



TECHNISCHE
UNIVERSITÄT
WIEN
Vienna | Austria



UCL

Predicting Capillary Ripples and Nonlinear Squire–Taylor Modes by Viscous–Inviscid Interaction past a Trailing Edge

Bernhard Scheichl^{1,2} Robert Bowles³

¹Institute of Fluid Mechanics and Heat Transfer, TU Wien

²AC2T research GmbH, Wiener Neustadt, Austria

³Department of Mathematics, UCL

UCL Applied Math Seminar (online), 21 March 2023

Acknowledgements & relevant papers

My thanks for funding go to

Austrian Research Promotion Agency (COMET-K2, grant no. 872176)

Our thanks, amongst others for their careful numerical work, go to

Samuel Harris, MSci (UCL, 2020)

Shiza Naqvi (UCL, Summer Project, 2020)

Michael Nguyen (UCL, Summer Project, 2021)

Georgios Pasiadis, PhD (UCL, 2022), Cyprus University of Technology

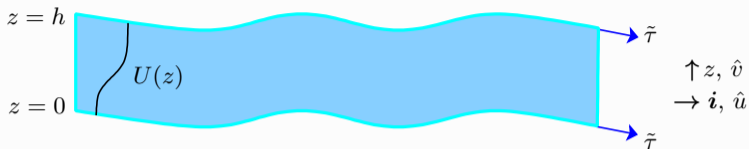
Publications

- ▶ Scheichl, Bowles & Pasiadis (JFM, **850**, 2018 & **926**, 2021)
- ▶ Scheichl, Bowles & Pasiadis (JFM, submitted soon – we talk about this)

Overview

- ▶ Motivation: local stability of non-interactive planar sheet
- ▶ Interaction problem
- ▶ Analytical & numerical treatment of individual flow regimes
- ▶ Capillary choking
- ▶ Far-downstream (WKBJ) asymptotics
- ▶ Context: (axi)symmetric flow through channel/pipe exit
- ▶ Achievements & outlook

Planar waves on a fluid (liquid) sheet



Linearise to obtain a Rayleigh problem, $c = c(k, U(z))$

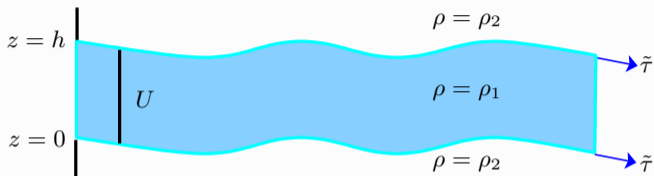
$$\mathbf{u} = U(z)\mathbf{i} + \hat{\mathbf{u}}, \quad (\hat{u}, \hat{v}) = (\psi'(z), -ik\psi(z)) \exp(ik(x - ct))$$

$$(U(z) - c) (\psi''(z) - k^2\psi(z)) + U''(z)\psi(z) = 0$$

inviscid interface conditions, surface tension $\tilde{\tau}$

This is a planar version of the Rayleigh-Plateau problem for droplet formation from a cylindrical stream of fluid.

Planar waves on a fluid sheet — uniform flow: Squire modes (1953)



Linearise to obtain a Rayleigh problem, $c = c(k, U)$

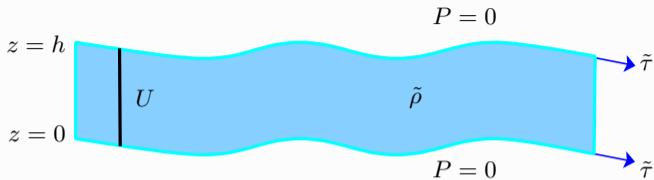
$$\mathbf{u} = U\mathbf{i} + \hat{\mathbf{u}}, \quad (\hat{u}, \hat{v}) = (\psi'(z), -ik\psi(z)) \exp(ik(x - ct))$$

$$(U - c) (\psi''(z) - k^2\psi(z)) = 0$$

Squire modes: $U(z) = U$, consider flow in air.

Instability possible if $T < 1$, depending on ρ_1/ρ_2 .

Planar waves on a fluid sheet — uniform flow: Taylor modes (1959)



Linearise to obtain a Rayleigh problem, $c = c(k, U)$

$$\mathbf{u} = U\mathbf{i} + \hat{\mathbf{u}}, \quad (\hat{u}, \hat{v}) = (\psi'(z), -ik\psi(z)) \exp(ik(x - ct))$$

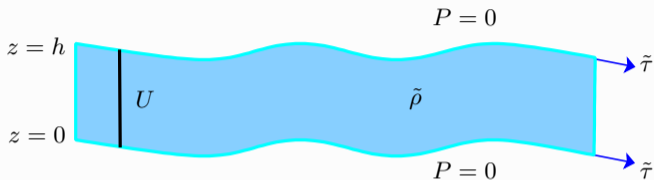
$$(U - c) (\psi''(z) - k^2\psi(z)) = 0$$

$$-(U - c)^2\psi'(z) \pm \frac{\tilde{\tau}k^2}{\tilde{\rho}}\psi(z) = 0 \quad \text{on} \quad z = 0, h$$

Taylor modes: $U(z) = U$, neglect air.

Neutral waves

Planar waves on a fluid sheet — uniform flow: Taylor modes (1959)

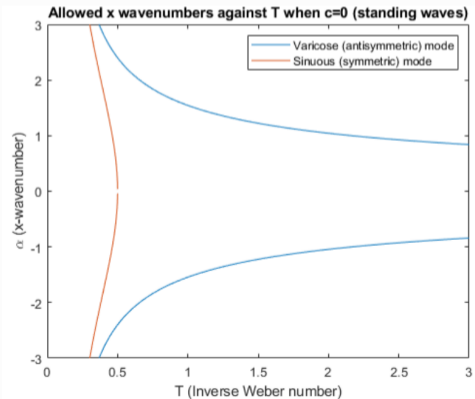
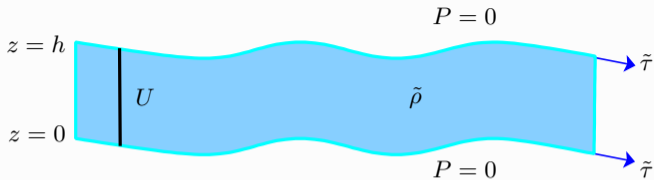


$$(c - U)^2 = \frac{\tilde{\tau}}{\tilde{\rho}h} kh \times \begin{cases} \coth(kh/2) & \text{sinuous modes} \\ \tanh(kh/2) & \text{varicose modes} \end{cases}$$

Anomalous dispersion: Drazin & Reid (1981, chap. 1)

Stability criteria for any $U(z)$: cf. Yih (1972)

Stationary planar waves on a fluid sheet — uniform flow

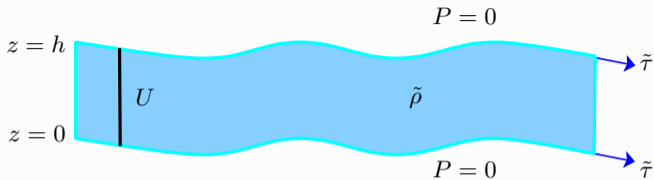


Stationary waves, $c = 0$, $(kh) = (kh)(T)$

$$1 = T(kh) \times \begin{cases} \coth(kh/2) & \text{sinuous modes} \\ \tanh(kh/2) & \text{varicose modes} \end{cases}$$

$$T = \frac{\tilde{\tau}}{U^2 \tilde{\rho} h}$$

Stationary planar waves on a fluid sheet — uniform flow



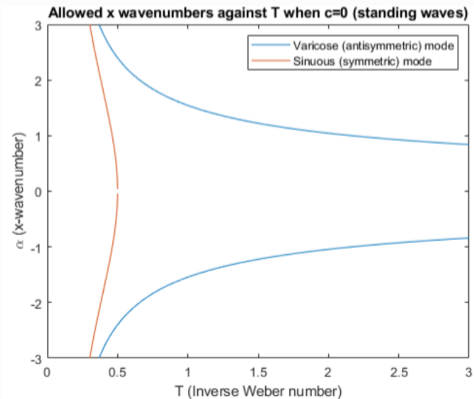
Stationary waves, $c = 0$, $(kh) = (kh)(T)$

$$1 = T(kh) \times \begin{cases} \coth(kh/2) & \text{sinuous modes} \\ \tanh(kh/2) & \text{varicose modes} \end{cases}$$

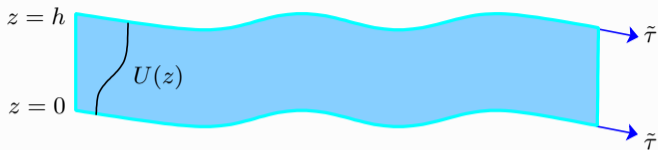
$$T = \frac{\tilde{\tau}}{U^2 \tilde{\rho} h}$$

Long waves: $kh \rightarrow 0$

$$\begin{cases} T \rightarrow 1/2 - & \text{sinuous modes} \\ T \sim 2/(kh)^2 & \text{varicose modes} \end{cases}$$



Stationary planar waves on a fluid sheet — evolving flow (M. Nguyen)



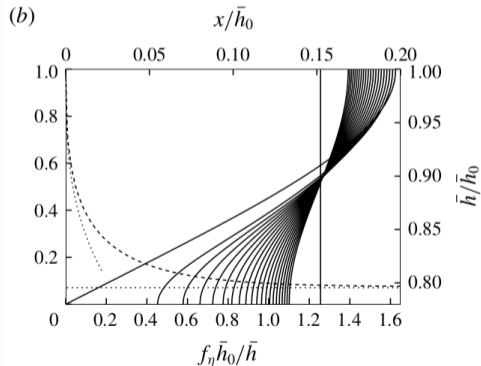
Profile evolution on $O(Re)$ -length scale

$$\bar{\psi}_z \bar{\psi}_{zx} - \bar{\psi}_x \bar{\psi}_{zz} = \bar{\psi}_{zzz},$$

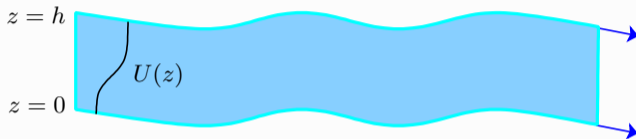
$$z = 0 : \bar{\psi} = \bar{\psi}_{zz} = 0,$$

$$z = \bar{h}(x) : \bar{\psi} - 1 = \bar{\psi}_{zz} = 0.$$

plate edge $x = 0$: Watson's profile (1964)



$$f(x, \eta) := \bar{\psi}(x, z), \quad \eta := z/\bar{h}(x), \quad h_0 := h(0)$$



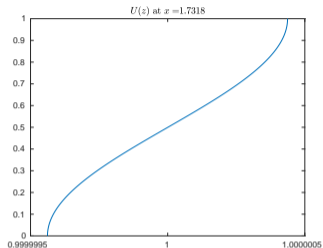
$$(U(z) - c) (\psi''(z) - k^2 \psi(z)) + U''(z) \psi(z) = 0$$

$$(U - c)^2 \psi'(z) = \pm \frac{\tilde{\tau} k^2}{\tilde{\rho}} \psi(z) \quad \text{on } z = 0, h$$

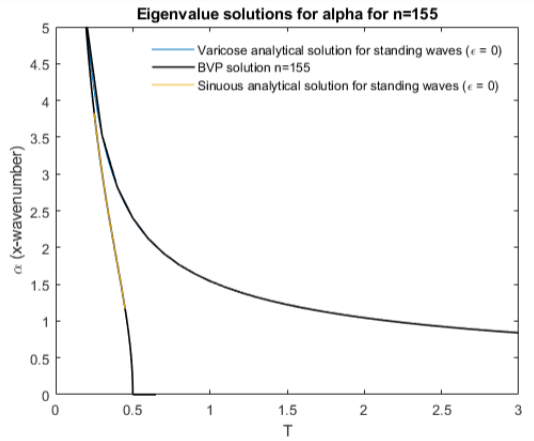
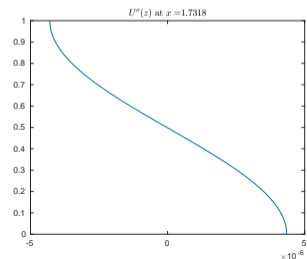
Note: $U'(0) = U'(h) = 0$

Stationary waves at $x = 1.7318$

$U(z)$



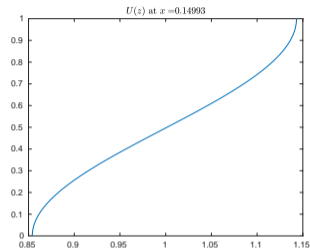
$U''(z)$



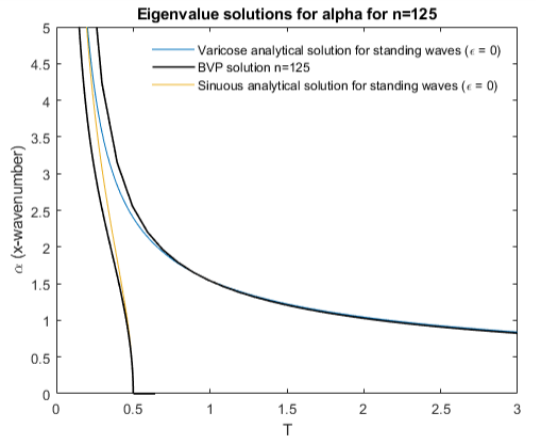
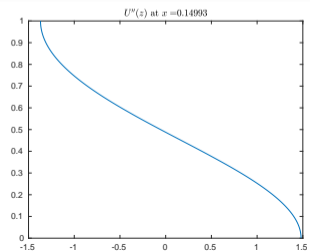
($\epsilon = 0$ is uniform profile)

Stationary waves at $x = 0.14993$

$U(z)$

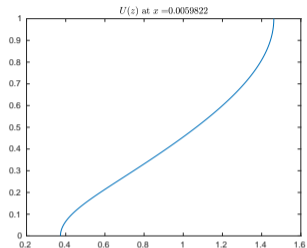


$U''(z)$

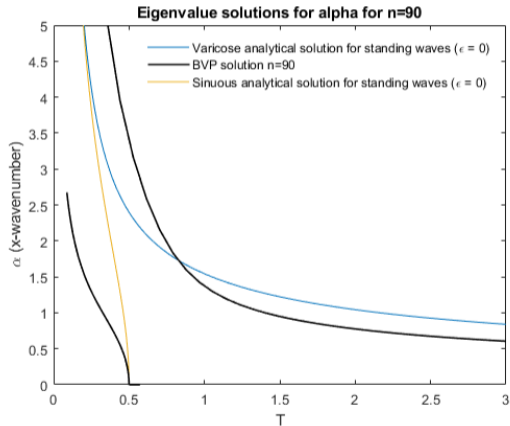
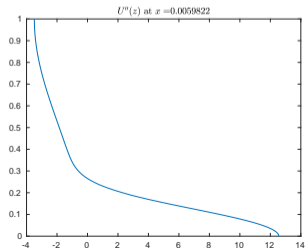


Stationary waves at $x = 0.005982$

$U(z)$

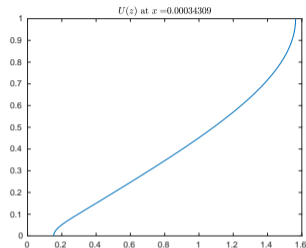


$U''(z)$

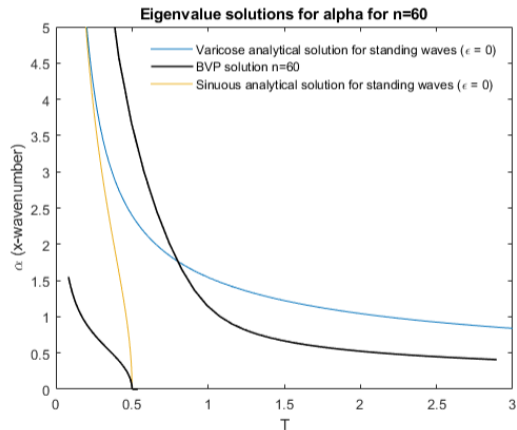
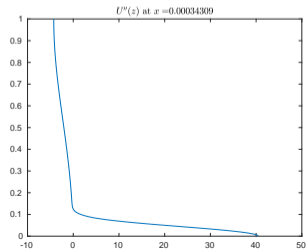


Stationary waves at $x = 0.0003431$

$U(z)$



$U''(z)$



Long-wave analysis of stationary waves

Normalise the Rayleigh problem to:

$$U (\psi'' - k^2 \psi) + U'' \psi = 0,$$
$$U^2 \psi' = \pm \bar{T} k^2 \psi(z) \quad \text{on} \quad z = 0, 1 \quad \psi(1) = 1, \quad \bar{T} = \frac{\tilde{\tau}}{\tilde{U}^2 \tilde{\rho} h}, \quad \tilde{U} = Q/h$$

Long-wave analysis of stationary waves

Normalise the Rayleigh problem to:

$$U(\psi'' - k^2\psi) + U''\psi = 0,$$
$$U^2\psi' = \pm\bar{T}k^2\psi(z) \quad \text{on} \quad z = 0, 1 \quad \psi(1) = 1, \quad \bar{T} = \frac{\tilde{\tau}}{\tilde{U}^2\tilde{\rho}h}, \quad \tilde{U} = Q/h$$

If $\psi = U(z)S(z)/U(h)$ then

$$[U^2S']' = k^2U^2S, \quad S(1) = 1, \quad U^2S' = \pm k^2\bar{T}S \quad \text{on} \quad z = 0, 1$$

Long-wave analysis of stationary waves

Normalise the Rayleigh problem to:

$$U(\psi'' - k^2\psi) + U''\psi = 0,$$
$$U^2\psi' = \pm\bar{T}k^2\psi(z) \quad \text{on} \quad z = 0, 1 \quad \psi(1) = 1, \quad \bar{T} = \frac{\tilde{\tau}}{\tilde{U}^2\tilde{\rho}h}, \quad \tilde{U} = Q/h$$

If $\psi = U(z)S(z)/U(h)$ then

$$[U^2S']' = k^2U^2S, \quad S(1) = 1, \quad U^2S' = \pm k^2\bar{T}S \quad \text{on} \quad z = 0, 1$$

Integrate:

$$\bar{T}(1 + S(0)) = \int_0^1 U^2S \, dz$$

Long-wave analysis of stationary waves

Normalise the Rayleigh problem to:

$$U(\psi'' - k^2\psi) + U''\psi = 0,$$
$$U^2\psi' = \pm \bar{T}k^2\psi(z) \quad \text{on} \quad z = 0, 1 \quad \psi(1) = 1, \quad \bar{T} = \frac{\tilde{\tau}}{\tilde{U}^2\tilde{\rho}h}, \quad \tilde{U} = Q/h$$

If $\psi = U(z)S(z)/U(h)$ then

$$[U^2S']' = k^2U^2S, \quad S(1) = 1, \quad U^2S' = \pm k^2\bar{T}S \quad \text{on} \quad z = 0, 1$$

Integrate:

$$\bar{T}(1 + S(0)) = \int_0^1 U^2S \, dz$$
$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v)S(v) \, dv \right]$$

Long-wave analysis of stationary waves

Normalise the Rayleigh problem to:

$$U(\psi'' - k^2\psi) + U''\psi = 0,$$
$$U^2\psi' = \pm\bar{T}k^2\psi(z) \quad \text{on} \quad z = 0, 1 \quad \psi(1) = 1, \quad \bar{T} = \frac{\tilde{\tau}}{\tilde{U}^2\tilde{\rho}h}, \quad \tilde{U} = Q/h$$

If $\psi = U(z)S(z)/U(h)$ then

$$[U^2S']' = k^2U^2S, \quad S(1) = 1, \quad U^2S' = \pm k^2\bar{T}S \quad \text{on} \quad z = 0, 1$$

Integrate:

$$\bar{T}(1 + S(0)) = \int_0^1 U^2S \, dz$$
$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v)S(v) \, dv \right]$$
$$\bar{T} \left(2 - k^2 \int_0^1 \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v)S(v) \, dv \right] \right) = \int_0^1 U^2S \, dz$$

Long-wave analysis of stationary waves

$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v) S(v) dv \right]$$

$$\bar{T}(1 + S(0)) = \int_0^1 U^2 S dt$$

Or:

$$\bar{T} \left(2 - k^2 \int_0^1 \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v) S(v) dv \right] \right) = \int_0^1 U^2 S dz$$

$k \rightarrow 0$, $\bar{T} = O(1)$ — sinuous mode

$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v) S(v) dv \right]$$

$$\bar{T} \left(2 - k^2 \int_0^1 \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v) S(v) dv \right] \right) = \int_0^1 U^2 S dz$$

$$S = 1 + \dots, \quad 2\bar{T} = J = \int_0^1 U^2 dz, \quad \text{or} \quad \frac{\tilde{\tau}}{\tilde{\rho} \int_0^{\tilde{h}} \tilde{u}^2 d\tilde{z}} = \frac{\tilde{\tau}}{\tilde{J}} = T = \frac{1}{2}$$

$k \rightarrow 0$, $\bar{T} = \hat{T}/k^2$ — varicose mode

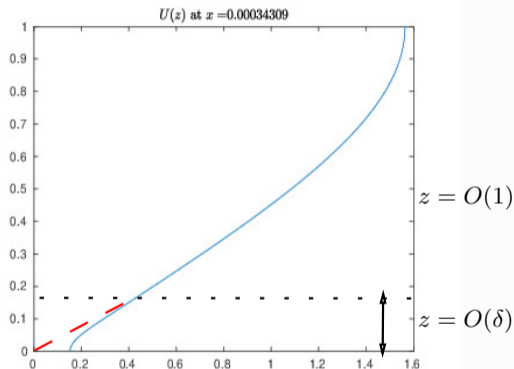
$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\frac{\hat{T}}{k^2} + \int_1^t U^2(v) S(v) dv \right]$$

$$\frac{\hat{T}}{k^2} \left(2 - k^2 \int_0^1 \frac{dt}{U^2(t)} \left[\frac{\hat{T}}{k^2} + \int_1^t U^2(v) S(v) dv \right] \right) = \int_0^1 U^2 S dz$$

$$\hat{T} \left(2 - \hat{T} \int_0^1 \frac{dz}{U^2} \right) = k^2 \left[\int_0^1 U^2 S dz + \hat{T} \int_0^1 \frac{dz}{U^2(z)} \int_1^z U^2(t) S(t) dt \right]$$

$$S = 1 + \hat{T} \int_1^z \frac{dt}{U^2(t)} + \dots, \quad \hat{T} = \frac{2}{\int_0^1 U^{-2} dz}, \quad \text{note: } S(0) = -1$$

Long waves: $U(0) \ll 1$



$$U = \delta U_\delta(\eta), \quad \eta = z/\delta$$
$$k^2 \int_0^1 \frac{dz}{U^2(z)} \sim \frac{k^2}{\delta} \int_0^\infty \frac{d\eta}{U_\delta^2(\eta)} = k^{*2} I_0$$
$$I_0 = \int_0^\infty \frac{d\eta}{U_\delta^2(\eta)}$$

$$\delta = k^2/k^{*2} \ll 1, \quad k^* = O(1)$$

Long waves: $U(0) \ll 1$, cf. interaction theory

$$S(z) = 1 + k^2 \int_1^z \frac{dt}{U^2(t)} \left[\bar{T} + \int_1^t U^2(v) S(v) dv \right]$$

$$\bar{T}(1 + S(0)) = \int_0^1 U^2 S dt = J_S$$

$$z = O(1) : \quad S = 1 + O(k^2), \quad J_S \sim J_1 = J$$

$$\text{So:} \quad \bar{T}(1 + S(0)) = J_S \sim J$$

$$z = O(\delta), \text{ put } \eta = 0 : \quad S(0) = 1 + k^{*2} (-I_0 \{\bar{T} - J_S\})$$

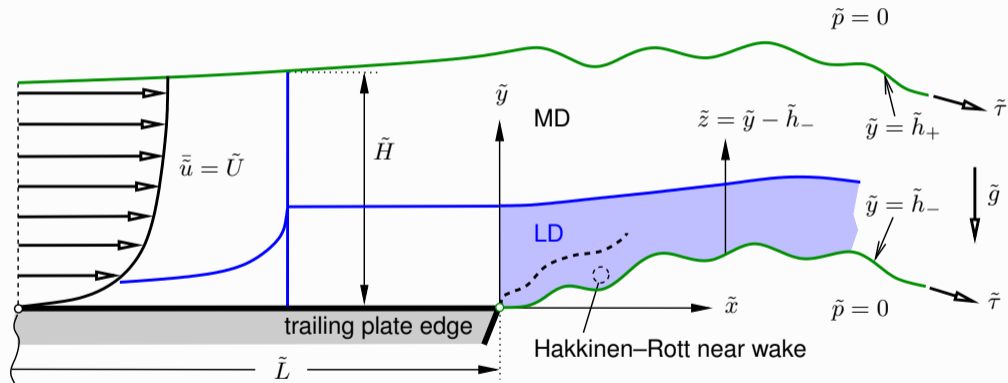
$$\text{So:} \quad \bar{T}[2 - k^{*2} I_0(\bar{T} - J)] = J$$

$$1 = \sigma k^{*2} I_0 J |T - 1|$$

$$\sigma = \frac{\text{sgn}(T - 1)T}{2T - 1}, \quad T = \bar{T}/J, \quad I_0 = \int_0^\infty \frac{d\eta}{U_\delta^2(\eta)}$$

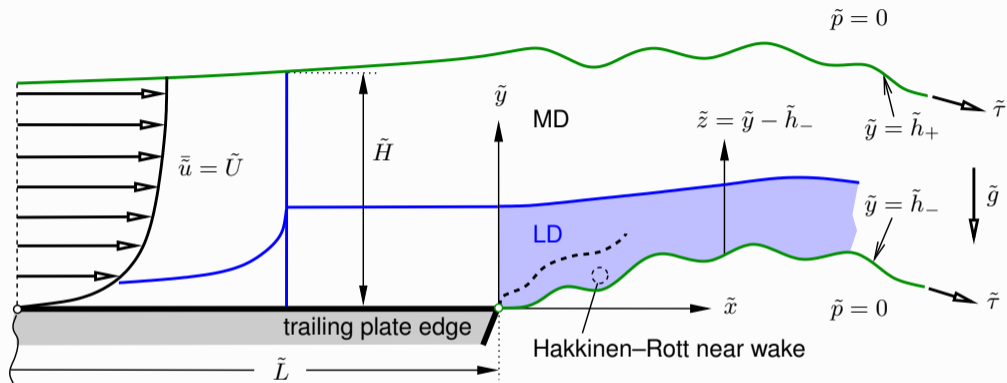
Interaction theory

Motivation: asymptotic theory of developed (real) flow negotiating trailing edge, classical 2D steady supercritical overfall of liquid layer



Topic: interactive LD limit downstream of edge

Basic scalings: high- Re shear-layer balance



Incident base flow: \tilde{Q} , adjustment length \tilde{L}

$$\tilde{Q} = \tilde{U}\tilde{H}, \quad \tilde{U}^2/\tilde{L} = \nu\tilde{U}/\tilde{H}^2 \Rightarrow \tilde{H}/\tilde{L} = \nu/\tilde{Q} = Re^{-1} \rightarrow 0$$

Interactive LD scales: $x = \tilde{x}/\tilde{L} = O(Re^{-6/7})$, $z = \tilde{z}/\tilde{H} = O(Re^{-2/7})$

Scaling laws

Watson's base flow above edge

$$\frac{\tilde{u}}{\tilde{U}} \sim u_0(z), \quad \frac{\tilde{h}_+}{\tilde{H}} \sim h_0 = \frac{\pi}{\sqrt{3}}, \quad \lambda_0 = u_0''(0) \approx 0.6930, \quad J_0 = \int_0^{h_0} u_0^2(z) dz = \lambda_0$$

Least-degenerate interactive limit: 2 control groups

$$T = \frac{\tilde{\tau}}{\tilde{\rho}\tilde{U}^2\tilde{H}J_0} = O(1), \quad G = \frac{\tilde{g}\tilde{H}}{\tilde{U}^2} \frac{h_0}{(\lambda_0^6 \epsilon^4)^{1/7}} = O(1)$$

$$\epsilon = (|T - 1|J)^{1/2}/Re \rightarrow 0$$

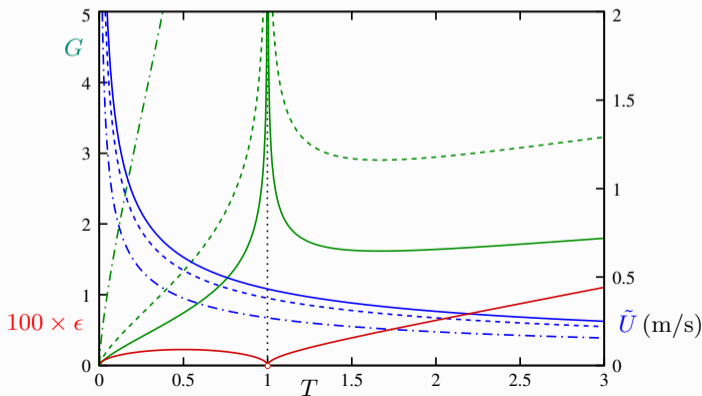
LD, leading order

$$X = (\lambda_0^5/\epsilon^6)^{1/7} x, \quad Z = (\lambda_0^4/\epsilon^2)^{1/7} z$$
$$\frac{\tilde{\psi}}{\tilde{Q}} \sim \frac{\epsilon^{4/7}}{\lambda_0^{1/7}} \Psi(X, Z), \quad \frac{\tilde{p}}{\tilde{\rho}\tilde{U}^2} \sim \frac{\epsilon^{4/7}}{\lambda_0^{6/7}} P(X), \quad \left(\frac{\tilde{h}_-}{\tilde{H}}, \frac{\tilde{h}_+}{\tilde{H}} - h_0 \right) \sim \frac{\epsilon^{2/7}}{\lambda_0^{4/7}} [H_-(X), H_+(X)]$$

Flow over edge in lab (H_2O , standard conditions): vary $\tilde{H}_0 = h_0 \tilde{H}$, \tilde{U}

$$\tilde{H}_r = \left(\frac{h_0^9 \lambda_0^6}{J_0^3} \frac{\tilde{\nu}^4 \tilde{\tau}^5}{\tilde{g}^7 \tilde{\rho}^5} \right)^{1/16} \approx 0.774 \text{ mm (!)}, \quad \tilde{U}_r = \left(\frac{h_0^7}{\lambda_0^6 J_0^{13}} \frac{\tilde{g}^7 \tilde{\tau}^{11}}{\tilde{\nu}^4 \tilde{\rho}^{11}} \right)^{1/32} \approx 0.433 \frac{\text{m}}{\text{s}}$$

$$G = \left(\frac{\tilde{H}_0}{\tilde{H}_r} \right)^{16/7} \frac{T^{5/7}}{|T-1|^{2/7}}, \quad \tilde{U} = \left(\frac{\tilde{H}_r}{\tilde{H}_0} \frac{1}{T} \right)^{1/2}$$



$T = 1$:
interaction invalid,
choking

$\tilde{H}_0 = \tilde{H}_r$ (—)
 $\tilde{H}_0 = 1 \text{ mm}$ (---)
 $\tilde{H}_0 = 2 \text{ mm}$ (-·-·-)

Interaction problem: $X \geq 0$, jet-type P/A law

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = -P'(X) + \Psi_{ZZZ}$$

$$X > 0, Z = 0: \Psi = \Psi_{ZZ} = 0$$

$$\Psi_{ZZ}(X, \infty) = 1, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - Z)$$

$$P = C(G + SA''), \quad C = T/(2T - 1), \quad S = \text{sgn}(T - 1)$$

$$\Psi(0+, Z) = \Psi(0-, Z), \quad A'(0+) = A'(0-), \quad A''(0+) = -SG \iff P(0) = 0$$

Classification: streamline curvature vs. capillarity

$$P' = \sigma A''', \quad \sigma = SC \begin{cases} > 0 & (0 < T < 1/2 \text{ or } T > 1) & \dots \text{ stabilising feedback: waves} \\ < 0 & (1/2 < T < 1) & \dots \text{ compressive/expansive} \\ = \mp \infty & (T = 1/2 \pm) & \dots \text{ choking (cf. linear waves)} \\ = \pm 1 & (T = 1 \pm) & \dots \text{ regular limits} \\ = 0 & (T = 1) & \dots \text{ choking (excluded)} \end{cases}$$

Elevations of free streamlines

Laplace pressure & interaction law

$$P = TH''/|T - 1| = C(G + SA''), \quad C = T/(2T - 1), \quad S = \text{sgn}(T - 1)$$

No slip to free slip: small-scale (Navier–Stokes) analysis

$$X = 0+: \quad H_- = H'_- = H''_- = 0 \quad \Rightarrow \quad P(0) = 0$$

Thus,

$$H_{\pm}(X) = \underbrace{(1 - C)[SGX^2/2 - A'(0)X - A(0)]}_{\text{parabola:}} - \underbrace{\begin{cases} CA(X) \\ (C - 1)A(X) \end{cases}}$$

$0 < T < 1/2$: classical downfall,

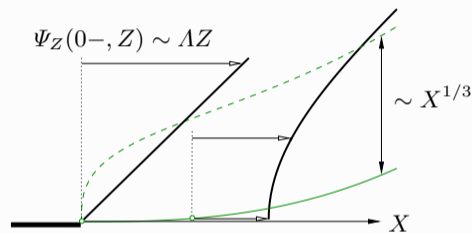
$1 < T$: 'upfall',

H_{\pm} wavy, in phase

H_{\pm} wavy, in antiphase

$(X \gg 1)$

Hakkinen–Rott near wake



$$0 < X \ll (T/|2T - 1|)^{3/7}, \quad \eta = Z(\Lambda/X)^{1/3}:$$

$$[\Psi, P] \sim X^{2/3}[\Lambda^{1/3}F(\eta), \Lambda^{4/3}\Pi], \quad \Pi \approx 0.61334$$

$$\eta \rightarrow \infty: \quad F' = \eta + \text{EST}$$

grants

$$A''(X) + SG = O(X^{2/3}), \quad H''_- = \frac{|1 - T|}{T} P$$

Downstream marching well-posed up to flow reversal

F not perturbed by eigensolutions (Scheichl 2023)

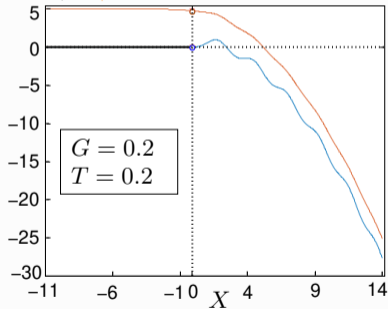
Condensed interaction

$$G = 0, \quad T = 1/2: \quad [\Psi, P] \equiv X^{2/3}[\Lambda^{1/3}F(\eta), \Lambda^{4/3}\Pi]$$

Numerical results (G. Pasiás)

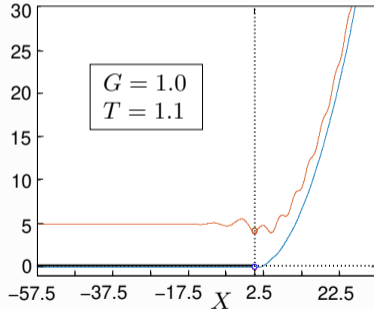
Sinuuous / supercritical:
no waves upstream

H_- , $H_+ + 5$

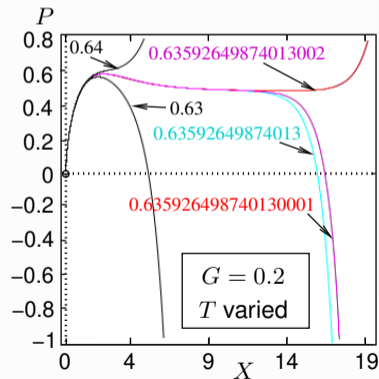


Varicose / subcritical:
waves upstream

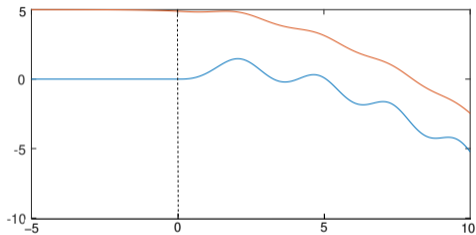
$H_- 5$, $H_+ + 5$



Bifurcation:
compressive flow reversal
vs.
expansive blow-up

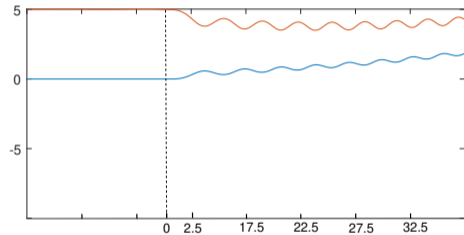


Sinuuous / 'flapping'



$$G = 0.1, T = 0.2$$

Varicose / 'sausage-type'



$$G = 0.01, T = 2.0$$

Choking of a capillary wave & non-wavy breakdown: $T \sim 1/2$

$$P = \frac{T}{2T-1} [G + \text{sgn}(T-1)A'']$$

Least-degenerate distinguished limit near condensed interaction

$$\hat{G} = \alpha^5 G = O(1), \quad \alpha = (4|T-1/2|)^{-1/7} \rightarrow \infty$$

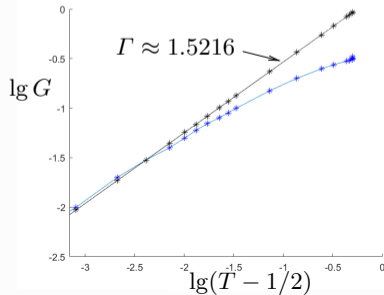
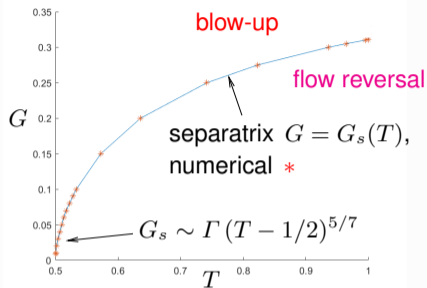
$$[X, Z, \Psi, A, P] \sim [\alpha^3 \hat{X}, \alpha \hat{Z}, \alpha^2 \hat{\Psi}, \alpha \hat{A}, \alpha^2 \hat{P}]$$

$$\hat{S}\hat{P} = \hat{G} - \hat{A}'', \quad \hat{S} = \text{sgn}(T-1/2)$$

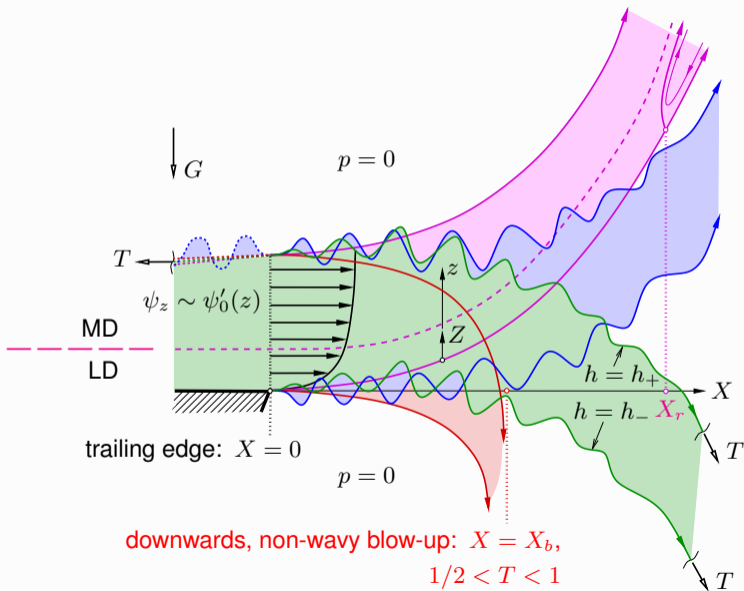
$$\hat{\Psi}(0, \hat{Z}) = \hat{Z}^2/2, \quad \hat{A}'(0) = 0, \quad \hat{A}''(0) = \hat{G}$$

$\hat{S} = -1$: (cnoidal) waves ($\hat{G} \rightarrow \infty$)

$$\hat{S} = +1: 4^{5/7} \hat{G} \begin{cases} < \Gamma: \text{flow reversal} & (\hat{X} \rightarrow \infty) \\ = \Gamma: \text{Goldstein wake} & (\hat{X} \rightarrow \infty) \\ > \Gamma: \text{finite-}\hat{X} \text{ blow-up} \end{cases}$$



Condensed results: 4 fundamental detached-jet manifestations



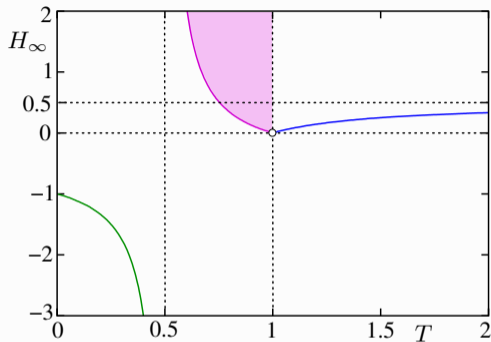
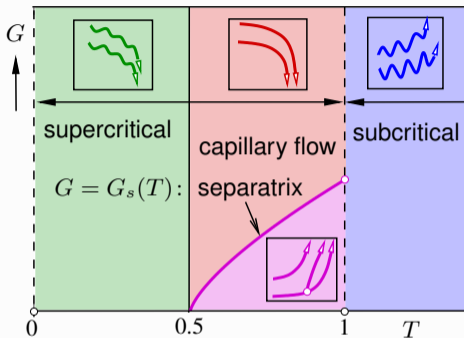
upwards, non-wavy
reversed-flow breakdown:
 $1/2 < T < 1$

upwards, symmetric (varicose)
modes, phase shift indefinite:
 $1 < T$

cf. inviscid slender jets
(Keller & Weitz 1957)

downwards,
antisymmetric (sinuous) modes,
self-consistent for all X :
 $0 < T < 1/2$

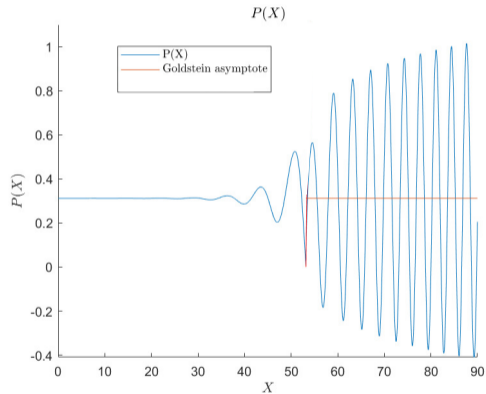
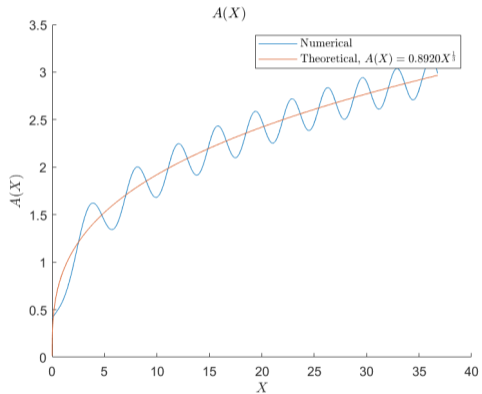
Condensed results: 3 manifestations valid for $X < \infty$



$$A \sim \begin{cases} a_G X^{1/3} & \rightarrow +\infty & (0 < T < 1/2, T > 1 \text{ or } 1/2 < T < 1, G = G_s) \\ A_\infty X^2/2 & \rightarrow -\infty & (1/2 < T < 1, G < G_s) \end{cases}$$

$$H_- \sim H_\infty \frac{GX^2}{2}, \quad H_\infty = \frac{|T-1|}{2T-1} \times \begin{cases} 1 & (0 < T < 1/2, T > 1) \\ 1 & (1/2 < T < 1, G = G_s) \\ (1 - A_\infty/G) & (1/2 < T < 1, G < G_s) \end{cases}$$

WKBJ analysis



WKBJ analysis: $\Psi = X^{1/3}F(X, \eta)$, $\eta = Z/X^{1/3}$, $X \rightarrow \infty$

Interaction problem

$$\underbrace{(F_\eta^2 - 2FF_{\eta\eta})/3 - F_{\eta\eta\eta}}_{\text{non-||, viscosity}} + \underbrace{X(F_\eta F_{\eta X} - F_X F_{\eta\eta})}_{\text{'rapid' convection}} = -X^{1/3}P'(X)$$

$$P'(X) = \sigma A'''(X), \quad A(X) = X^{1/3}a(X)$$

$$\eta = 0: F = F_{\eta\eta} = 0, \quad \eta \rightarrow \infty: F_\eta = \eta + a + \text{EST}$$

Translational invariance absorbed

$$X \mapsto X - X_0, \quad \eta \mapsto Z/(X - X_0)^{1/3}$$

Global conservation of momentum

$$F = \underbrace{F_m(\eta)}_{\text{mean flow}} + \underbrace{f(X, \eta)}_{\text{'rapid' convection}}, \quad f \rightarrow 0$$

WKBJ analysis: $X \rightarrow \infty$

Asymptotic hierarchy: algebraic-log decay

$$k(X) = (6k_0/7)X^{1/6} + k_1X^\kappa + o(1) \quad (k_0 > 0, \quad 1/6 > \kappa > -1), \quad E = \exp[ik(X)X]$$

$$\{f, a - a_m\} = E^0 \left[\underbrace{X^{2\mu+7/6} b_{00} \{f_{00}(\eta), 1\}}_{\text{by 'Reynolds stress'}} + \dots \right]$$

$$+ E^1 X^\mu \left[\underbrace{b_{10} \{f_{10}(\eta), 1\}}_{\text{eigenfunction}} + \underbrace{X^\beta b_{11} \{f_{11}(\eta), 1\} + X^{-7/6} b_{12} \{f_{12}(\eta), 1\} + \dots}_{\text{enforced}} \right]$$

$$+ E^2 X^{2\mu} [b_{20} \{f_{20}(\eta), 1\} + \dots] + O(E^3 X^{3\mu}) + c.c. \quad (\mu, \beta < 0)$$

$$X^{1/3} P' / \sigma = \dots - ik_0^3 E^1 X^{\mu+7/6} [b_{10} + b_{11} X^\beta + (3b_{10}k_1/k_0)(\kappa + 1)X^{\kappa-1/6} + \dots] + \dots + c.c.$$

RC: $X\partial_X \sim XE'/E \sim ik_0X^{7/6} \quad \square$

WKBJ analysis: $X \rightarrow \infty$

$$k(X) = (6k_0/7)X^{1/6} + k_1X^\kappa + o(1) \quad (k_0 > 0, \quad 1/6 > \kappa > -1), \quad E = \exp[ik(X)X]$$

$$\{f, a - a_m\} = E^0 \left[\underbrace{X^{2\mu+7/6} b_{00} \{f_{00}(\eta), 1\}}_{\text{by 'Reynolds stress'}} + \dots \right]$$

$$+ E^1 X^\mu \left[\underbrace{b_{10} \{f_{10}(\eta), 1\}}_{\text{eigenfunction}} + \underbrace{X^\beta b_{11} \{f_{11}(\eta), 1\} + X^{-7/6} b_{12} \{f_{12}(\eta), 1\} + \dots}_{\text{enforced}} \right]$$

$$+ E^2 X^{2\mu} [b_{20} \{f_{20}(\eta), 1\} + \dots] + O(E^3 X^{3\mu}) + c.c. \quad (\mu, \beta < 0)$$

$$X^{1/3} P' / \sigma = \dots - ik_0^3 E^1 X^{\mu+7/6} [b_{10} + b_{11} X^\beta + (3b_{10}k_1/k_0)(\kappa + 1)X^{\kappa-1/6} + \dots] + \dots + c.c.$$

Upstream history fixes amplitudes $b_{jl} \in \mathbb{C}$

We seek $F_m(\eta), f_{10}(\eta), k_0, \mu$

WKBJ analysis: $f'_{jl}(\infty) = 1$

P' , k' , nonlinear, non-||, viscosity \Rightarrow forcing $I_{jl}(\eta)$ of j -th mode, $I_{10} = 0$

► $j > 0$, $l \geq 0$

$$F'_m f'_{jl} - F''_m f_{jl} - \sigma(jk_0)^2 = I_{jl}, \quad f_{jl}(0) = 0 \Rightarrow \frac{f_{jl}(\eta)}{F'_m(\eta)} = \int_0^\eta \frac{\sigma(jk_0)^2 + I_{jl}(t)}{F'^2_m(t)} dt$$

$$1 - \sigma(T)(jk_0)^2 I_0 = \int_0^\infty \frac{I_{jl}(\eta)}{F'^2_m(\eta)} d\eta, \quad I_0 = \int_0^\infty \frac{d\eta}{F'^2_m(\eta)}$$

WKBJ analysis: $f'_{jl}(\infty) = 1$

P' , k' , nonlinear, non-||, viscosity \Rightarrow forcing $I_{jl}(\eta)$ of j -th mode, $I_{10} = 0$

► $j > 0$, $l \geq 0$

$$F'_m f'_{jl} - F''_m f_{jl} - \sigma(jk_0)^2 = I_{jl}, \quad f_{jl}(0) = 0 \Rightarrow \frac{f_{jl}(\eta)}{F'_m(\eta)} = \int_0^\eta \frac{\sigma(jk_0)^2 + I_{jl}(t)}{F'^2_m(t)} dt$$

$$1 - \sigma(T)(jk_0)^2 I_0 = \int_0^\infty \frac{I_{jl}(\eta)}{F'^2_m(\eta)} d\eta, \quad I_0 = \int_0^\infty \frac{d\eta}{F'^2_m(\eta)}$$

► $j = 1$, $l = 0$

$$1 = \sigma(T)k_0^2 I_0, \quad \text{Im } f_{10} = 0$$

WKBJ analysis: $f'_{jl}(\infty) = 1$

P' , k' , nonlinear, non-||, viscosity \Rightarrow forcing $I_{jl}(\eta)$ of j -th mode, $I_{10} = 0$

► $j > 0, l \geq 0$

$$F'_m f'_{jl} - F''_m f_{jl} - \sigma(jk_0)^2 = I_{jl}, \quad f_{jl}(0) = 0 \Rightarrow \frac{f_{jl}(\eta)}{F'_m(\eta)} = \int_0^\eta \frac{\sigma(jk_0)^2 + I_{jl}(t)}{F'^2_m(t)} dt$$

$$1 - \sigma(T)(jk_0)^2 I_0 = \int_0^\infty \frac{I_{jl}(\eta)}{F'^2_m(\eta)} d\eta, \quad I_0 = \int_0^\infty \frac{d\eta}{F'^2_m(\eta)}$$

► $j = 1, l = 0$

$$1 = \sigma(T)k_0^2 I_0, \quad \text{Im } f_{10} = 0$$

► $j = l = 0$

$$(F'^2_m - 2F_m F''_m)/3 - F'''_m \sim \underbrace{2k_0 |b_{10}|^2 X^{2\mu+7/6} \text{Im}(\overline{f_{10}} f''_{10})}_{\text{dominant Reynolds stress}} = 0 \quad \forall \mu$$

$\Rightarrow b_{00} = 0, \quad U_\delta = F'_m = G' \dots$ Goldstein wake, $a_m \approx 0.89200$

WKBJ analysis: $f'_{jl}(\infty) = 1$

- ▶ $j = 0, l > 0$: $E^0 X^{\lambda(l)}$ (non-interactive)

$$(2/3 + \lambda)(G' f'_{0l} - G'' f_{0l}) - 2G f''_{0l}/3 - f'''_{0l} = I_{0l}, \quad f_{0l}(0) = f''_{0l}(0) = 0$$

$$\eta \rightarrow \infty: f'_{0l} = 1 + \text{EST}$$

- ▶ $j = 1, l = 0$: $E^1 X^\mu$

$$G' f'_{10} - G'' f_{10} - \sigma k_0^2 = 0$$

$$1 = \sigma(T) k_0^2 I_0, \quad I_0 = \int_0^\infty \frac{d\eta}{G'^2(\eta)} \approx 0.8525 \Rightarrow k_0(T), \quad \sigma > 0 \quad \square$$

- ▶ else

$$G' f'_{jl} - G'' f_{jl} - \sigma(jk_0)^2 = I_{jl}$$

$$1 - j^2 = \int_0^\infty \frac{I_{jl}(\eta)}{G'^2(\eta)} d\eta$$

WKBJ analysis: $1 - j^2 = \int_0^\infty (I_{jl}/G'^2)(\eta) d\eta$ (SC)

► $j = 2, l = 0: E^2 X^{2\mu}$

$$I_{20} = (f_{10}f_{10}'' - f_{10}'^2) \frac{b_{01}^2}{2b_{20}} \Rightarrow \frac{b_{20}}{b_{10}^2} = \frac{1}{6} \int_0^\infty \frac{f_{10}'^2 - f_{10}f_{10}''}{G'^2} d\eta, \quad \text{Im } f_{20} = 0$$

► $j = 1, l = 1: E^1 X^{\mu+\beta}$

$$\begin{aligned} \text{Re}(b_{11}I_{11}/b_{10}) &= k_0k_1 \underbrace{[3\sigma - (G'f_{10}' - G''f_{10})/k_0^2]}_{2\sigma} (\kappa + 1) X^{\kappa-1/6-\beta} \\ &\quad - \underbrace{(b_{20}/b_{10}^2)|b_{10}|^2(f_{20}'f_{10}' - 2f_{20}f_{10}'' + f_{10}f_{20}'')}_{\text{nonlinear feedback}} X^{2\mu-\beta} \end{aligned}$$

$$\text{Im}(b_{11}I_{11}/b_{10}) = O(X^{-7/6-\beta})$$

$$\Rightarrow \beta = 2\mu = \kappa - 1/6 > -7/6 \quad \square$$

WKBJ analysis: $1 - j^2 = \int_0^\infty (I_{jl}/G'^2)(\eta) d\eta$ (SC)

- $j = 2, l = 0: E^2 X^{2\mu}$

$$I_{20} = (f_{10}f''_{10} - f'^2_{10}) \frac{b^2_{01}}{2b_{20}} \Rightarrow \frac{b_{20}}{b^2_{10}} = \frac{1}{6} \int_0^\infty \frac{f'^2_{10} - f_{10}f''_{10}}{G'^2} d\eta, \quad \text{Im } f_{20} = 0$$

- $j = 1, l = 1: E^1 X^{\mu+\beta}$

$$\begin{aligned} \text{Re}(b_{11}I_{11}/b_{10}) &= 2\sigma k_0 k_1 (\kappa + 1) \\ &\quad - (b_{20}/b^2_{10}) |b_{10}|^2 (f'_{20}f'_{10} - 2f_{20}f''_{10} + f_{10}f''_{20}) \end{aligned}$$

$$\text{Im}(b_{11}I_{11}/b_{10}) \equiv 0$$

$$\beta = 2\mu = \kappa - 1/6 > -7/6,$$

$$\text{(SC)} \Rightarrow k_1 \propto |b_{10}|^2$$

WKBJ analysis: $1 - j^2 = \int_0^\infty (I_{jl}/G'^2)(\eta) d\eta$ (SC)

► $j = 1, l = 2$: $E^1 X^{\mu-7/6}$

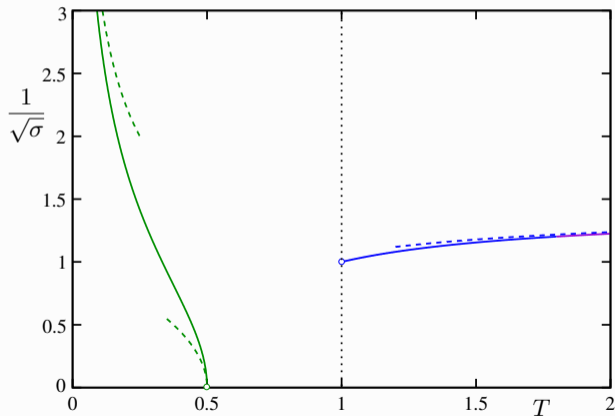
$$\begin{aligned} \text{Im}(b_{12}I_{12}/b_{10}) &= \underbrace{[(2/3 + \mu)(\overbrace{G' f'_{10} - G'' f_{10}}^{\sigma k_0^2}) - 2/3 G f''_{10} - f'''_{10}]/k_0}_{\text{non-||, viscosity}} - \sigma k_0(3\mu + 3/2) \\ &= -(2/3 G f''_{10} + f'''_{10})/k_0 - \sigma k_0(5/6 + 2\mu) \end{aligned}$$

$$\text{(SC)} \Rightarrow \mu = -\frac{5}{12} - \frac{\Omega}{2} > -\frac{7}{12}, \quad \Omega = \int_0^\infty \frac{2/3 G f''_{10} + f'''_{10}}{G'^2} d\eta \approx 0.1074 \quad \square$$

$$\beta = -\frac{5}{6} - \Omega, \quad \kappa = -\frac{2}{3} - \Omega$$

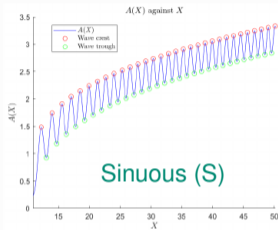
WKBJ analysis: recovers linear long-wave limit

$$k_0 = \frac{1}{\sqrt{I_0 \sigma(T)}}, \quad I_0 = \int_0^\infty \frac{d\eta}{G'^2(\eta)}$$

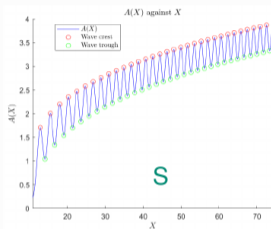


WKBJ analysis (G. Pasiadis)

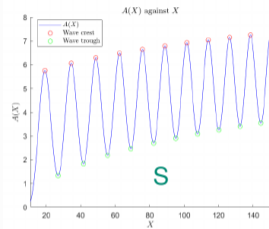
Numerical trends confirm $b_{10} \rightarrow \infty$, $k_0 \rightarrow 0$ as $T \rightarrow 1/2-$ (choking)



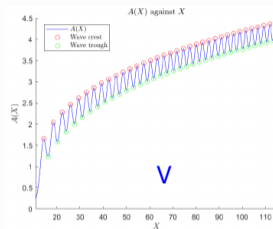
(a) $G = 0.2, T = 0.1$



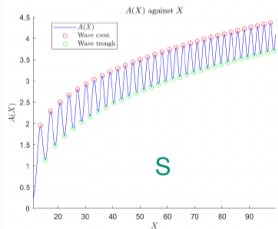
(b) $G = 0.2, T = 0.2$



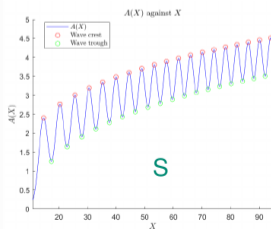
(e) $G = 0.2, T = 0.49$



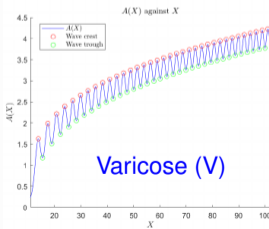
(f) $G = 0.2, T = 1.1$



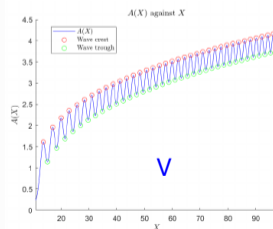
(c) $G = 0.2, T = 0.3$



(d) $G = 0.2, T = 0.4$



(g) $G = 0.2, T = 2$



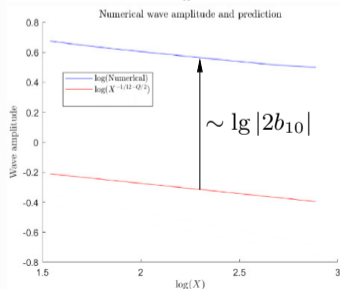
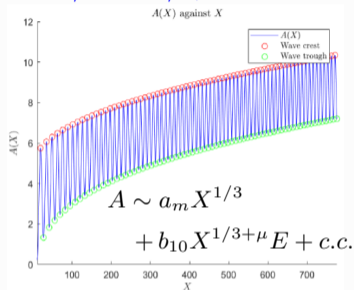
(h) $G = 0.2, T = 5$

WKBJ analysis (G. Pasiadis)

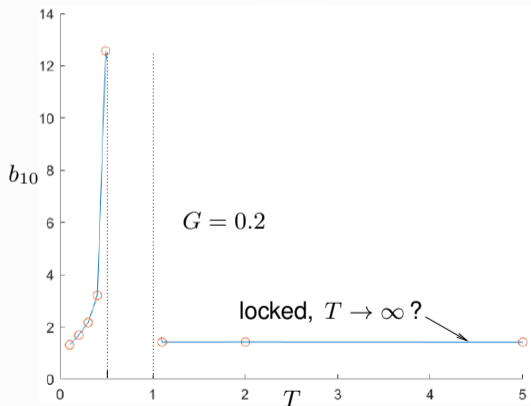
$$\mu = -5/12 - \Omega/2, \quad \Omega \approx 0.1074$$

$$G = 0.2,$$

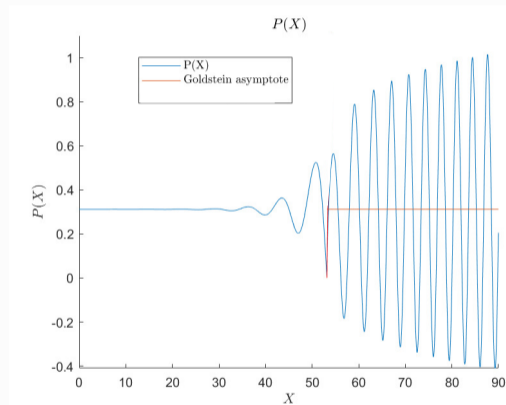
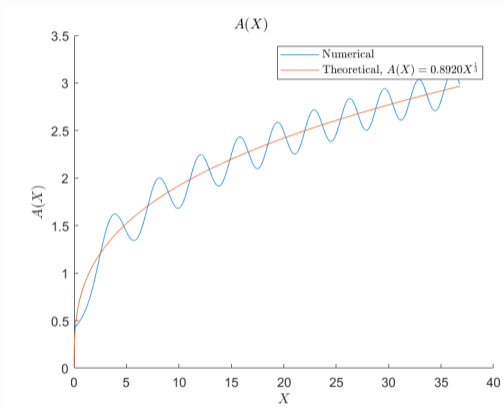
$$T = 0.49$$



WKBJ don't unveil $b_{10}(G, T) \dots$

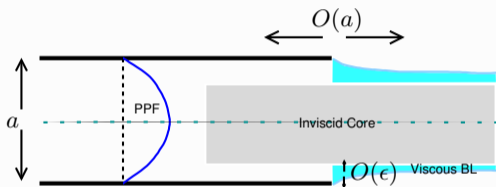


WKBJ analysis (G. Pasiadis)



$$X \rightarrow \infty: A \sim a_m X^{1/3} + b_{10} X^{-1/12 - \Omega/2} E(X) + c.c., \quad P \sim -(b_{10}/I_0) X^{1/4 - \Omega/2} E(X) + c.c. !$$

Flow through channel exit ($G = 0$, S. Harris)



$$\epsilon = Re^{-1/3}, \quad Re = U_{\max} a / \nu$$

No surface tension: Tillett (1968)

Flow symmetric, gravity in flow direction.

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = \Psi_{ZZZ}$$

$$X > 0, \quad Z = 0: \quad \Psi = \Psi_{ZZ} = 0$$

$$\Psi_{ZZ}(X, \infty) = 2, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - 2Z)$$

$$\Psi(0+, Z) = \Psi(0-, Z) = Z^2$$

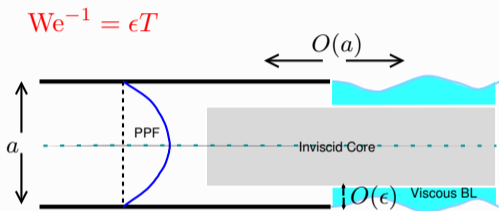
Symmetry imposes no net displacement from BL

No upstream influence

$$H = A$$

$$H \sim X^{1/3} \quad \text{Goldstein wake}$$

Flow through channel exit ($G = 0$, S. Harris)



$$\epsilon = Re^{-1/3}, \quad Re = U_{\max} a / \nu$$

$$P = TA_{XX}$$

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = -P_X + \Psi_{ZZZ}$$

$$X > 0, \quad Z = 0: \quad \Psi = \Psi_{ZZ} = 0$$

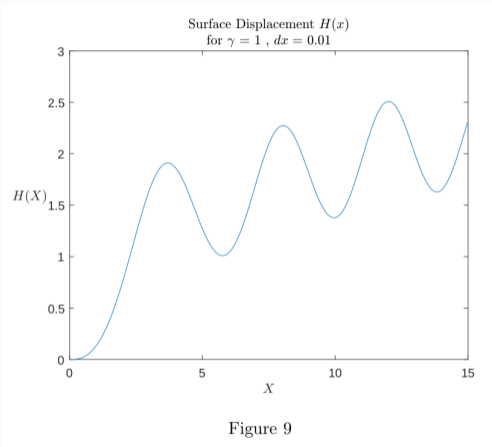
$$\Psi_{ZZ}(X, \infty) = 2, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - 2Z)$$

$$\Psi(0+, Z) = \Psi(0-, Z) = Z^2$$

- ▶ No upstream influence
- ▶ $H = A$
- ▶ T can be scaled out:

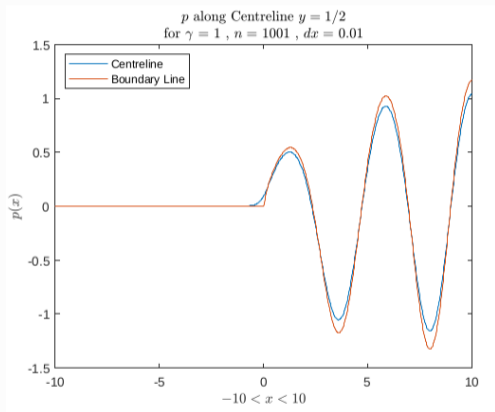
$$[X, \Psi, H, P] \sim [T^{3/7}, T^{2/7}, T^{1/7}, T^{2/7}]$$

Flow through channel exit ($G = 0$, S. Harris)



- ▶ Waves with Goldstein wake emerging on average

Flow through channel exit ($G = 0$, S. Harris)



Tillett's core-flow/Rayleigh problem

$$y(1 - y) [v_{xx} + v_{yy}] + 2v = 0$$

$$v(x, \frac{1}{2}) = 0$$

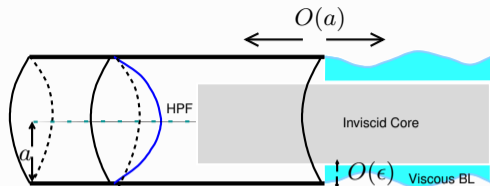
$$v(x, 0) = -\frac{1}{2}p_x$$

$$\psi_x = -v$$

$$p = 2(1 - 2y)\psi - 2y(1 - y)\psi_y$$

- Weak linear upstream influence through core.

Flow through pipe exit ($G = 0$, S. Harris)



$$P = T(A + A_{XX})$$

$$\epsilon = Re^{-1/3}, \quad Re = U_{\max} a / \nu$$

$$p \sim We^{-1} (\nabla \cdot \mathbf{n})$$

$$\nabla \cdot \mathbf{n} = \frac{-R''(x)}{(1 + R'^2)^{3/2}} + \frac{1}{R\sqrt{1 + R'^2}}$$

$$R(x) = 1 - \epsilon H(x), \quad We^{-1} = \frac{\tilde{\tau}}{\tilde{\rho} U_{\max}^2 a} = \epsilon T$$

$$p \sim \epsilon^2 T (H + H'')$$

$+H$: cf. subcritical hydrostatic layer

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = -P_X + \Psi_{ZZZ}$$

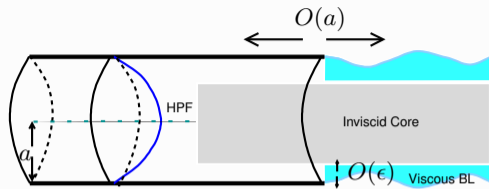
$$X > 0, \quad Z = 0: \quad \Psi = \Psi_{ZZ} = 0$$

$$\Psi_{ZZ}(X, \infty) = 2, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - 2Z)$$

$$\Psi(0+, Z) = \Psi(0-, Z) = Z^2$$

$$H = A$$

Flow through pipe exit ($G = 0$, S. Harris)



$$\epsilon = Re^{-1/3}, \quad Re = U_{\max} a / \nu$$

$$p \sim We^{-1} (\nabla \cdot \mathbf{n})$$

$$\nabla \cdot \mathbf{n} = \frac{-R''(x)}{(1+R^2)^{3/2}} + \frac{1}{R\sqrt{1+R^2}}$$

$$R(x) = 1 - \epsilon H(x), \quad We^{-1} = \frac{\tilde{\tau}}{\tilde{\rho} U_{\max}^2 a} = \epsilon T$$

$$p \sim \epsilon^2 T (H + H'')$$

$$P = T (A + A_{XX})$$

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = -P_X + \Psi_{ZZZ}$$

$$X > 0, \quad Z = 0: \quad \Psi = \Psi_{ZZ} = 0$$

$$\Psi_{ZZ}(X, \infty) = 2, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - 2Z)$$

$$\Psi(0+, Z) = \Psi(0-, Z) = Z^2$$

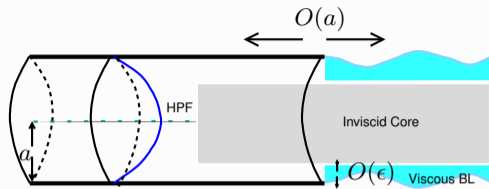
$$H = A$$

$$T \rightarrow 0$$

$$[X, H] \sim [T^{3/7}, T^{1/7}]$$

$$P = T^{5/7} A + A_{XX} \sim A_{XX}$$

Flow through pipe exit ($G = 0$, S. Harris)



$$\epsilon = Re^{-1/3}, \quad Re = U_{\max} a / \nu$$

$$p \sim We^{-1} (\nabla \cdot \mathbf{n})$$

$$\nabla \cdot \mathbf{n} = \frac{-R''(x)}{(1+R^2)^{3/2}} + \frac{1}{R\sqrt{1+R^2}}$$

$$R(x) = 1 - \epsilon H(x), \quad We^{-1} = \frac{\tilde{\tau}}{\tilde{\rho} U_{\max}^2 a} = \epsilon T$$

$$p \sim \epsilon^2 T (H + H'')$$

$$P = T (A + A_{XX})$$

$$\Psi_Z \Psi_{ZX} - \Psi_X \Psi_{ZZ} = -P_X + \Psi_{ZZZ}$$

$$X > 0, \quad Z = 0: \quad \Psi = \Psi_{ZZ} = 0$$

$$\Psi_{ZZ}(X, \infty) = 2, \quad A(X) = \lim_{z \rightarrow \infty} (\Psi_Z - 2Z)$$

$$\Psi(0+, Z) = \Psi(0-, Z) = Z^2$$

$$H = A$$

$$T \rightarrow \infty$$

$$[X, H] \sim [T^3, T]$$

$$P = A + T^{-7} A_{XX} \sim A$$

Achievements & further outlook

Core results

- ▶ Self-consistent theory of developed film having just passed plate edge
- ▶ Flow regimes of surprisingly rich physics identified
- ▶ Capillary ripples: nonlinear extension
- ▶ Choking: $T \sim 1/2$, $T \sim 1$
- ▶ Breakdowns by flow reversal or blow-up

To-dos

- ▶ Regularise: breakdowns, $T \sim 1$
- ▶ Unsteadiness & stability
- ▶ Symmetry-breaking effects in exit problem
- ▶ Careful experiment desirable!

Thank you for attention!