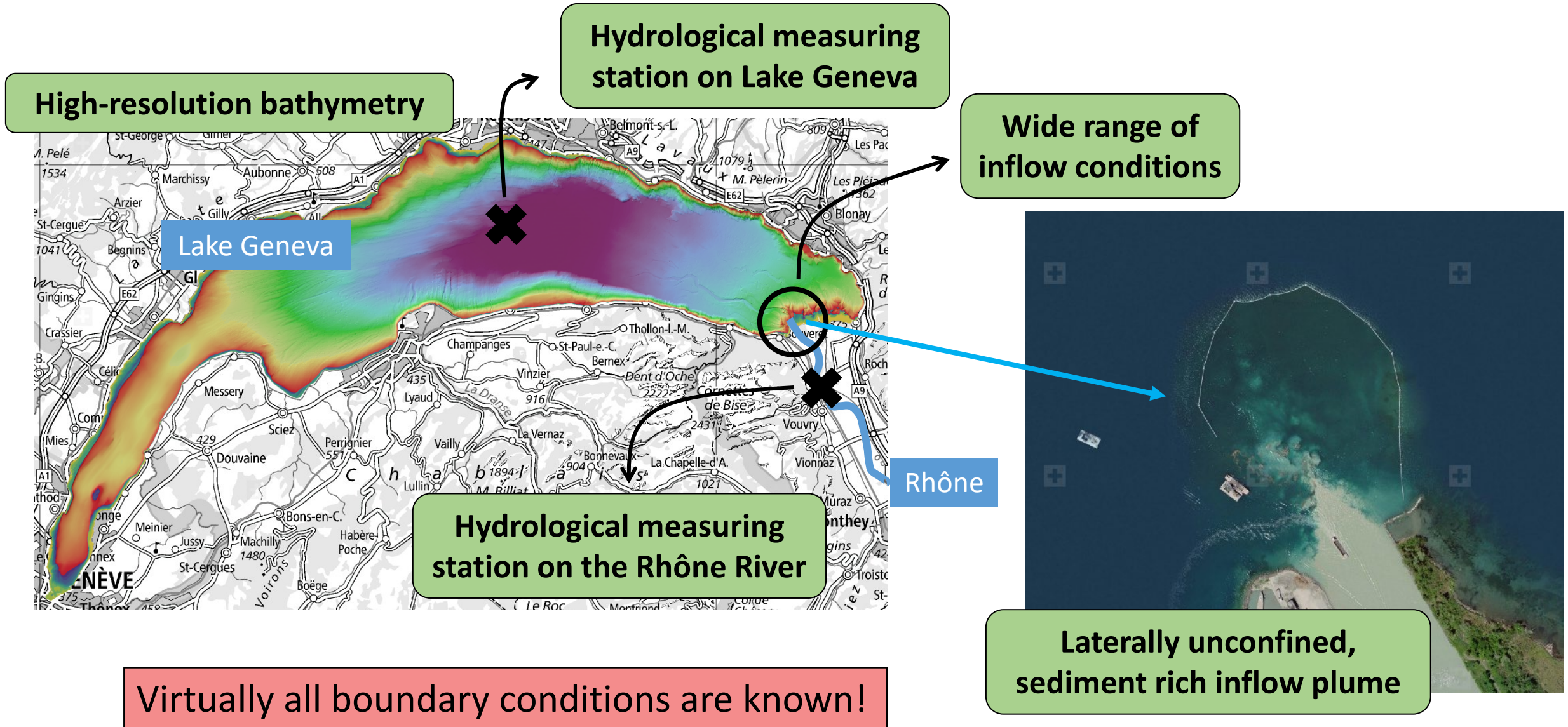
- plunging process provides upstream boundary conditions for density currents
- UF-IF transition has crucial influence on final destination of sediment, nutrients and contaminants
- important to identify and quantify the mixing processes involving entrainment of ambient water into the plunging flow as a function of the inflow properties (characterized by Fr_d)



! hydrodynamics of plunging process still poorly understood, especially in laterally unconfined configurations

! hydrodynamics of UF-IF transition still poorly understood, especially in turbid flows (density excess due to sediment)

Study site: Rhône inflow into Lake Geneva



High-resolution bathymetry

Hydrological measuring station on Lake Geneva

Wide range of inflow conditions

Lake Geneva

Hydrological measuring station on the Rhône River

Rhône

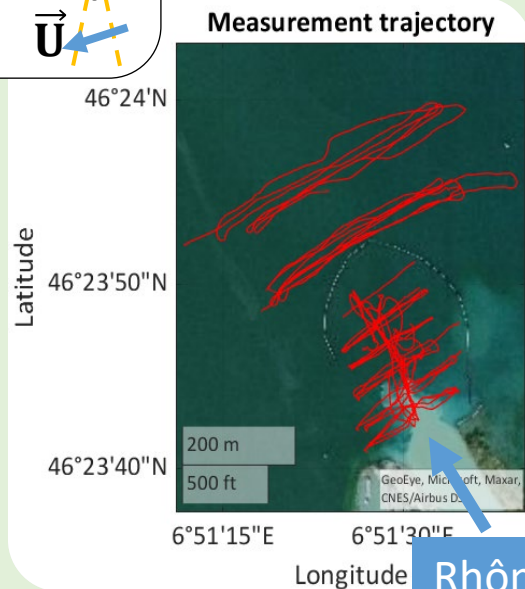
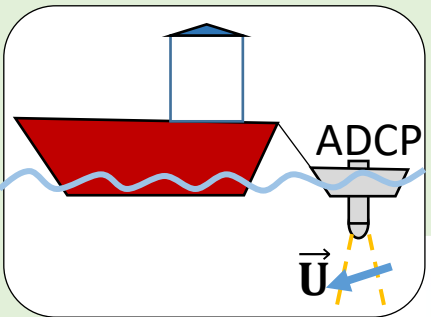
Virtually all boundary conditions are known!

Laterally unconfined, sediment rich inflow plume

Methods

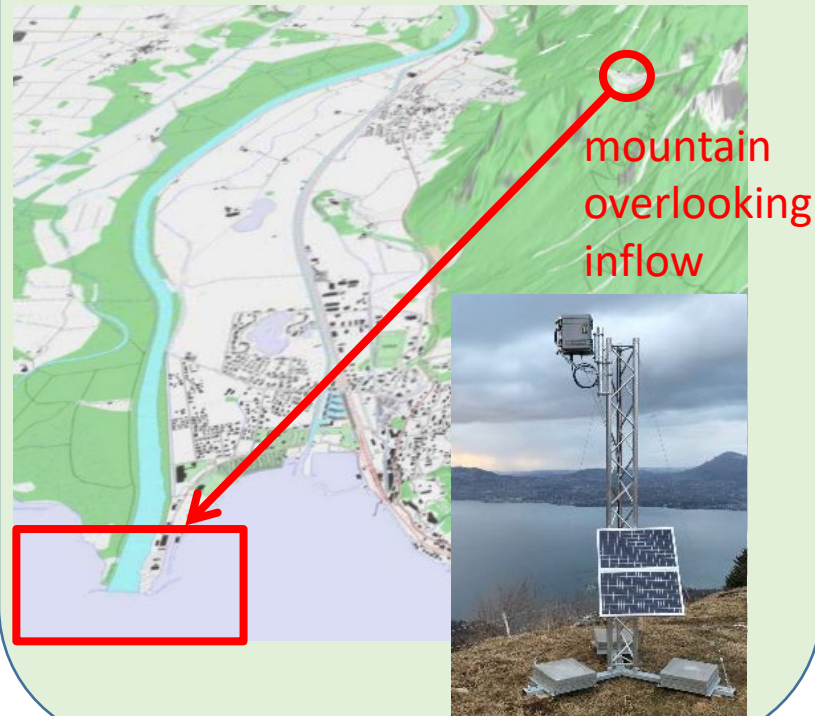
vessel-mounted ADCP

- three-dimensional velocity field along transversal and longitudinal transects
- multiple repetitions to catch low magnitude, secondary currents
- event-wise



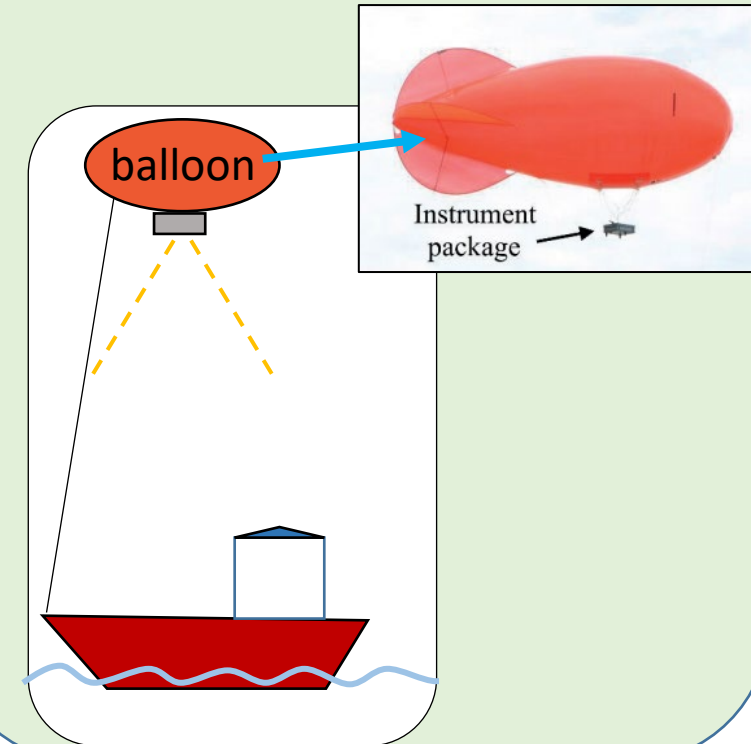
static remote-sensing camera system

- two-dimensional surface patterns
- large to intermediate scale processes
- 1-10 minute resolution
- continuous: ongoing since June 2019

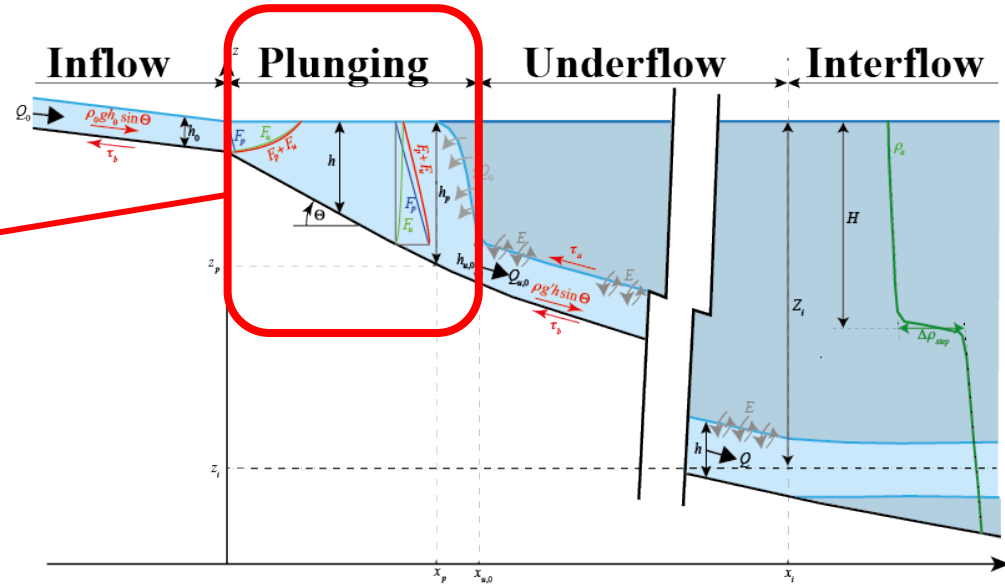
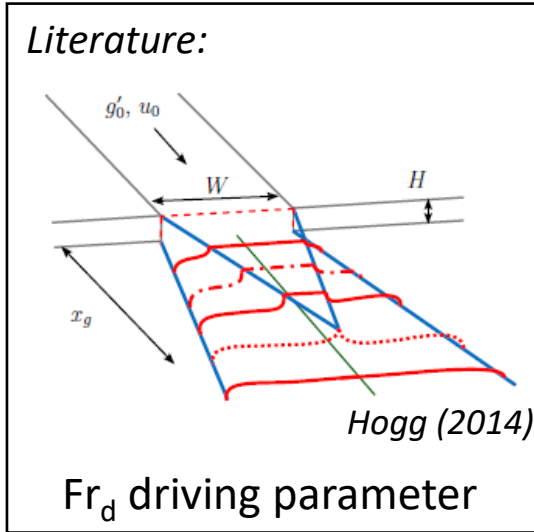


mobile balloon-mounted camera system

- two-dimensional surface patterns
- intermediate to small scale processes
- 1 second resolution
- event-wise

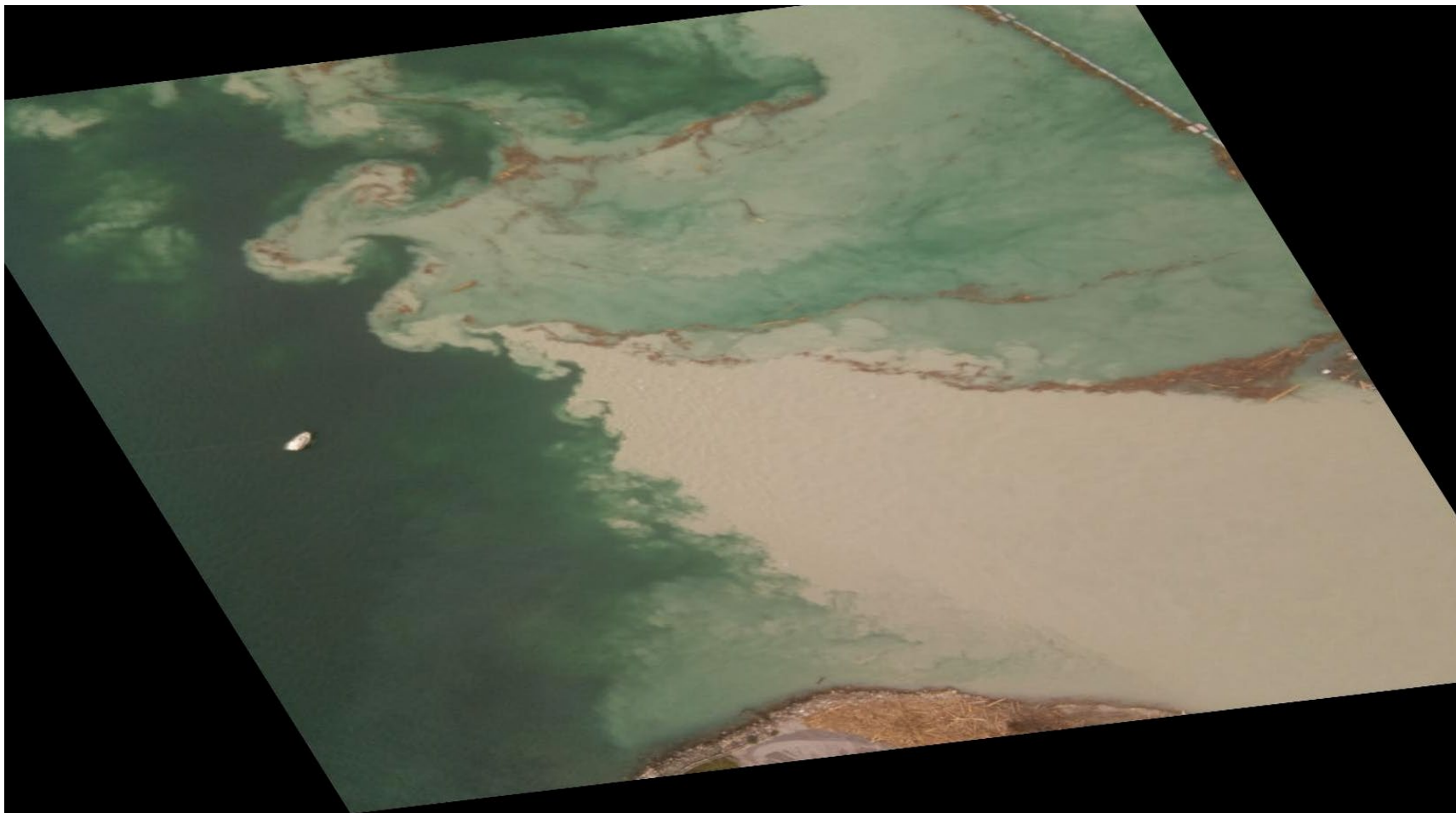


Results: overview



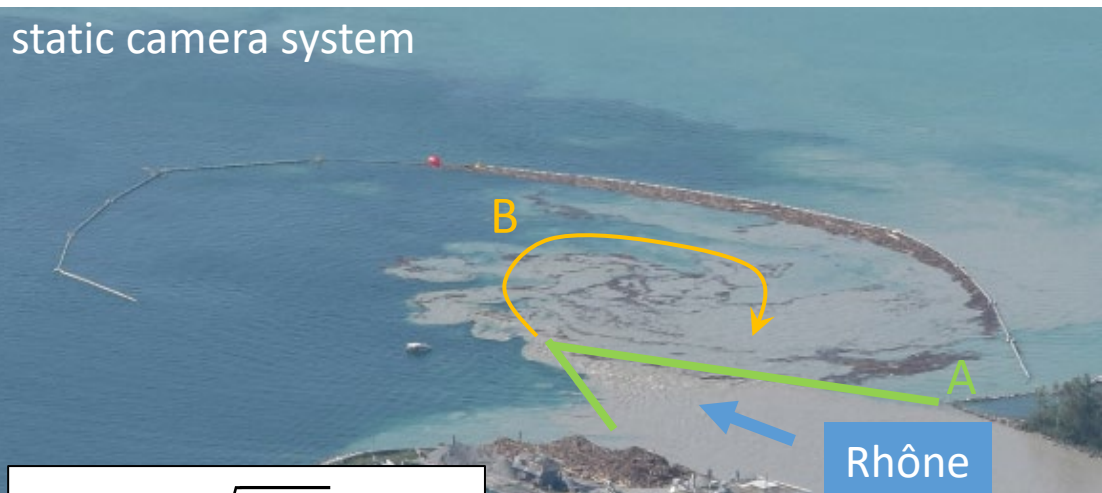
Results: plunging

Video for 1 BLIMP run → here $Fr_d = U_0 / \sqrt{g'h_0} = 3.75$ at inflow



Results: plunging

static camera system



$$Fr_d = U_0 / \sqrt{g'h_0} = 3.75$$

Rhône

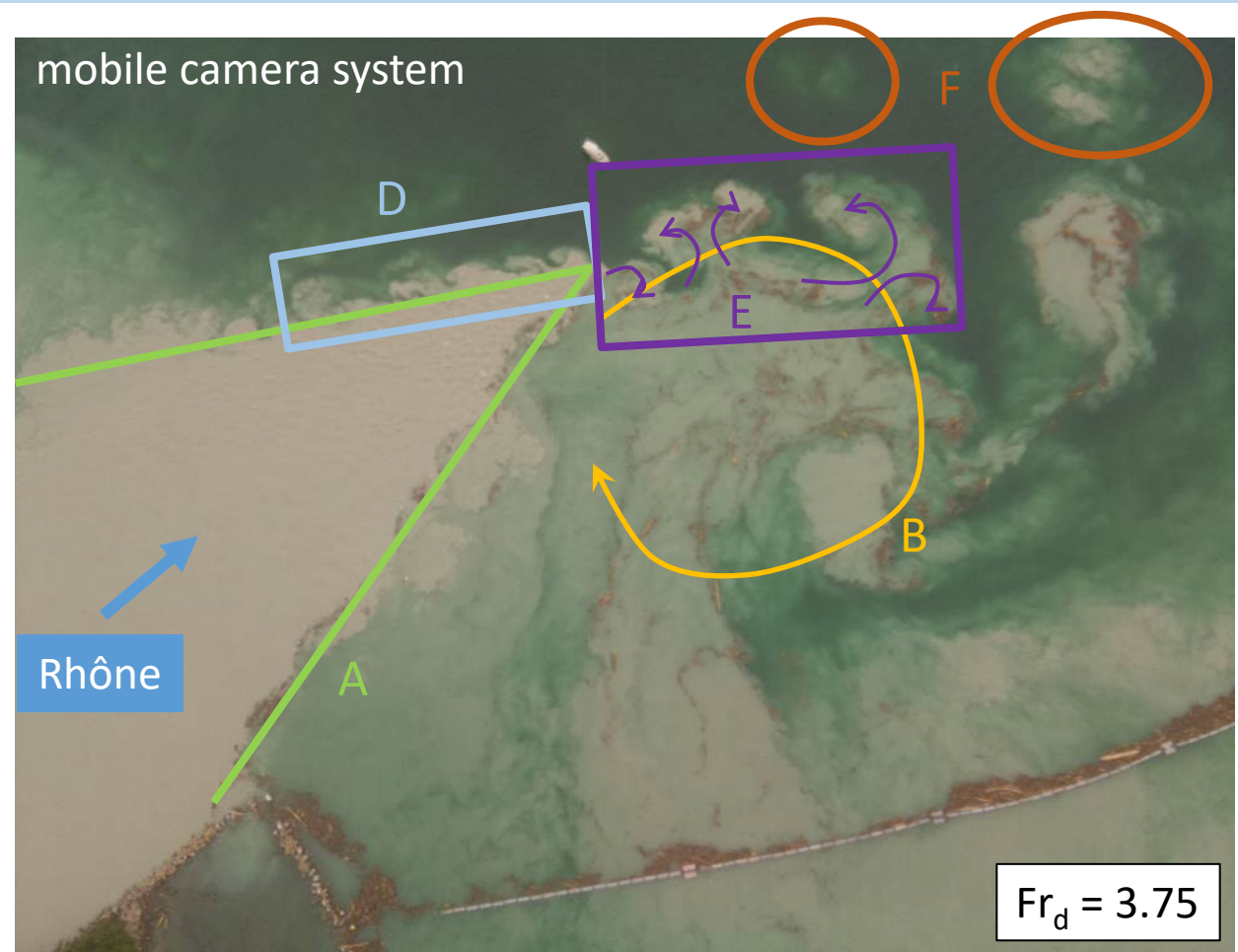
static camera system



$$Fr_d = 3.1$$

Rhône

mobile camera system

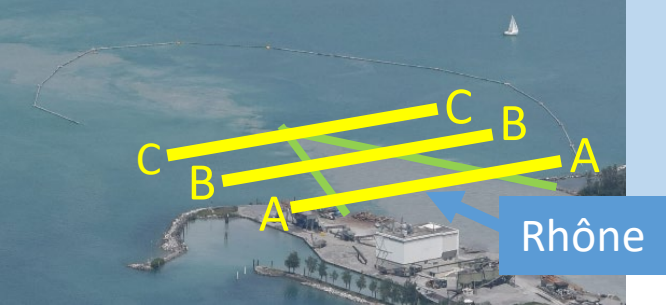


$$Fr_d = 3.75$$

Process description:

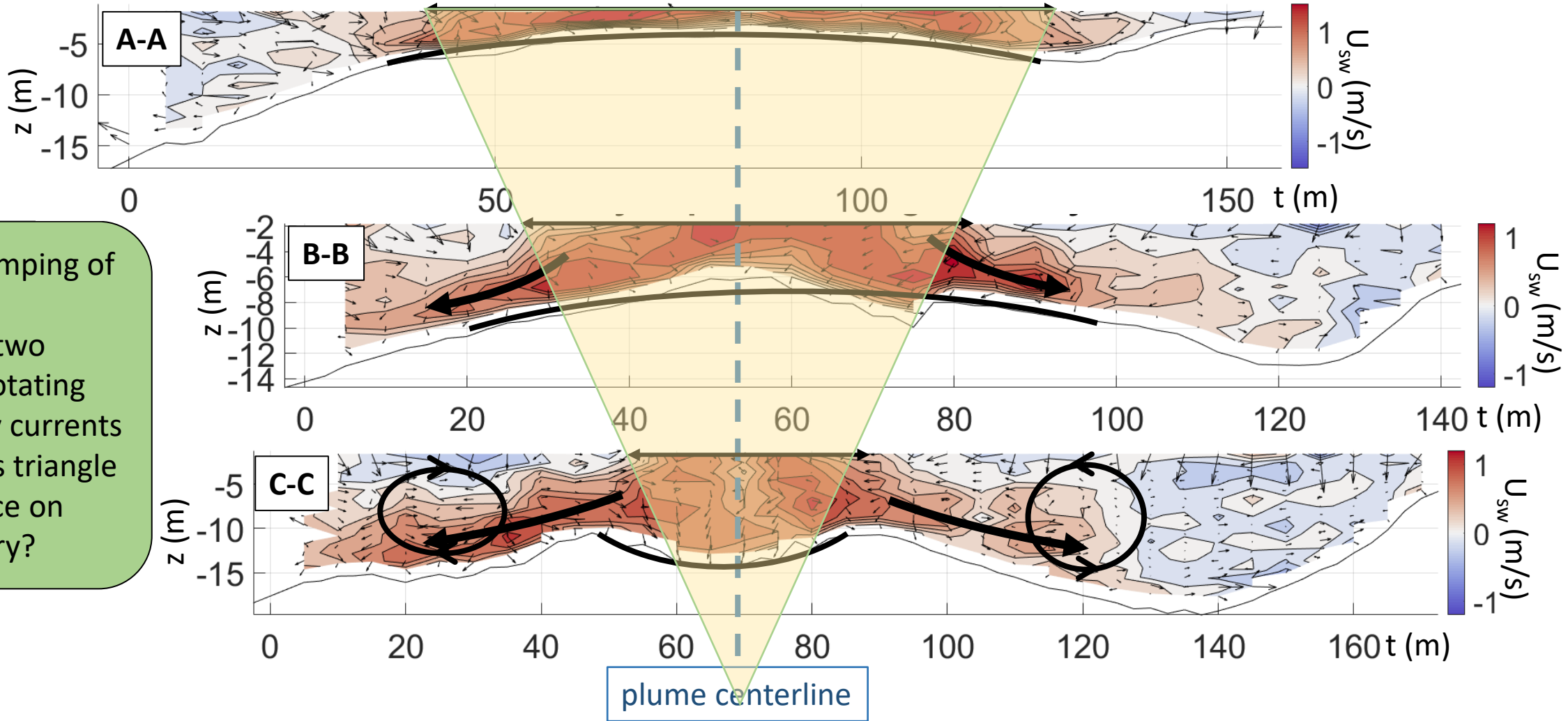
→ Question: what causes the plume to have a persistent triangular shape over all measured inflow conditions?

Results: plunging



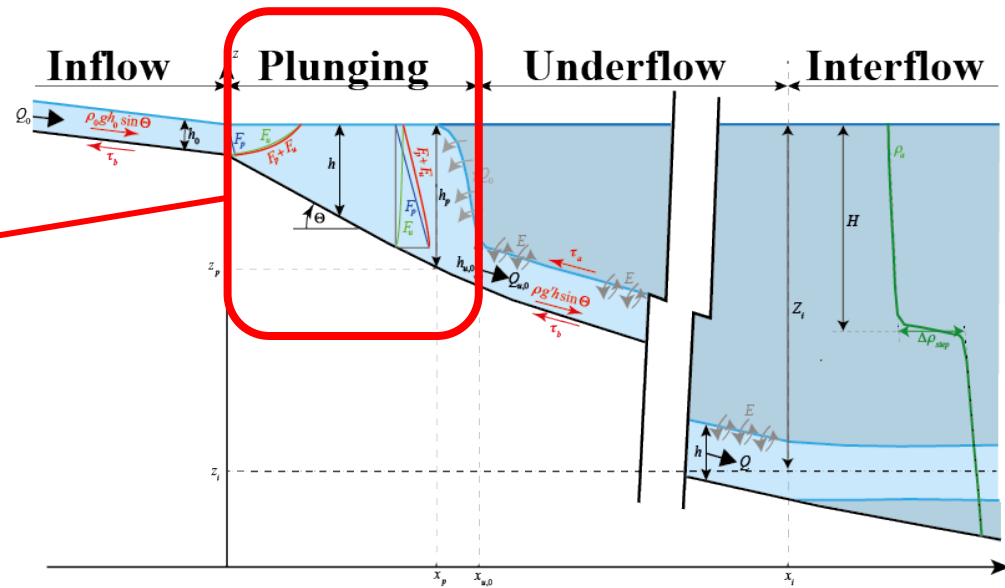
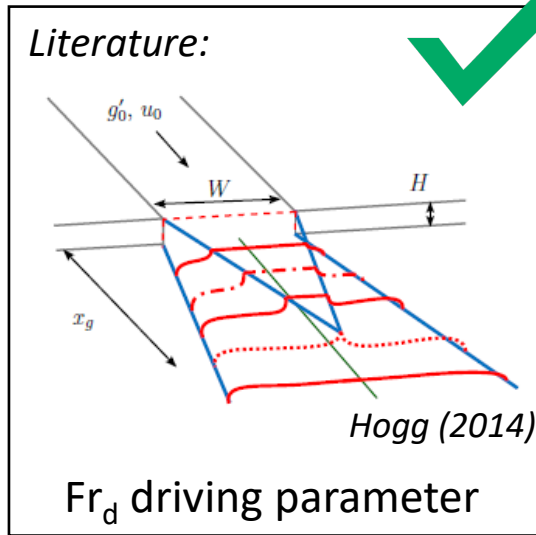
Results for 1 ADCP campaign → here $Fr_d = U_0 / \sqrt{g'h_0} = 4$ at inflow

Velocities in "streamwise" (colors) and transverse (vectors) direction



lateral slumping of plume
 → causes two counter-rotating secondary currents
 → explains triangle
 → influence on bathymetry?

Results: overview



Plunging additions:

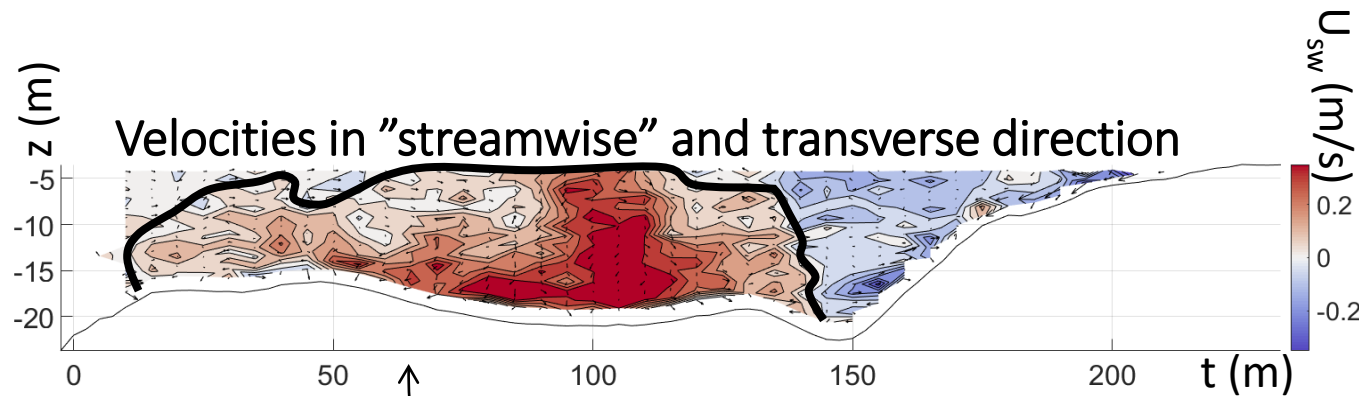
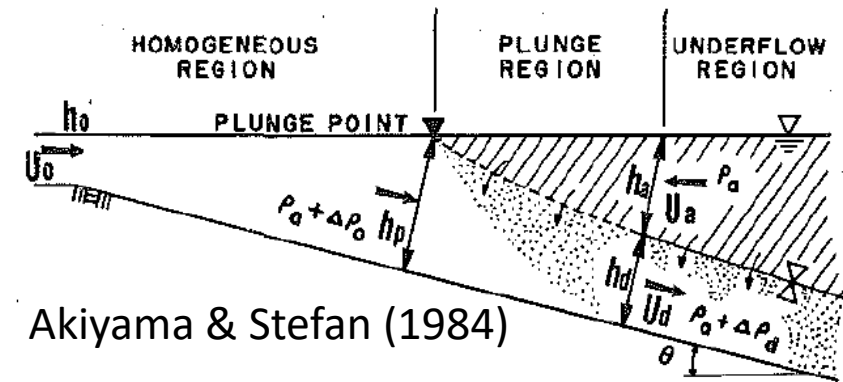
Qualitative:

1. First detailed direct measurements of main flow processes
2. More mixing processes described

Results: plunging

Quantifying mixing through the entrainment coefficient E :

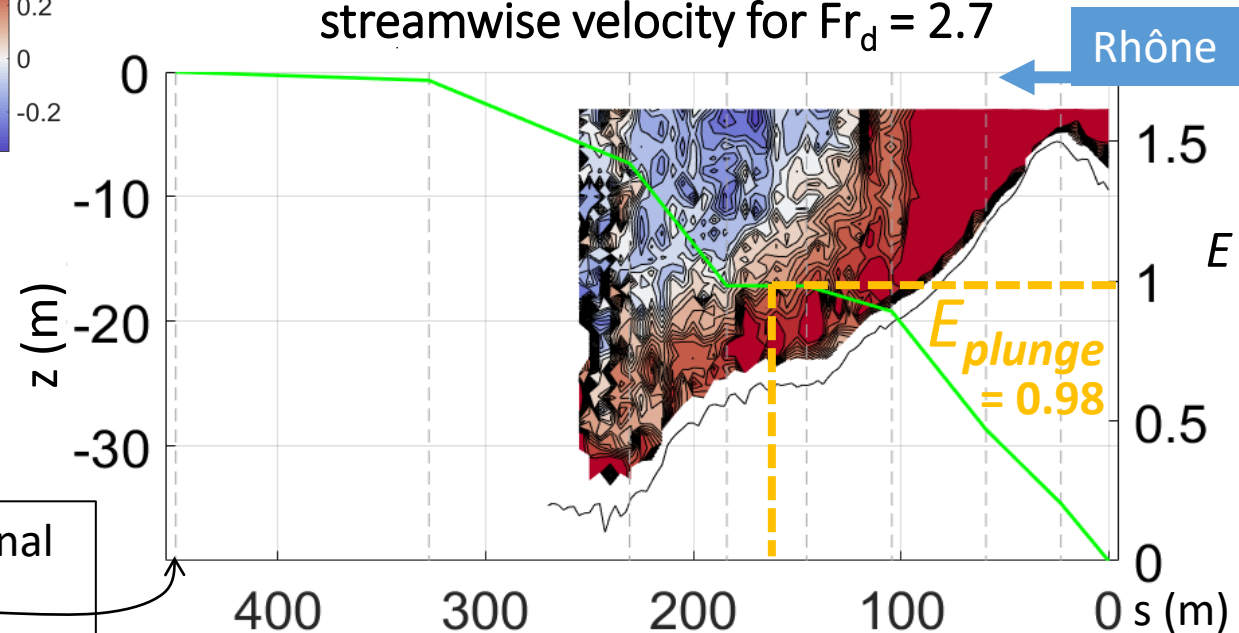
- Akiyama & Stefan (1984) for 2D case: $u_d = \frac{(1+E)q_0}{h_d}$
- In 3D: $E = \frac{Q_d}{Q_0} - 1 \rightarrow$ integrate streamwise velocities over high velocity core to find Q_d in every transversal transect, Q_0 is (known) discharge at inflow



Manually define underflow extent and integrate velocities

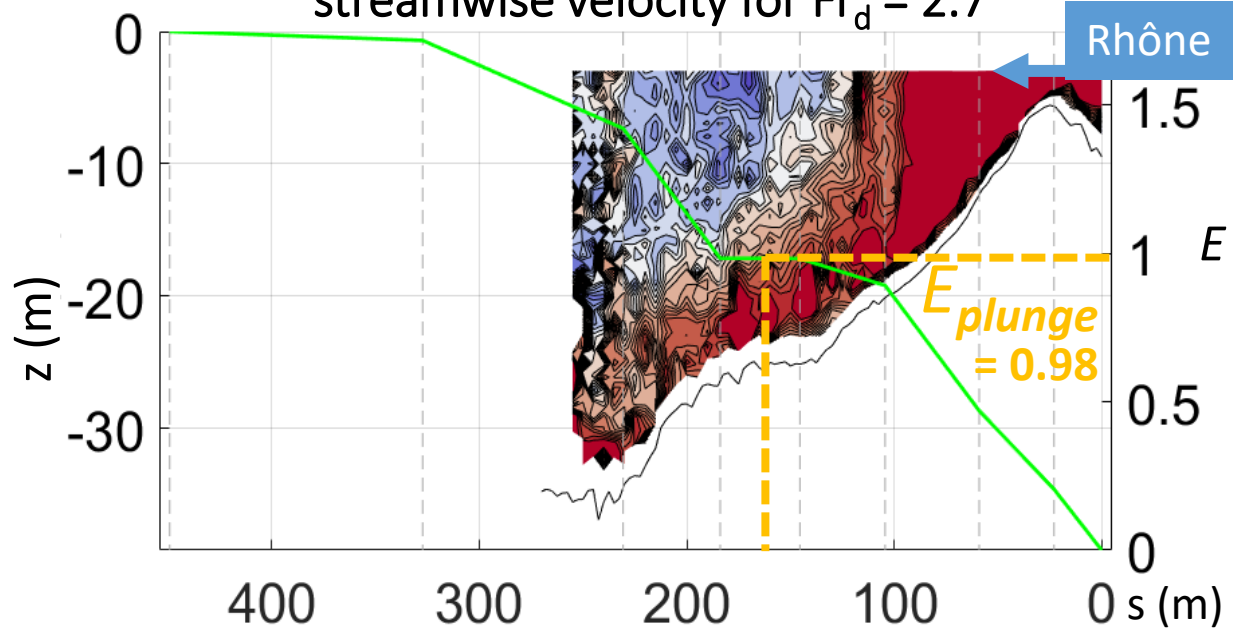
Gray, dotted lines indicate longitudinal positions of transversal transects

Entrainment coefficient superposed on streamwise velocity for $Fr_d = 2.7$

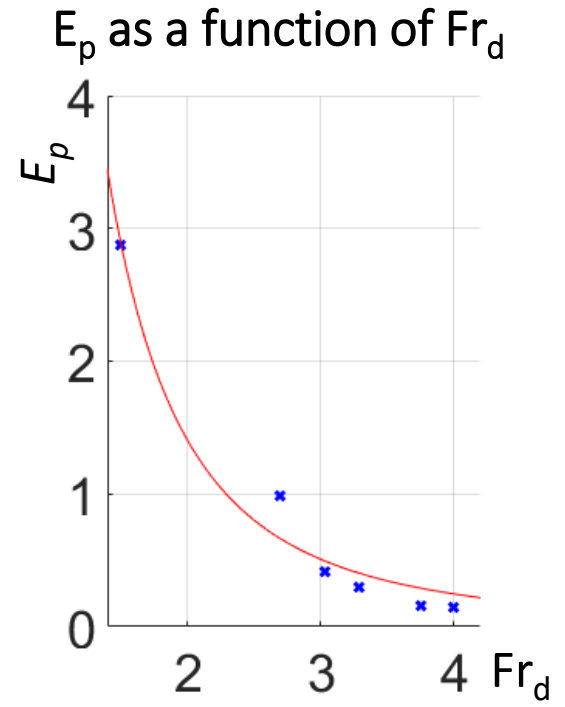


Results: plunging

Entrainment coefficient superposed on streamwise velocity for $Fr_d = 2.7$

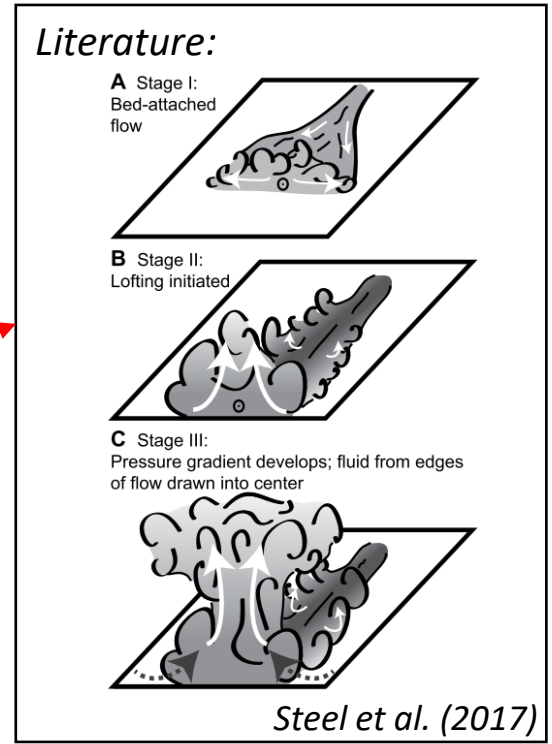
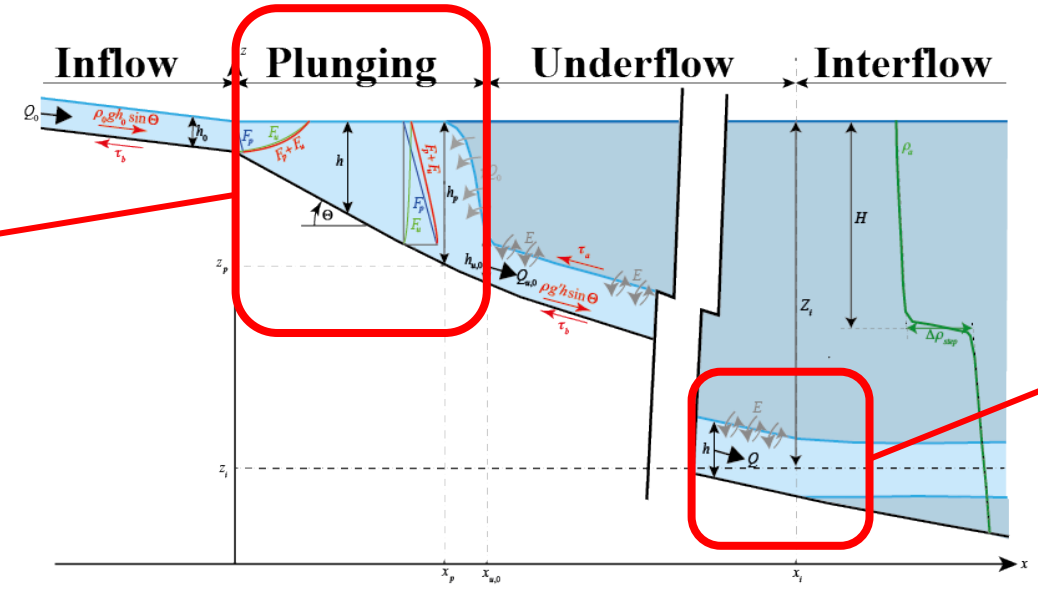
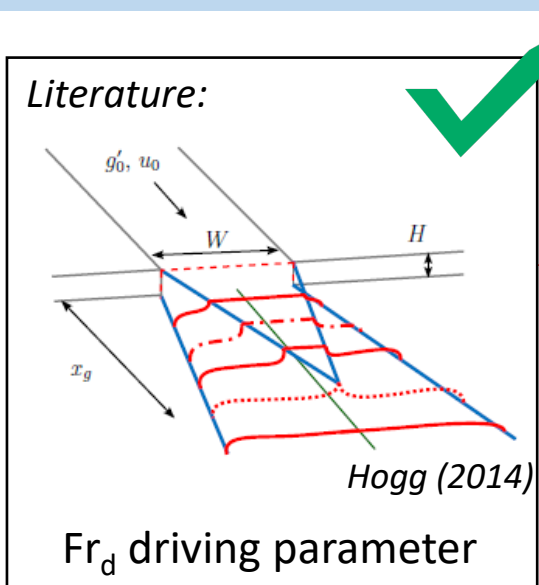


Do this for multiple inflow conditions



$Fr_d \uparrow \Rightarrow E_p \downarrow$

Results: overview



Plunging additions:

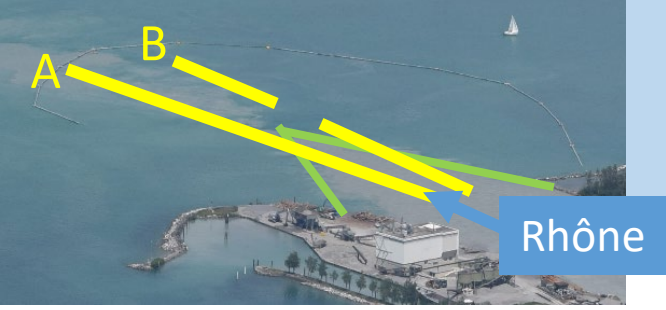
Qualitative:

1. First detailed direct measurements of main flow processes
2. More mixing processes described

Quantative:

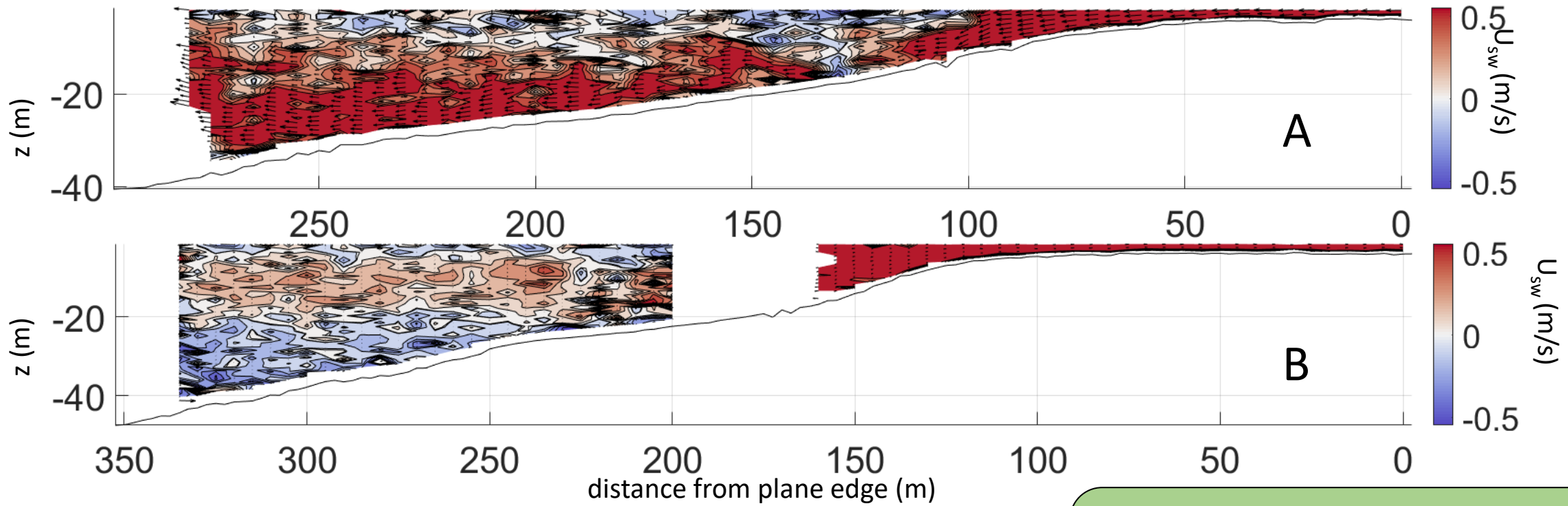
1. First direct quantification of mixing processes
2. Relation driving parameter-mixing processes

Results: UF-IF transition



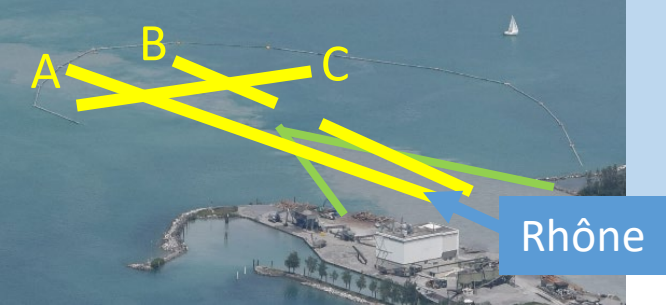
Results for 1 ADCP campaign → here $Fr_d = U_0 / \sqrt{g'h_0} = 3.3$ at inflow

Velocities in "streamwise" direction



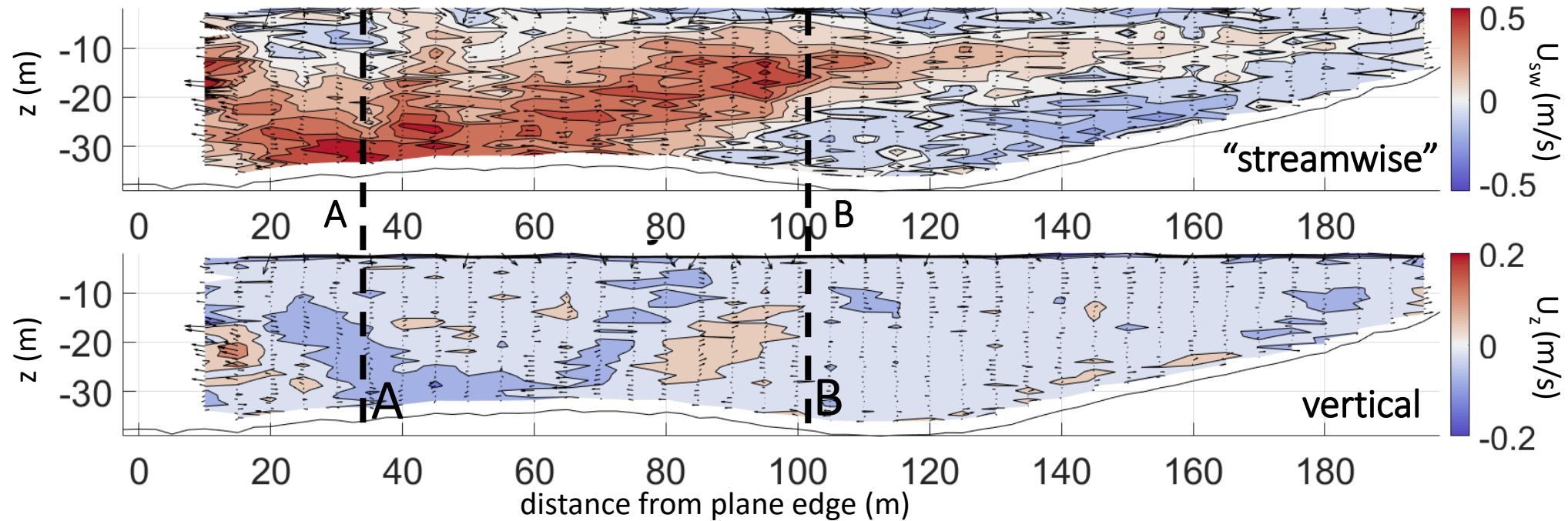
2 "streamwise" transects A and B
→ A: plunge at $d = 100$ m and continuous UF
→ B: plunge after $d = 160$ m and IF right after
→ inconsistent results? **NO**

Results: UF-IF transition



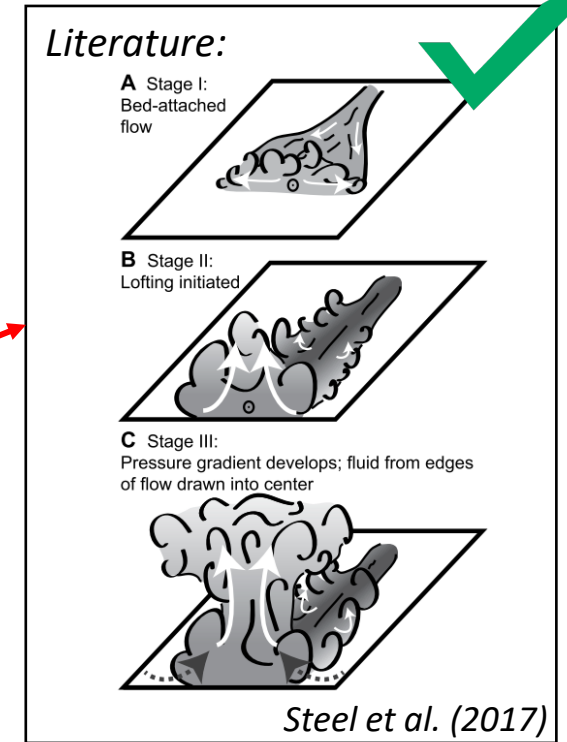
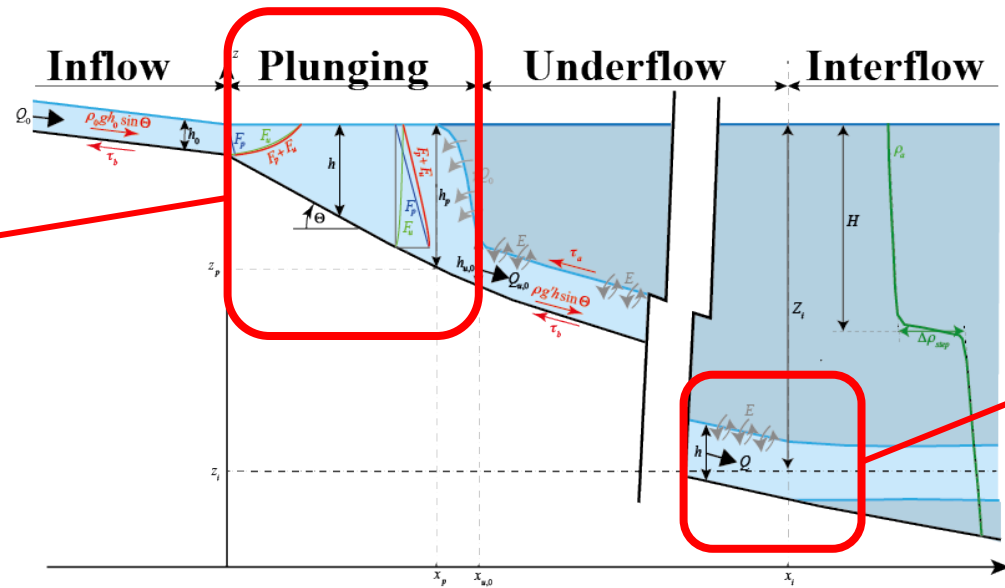
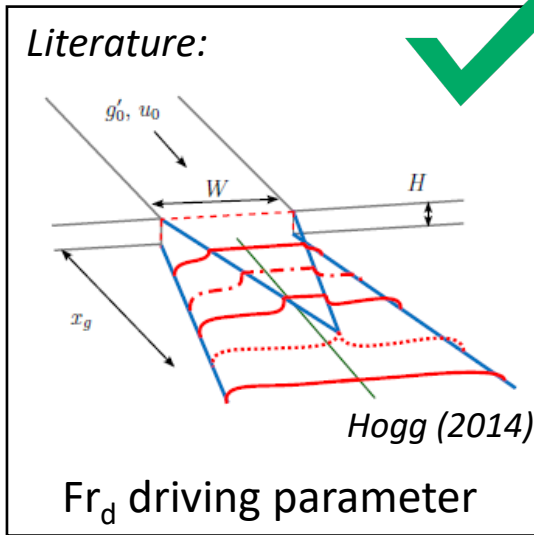
Results for 1 ADCP campaign → here $Fr_d = U_0 / \sqrt{g'h_0} = 3.3$ at inflow

C. Velocities in ... direction



- transversal plane C shows 2 flow regions: core continues as UF, while sides form IF
- planes A and B cut through C in different flow regions
- certain parts of plume become positively buoyant and rise up, process known as lofting
- higher rate of particle sedimentation on lower velocity plume edges, resulting in increased lowering of density?
- followed by lofting of UF core in later stage of UF (not shown here)

Results: overview



Plunging additions:

Qualitative:

1. First detailed direct measurements of main flow processes
2. More mixing processes described

Quantative:

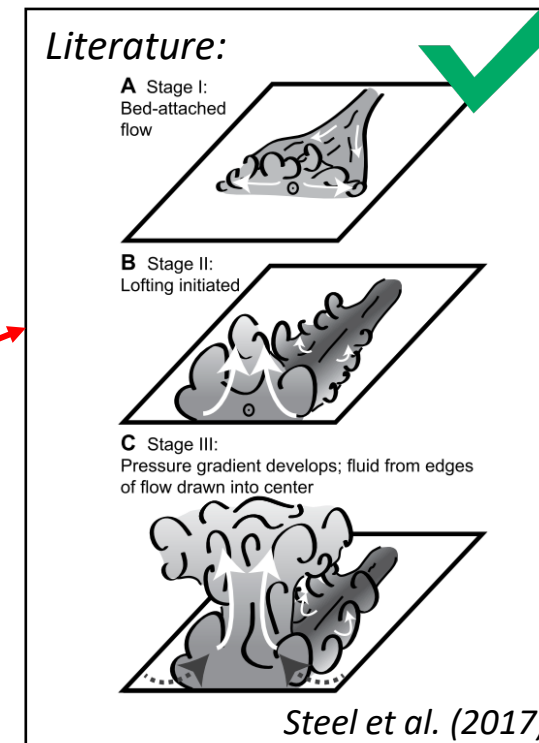
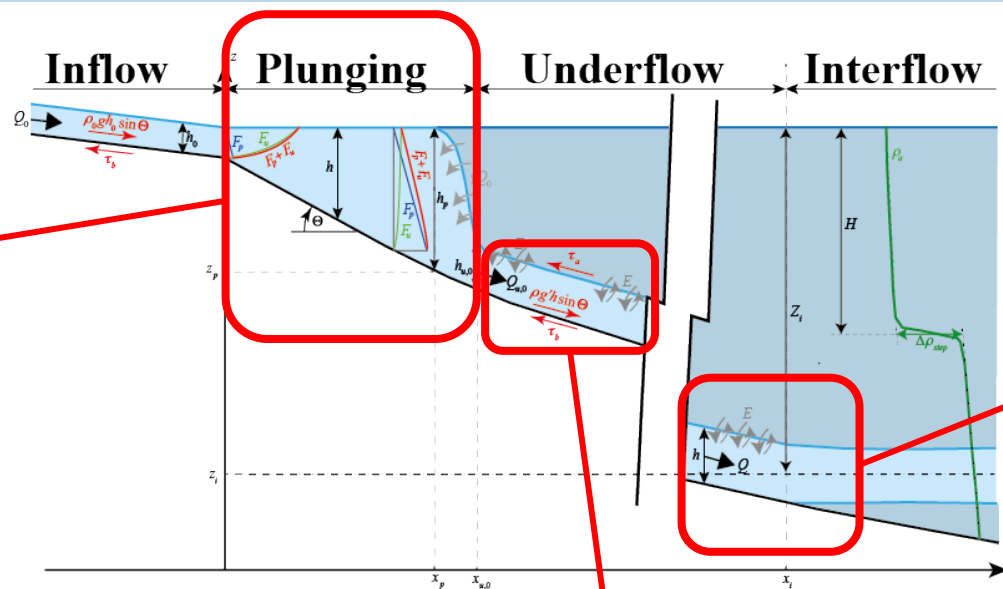
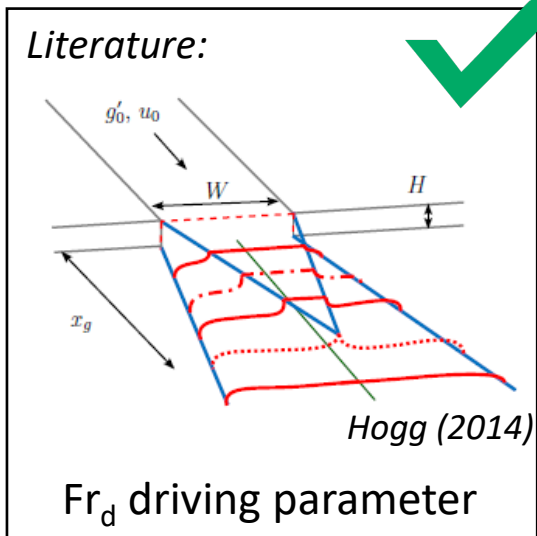
1. First direct quantification of mixing processes
2. Relation driving parameter-mixing processes

Lofting additions:

Qualitative:

1. First direct measurements of main flow process
2. Sideways lofting also present

Ongoing work: overview



Plunging additions:

Qualitative:

1. First detailed direct measurements of main flow processes
2. More mixing processes described

Quantative:

1. First direct quantification of mixing processes
2. Relation driving parameter-mixing processes
3. Fr_d driving parameter?

Underflow additions:

Qualitative:

1. Interesting flow processes visible?

Quantative:

1. Quantify processes?
2. Link processes to plunging?

Sediment?

Lofting additions:

Qualitative:

1. First direct measurements of main flow process
2. Sideways lofting also present

Conclusions



Combination of static and mobile camera systems and boat-towed ADCP measurements enables the investigation of the full 3D velocity field of a plunging flow

- The dominant flow processes were **identified**
 - Inflow-underflow: plunging, with lateral settling and a wide range of other processes
 - Underflow-interflow: lofting, both longitudinal and lateral
- The dominant flow processes related to plunging were **quantified**
 - Relation inflow properties to amount of plunging mixing
 - Plunging entrainment decreases for higher inflow densimetric Froude numbers
- *Work to find with certainty the main **control parameter(s)** driving the flow processes is ongoing*