



# DIPLOMARBEIT

## Splitting-Verfahren für nichtlineare Evolutionsgleichungen

Ausgeführt am Institut für

Analysis und Scientific Computing  
der Technischen Universität Wien

unter der Anleitung von Prof. Winfried Auzinger

durch

Michael Quell

Döblergasse 4/12  
1070 WIEN

24.01.2018

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Unterschrift



# Abstract

This thesis motivates and summarizes the construction of splitting schemes for evolution equations. Further asymptotic correct local error estimators are proposed, to adapt the step-size in time propagation and reduce total computation time. Commutator free Magnus-type integrators are compared to splitting off the time variable. The Methods are tested by three applications: Models for solar cells, reaction-diffusion system by Gray-Scott and Schrödinger wave equations.

**Keywords:** Evolution equations, splitting methods, order conditions, local error estimators, commutator free Magnus integrators,

I declare by my signature that this assignment is my own work and that I have correctly acknowledged the work of others. This assignment is in accordance with University guidance on good academic conduct.

Vienna, January 24, 2018

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Michael Quell

# Acknowledgments

I wish to thank various people for their contribution to this thesis. First I would like to acknowledge the support provided by my family during the hard times of my study. I am particularly grateful for the assistance given by Dr. Benson Muite in the beginning. Special thanks should be given to Professor Winfried Auzinger, my research project supervisor for his professional guidance and valuable support and to Dr. Othmar Koch for his useful and constructive recommendations on this project. I would also like to thank Dr. Harald Hofstätter for his technical advice.

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# Chapter 1

## Introduction

In many fields in science researchers model systems over time. This leads to the class of differential equations called evolution equations. Often their problems are too complex to be linear, therefore the nonlinear case is studied too. The thesis starts in Chapter 2 with an motivation to use splitting methods on solving nonlinear evolution equations. Then is followed by a Chapter 3 about getting the order conditions and constructing splitting schemes. Explicit algorithms are not given, though they are referenced. The next Chapter 4 gives 4 different methods to estimate the local posterior error of the splitting schemes. The Chapter 5 analyzes a special kind of evolution equations, where the numerical results and numerical comparisons are then displayed in the next Chapter 6. Three types of evolution equations are discussed

- linear time dependent right hand side in Section 6.2,
- nonlinear parabolic equations in Section 6.3 and
- wave equations in Section 6.4.

In all the three cases it is investigated how well the splitting methods perform, especially in 6.2 they are compared to the Magnus-type integrators. It is also tried to answer the question if the computational time can be improved using adaptive step size selection algorithms based on an estimated local error. In the last Chapter 7 the underlying concept of the space discretization is explained in Section 6.3 and 6.4.

# Chapter 2

## Operator Splitting Methods

We consider evolution equations of the form

$$\partial_t u(t) = F(u(t)), \quad t \geq 0, \quad \text{and } u(0) \text{ given.} \quad (2.1)$$

In many cases splitting the right-hand side  $F(u)$  into two or more components leads to an easy way to achieve accurate and efficient results. [23] Let the right-hand side be

$$F(u) = A(u) + B(u) + (C(u) + \dots). \quad (2.2)$$

In many cases one can integrate all the sub-problems exactly, reducing the complexity and leading to simple and explicit numerical algorithms. A collection of splitting schemes. I would recommend and which was used here, is authored by W. Auzinger and O. Koch and can be found at

<http://www.asc.tuwien.ac.at/~winfried/splitting>

this will be referenced by [5]. This collection lists only schemes, where no assumptions were made on the operators, though for special cases one may find optimized schemes somewhere else. First we will discuss the case, when the right hand side is split only in to two components, as the notation is shorter and everything can easily be expanded to more terms. This results in an evolution equation (2.1) where the right-hand side is split into two operators,

$$\partial_t u(t) = F(u(t)) = A(u(t)) + B(u(t)), \quad t \geq 0. \quad (2.3)$$

A single step of a multiplicative splitting scheme, starting from  $u$ , having  $s$  stages and over a step of length  $h$ , is given by

$$\mathcal{S}(h, u) = \mathcal{S}_s(h, \mathcal{S}_{s-1}(h, \dots, \mathcal{S}_1(h, u))) \approx \mathcal{E}_F(h, u), \quad (2.4a)$$

with

$$\mathcal{S}_j(h, u) = \mathcal{E}_B(b_j h, \mathcal{E}_A(a_j h, u)), \quad (2.4b)$$



with appropriate coefficients  $a_j, b_j$ .  $\mathcal{E}_F$  denotes the exact flow associated with the given evolution equation (2.3). For the simplest case  $s = 1$  and  $a_1 = b_1 = 1$ , one can easily verify by Taylor expansion of the solution that this yields a scheme of order 1. The computational effort to achieve high accuracy is lower for higher order methods. There are generally two ways to create higher order schemes, either generating and solving a system of polynomial order conditions or by composition of lower order methods. The composition is not discussed here. For a scheme of order  $p$  the local error of a splitting step, which is denoted by

$$\mathcal{S}(h, u) - \mathcal{E}_F(h, u) =: \mathcal{L}(h, u) = \mathcal{O}(h^{p+1}), \quad (2.5)$$

is of order  $p + 1$  for  $h \rightarrow 0$ .

## Chapter 3

### Order Conditions

As stated in [3] it is sufficient, to assume a linear right hand side  $F$  to construct the order conditions ,

$$\frac{d}{dt}u(t) = Fu(t) = (A + B)u(t), \quad u(0) \text{ given.} \quad (3.1)$$

This gives for (2.4)

$$\mathcal{S}(h) = \mathcal{S}_s(h, \mathcal{S}_{s-1}(h, \dots, \mathcal{S}_1(h))) \approx \mathcal{E}_F(h) = e^{hF}, \quad (3.2)$$

with

$$\mathcal{S}_j(h) = e^{hB_j} e^{hA_j}, \quad A_j = a_j A, \quad B_j = b_j B, \quad j = 1, \dots, s. \quad (3.3)$$

In this case the local error (2.5) is of the form (2.5) with a linear operator  $\mathcal{L}(h)$ . The Taylor expansion of  $\mathcal{L}(h)u$  at  $h = 0$  up to order  $p + 1$  gives,

$$\mathcal{L}(h)u = \sum_{q=1}^{p+1} \frac{h^q}{q!} \frac{d^q}{dh^q} \mathcal{L}(0)u + \mathcal{O}(h^{p+2}). \quad (3.4)$$

If

$$0 = \frac{d}{dh} \mathcal{L}(0) = \frac{d^2}{dh^2} \mathcal{L}(0) = \dots = \frac{d^p}{dh^p} \mathcal{L}(0) \quad \Leftrightarrow \quad \mathcal{L}(h) = \mathcal{O}(h^{p+1}), \quad (3.5)$$

then the method is of order  $p$  and the leading local error term is given by

$$\frac{h^{p+1}}{(p+1)!} \frac{d^{p+1}}{dh^{p+1}} \mathcal{L}(0), \quad (3.6)$$

whereas

$$\frac{d^q}{dh^q} \mathcal{L}(0) = \sum_{|\mathbf{k}|=q} \binom{n}{\mathbf{k}} \cdot \prod_{j=1}^s \sum_{l=0}^{k_j} \binom{k_j}{l} B_j^l A_j^{k_j-l} - (A + B)^q, \quad (3.7)$$

with  $\mathbf{k} = (k_1, k_2, \dots, k_s) \in \mathbb{N}^s$  and  $|\mathbf{k}| = k_1 + k_2 + \dots + k_s$ . The righthandside of (3.7) can be written [9] as linear combination of higher order commutators of  $A$  and  $B$ . Consider the ring

$$\mathbb{C}\langle A, B \rangle \quad (3.8)$$

in the not commuting powerseries of  $A$  and  $B$  and with the Lie-bracket

$$[A, B] := AB - BA, \quad (3.9)$$

which will also sometimes be referred as commutator of  $A$  and  $B$ , gives an free Lie algebra. The representation in the Lyndon–Shirshov basis [3] of the free Lie algebra generated by  $A$  and  $B$  yield non-redundant order conditions. To compare to methods of the same order, one considers the leading error term (3.6) of the local error representation,

$$\frac{h^{p+1}}{(p+1)!} \frac{d^{p+1}}{dh^{p+1}} \mathcal{L}(0) = \sum_{k=1}^{l_{p+1}} \kappa_{p+1,k} K_{p+1,k}, \quad (3.10)$$

with  $l_{p+1}$  commutators  $K_{p+1,k}$  of order  $p+1$ , and computes

$$\left( \sum_{k=1}^{l_{p+1}} |\kappa_{p+1,k}|^2 \right)^{\frac{1}{2}}. \quad (3.11)$$

or, in fact easier to compute and local error measure (LEM)

$$LEM := \left( \sum_{k=1}^{l_{p+1}} |\lambda_{p+1,k}|^2 \right)^{\frac{1}{2}}. \quad (3.12)$$

The  $\lambda_{p+1,k}$  are the coefficients generated for the order condition for  $p+1$ . Because the LEM varies over several orders of magnitudes (3.11) and (3.12) are equally reasonable; See [9] for details.

### 3.0.1 Solving order conditions

The number of order conditions grows exponentially, with the number of stages. Higher order schemes found at [5] are numeric solutions to the order conditions and than refined with software floats and Newton method to full double precision. If the number of coefficients is larger than the number of equations the LEM (3.12) is minimized using state of the art solvers or plain Monte Carlo simulation, though the minimum given by the Monte Carlo search is not guaranteed to be the

global minimum. An alternative is to reduce the number of order condition by considering special symmetries. For example one considers symmetric schemes,

$$a_j = a_{s+1-j} \text{ and } b_j = b_{s-j}, \text{ with } b_s = 0, \quad (3.13)$$

which are a standard choice for long time integration. Another possibility is to exchange the roles of  $A$  and  $B$ , leading to reflected coefficients,

$$a_j = b_{s+1-j} \text{ and } b_j = a_{s+1-j}, \quad (3.14)$$

or so-called palindromic schemes.

# Chapter 4

## Local Error Estimators

In this chapter various asymptotically correct local error estimators will be proposed. The local error estimator is denoted by

$$\mathcal{P}(h, u) \approx \mathcal{L}(h, u), \quad (4.1)$$

which has the same order as the local error and  $\mathcal{P}(h, u) - \mathcal{L}(h, u) = \mathcal{O}(h^{p+2})$ . The estimate will be used to adapt the step size.

### 4.1 Defect based

In [4, 6, 7, 8], asymptotically correct local error estimators based on the defect which is defined by plugging the splitting operator  $\mathcal{S}$  into (2.1)

$$\mathcal{D}(h, u) = \frac{d}{dh} \mathcal{S}(h, u) - F \mathcal{S}(h, u), \quad (4.2)$$

have been constructed and analysed. This idea is based on the integral representation

$$\mathcal{L}(h, u) = \int_0^h \underbrace{\partial_2 \mathcal{E}_F(h - \tau, \mathcal{S}(\tau, u))}_{=: \ell(\tau)} \mathcal{D}(\tau, u) d\tau, \quad (4.3)$$

The notation for the Fréchet derivative of the flux  $\mathcal{E}_F(h, u)$  is,  $\partial_2 \mathcal{E}_F(h, u)$ . One can verify by repeating differentiation and evaluation for  $h = 0$  that for a scheme of order  $p \geq 1$  it is equivalent that

$$0 = \frac{d}{dh} \mathcal{L}(0, u) = \frac{d^2}{dh^2} \mathcal{L}(0, u) = \dots = \frac{d^p}{dh^p} \mathcal{L}(0, u) \quad (4.4)$$

$$\Leftrightarrow 0 = \mathcal{D}(0, u) = \frac{d}{dh} \mathcal{D}(0, u) = \dots = \frac{d^{p-1}}{dh^{p-1}} \mathcal{D}(0, u) \quad (4.5)$$

I.e. the validity of the  $p$ -th order conditions guarantees that the first  $p - 1$  derivatives of  $\mathcal{D}$  vanish at  $t = 0$ . By Taylor expansion of (4.3) and ignoring higher order terms ,

$$\mathcal{L}(h, u) = \int_0^h l(\tau) d\tau \approx \int_0^h \frac{\tau^p}{p!} \ell^{(p)}(0) d\tau = \frac{\tau^{p+1}}{(p+1)!} \ell^{(p)}(0). \quad (4.6)$$

The notation  $\approx$  stands for asymptotic equivalence. Reversing the Taylor expansion gives,

$$\frac{\tau^{p+1}}{(p+1)!} \ell^{(p)}(0) \approx \frac{h}{p+1} \ell(h) = \frac{h}{p+1} \mathcal{D}(h, u). \quad (4.7)$$

This leads to a local error estimator involving a single evaluation of the defect,

$$\mathcal{P}(h, u) = \frac{h}{p+1} \mathcal{D}(h, u) \approx \mathcal{L}(h, u). \quad (4.8)$$

This algorithm works generally for splittings of any order into an arbitrary number of operators if Fréchet derivatives of the subflows are available, see [3].

### 4.1.1 Efficient evaluation of the defect

The defect can be computed simultaneously with the the update of the solution  $u$ . Considering a scheme  $\mathcal{S}$  with  $s$  stages and let  $d = \mathcal{D}(h, u)$ . Hence algorithms for splitting in 2 , 3 and  $n$  operators are given, which can be easily deduced from [8]. Splitting into two operators gives equation (2.3). The sub flows of the operators are given by  $\mathcal{E}_A$  and  $\mathcal{E}_B$ .

```

d = 0
for k = 1 : s
    d = d + a_k A(u)
    d = \partial_2 \mathcal{E}_A(a_k h, u) \cdot d
    u = \mathcal{E}_A(a_k h, u)
    d = \partial_2 \mathcal{E}_B(b_k h, u) \cdot d
    u = \mathcal{E}_B(b_k h, u)
d = d + \begin{cases} b_k B(u), & k < s \\ (b_k - 1) B(u), & k = s \end{cases}
end
d = d - A(u)

```

In case of splitting (2.1) into three operators,

$$\partial_t u(t) = F(u(t)) = A(u(t)) + B(u(t)) + C(u(t)), \quad t \geq 0. \quad (4.9)$$

The coefficients of splitting scheme are named  $a_j, b_j$  and  $c_j$  with respect to the name of their operator.

```

d = 0
for k = 1 : s
    d = d + a_k A(u)
    d = ∂2ℰA(a_k h, u) · d
    u = ℰA(a_k h, u)
    d = d + b_k B(u)
    d = ∂2ℰB(b_k h, u) · d
    u = ℰB(b_k h, u)
    d = ∂2ℰC(c_k h, u) · d
    u = ℰC(c_k h, u)
    d = d + { c_k C(u),      k < s
              (c_k - 1)C(u), k = s
    end
d = d - A(u) - B(u)

```

The general case using  $n$  operators (2.1) yields,

$$\partial_t u(t) = F(u(t)) = A_1(u(t)) + A_2(u(t)) + \cdots + A_n(u(t)), \quad t \geq 0. \quad (4.10)$$

One may already guessed the algorithm, but here it is anyway

```

d = 0
for k = 1 : s
    for j = 1 : n - 1
        d = d + a_{jk} A_j(u)
        d = ∂2ℰA_j(a_{jk} h, u) · d
        u = ℰA_j(a_{jk} h, u)
    end
    d = ∂2ℰA_n(a_{nk} h, u) · d
    u = ℰA_n(a_{nk} h, u)
    d = d + { a_{nk} A_n(u),      k < s
              (a_{nk} - 1)A_n(u), k = s
    end
d = d - ∑_{j=1}^{n-1} A_j(u)

```

## 4.2 Embedded formulae

Consider a pair of two schemes with orders  $p$ , and  $p + 1$ . The scheme  $\mathcal{S}$  of order  $p$  is called the worker, which propagates the solution in time and the scheme  $\hat{\mathcal{S}}$  of order  $p + 1$  is the controller. An estimate for the local error is given by the distance between the solutions of the different schemes.

$$\mathcal{P}(h, u) = \mathcal{S}(h, u) - \hat{\mathcal{S}}(h, u) \approx \mathcal{L}(h, u) \quad (4.11)$$

For computational efficiency it is desired that most parts of the computation from the worker can be reused for the controller. To setup those pairs choose first an efficient controller of order  $p + 1$  and  $\hat{s}$  stages. Denote the coefficients of the controller  $\hat{\mathcal{S}}$  as  $\hat{a}_1, \hat{a}_2, \dots, \hat{a}_{\hat{s}}$  and  $\hat{b}_1, \hat{b}_2, \dots, \hat{b}_{\hat{s}}$ . The worker is only a scheme of order  $p$  and therefore does not need to fulfill as many order conditions. This makes it possible to choose the worker  $\mathcal{S}$  to have  $s \leq \hat{s}$  stages and coefficients  $a_1, a_2, \dots, a_s$  and  $b_1, b_2, \dots, b_s$  where  $a_i = \hat{a}_i$  and  $b_i = \hat{b}_i$  for the first  $k$  coefficients of the scheme. In [9], it is described how to choose a 'good'  $\mathcal{S}$  from a set of possible candidates.

## 4.3 Palindromic schemes

The local error estimator is based on the adjoint scheme  $\mathcal{S}^*$  of  $\mathcal{S}$  which is satisfies,

$$\mathcal{S}^*(h, u) = \mathcal{S}^{-1}(-h, u). \quad (4.12)$$

The leading error term of  $\mathcal{S}$  and its adjoint  $\mathcal{S}^*$  are identical up to the factor  $(-1)^p$  see [9] and [14],

$$\mathcal{L}(h, u) = C(u) h^{p+1} + \mathcal{O}(h^{p+2}), \quad (4.13)$$

$$\mathcal{L}^*(h, u) = (-1)^p C(u) h^{p+1} + \mathcal{O}(h^{p+2}), \quad (4.14)$$

If  $p$  is odd, the averaged scheme

$$\overline{\mathcal{S}}(h, u) = \frac{1}{2}(\mathcal{S}(h, u) + \mathcal{S}^*(h, u)), \quad (4.15)$$

is of order  $p + 1$ . The local error estimator is, defined in the same way as for an embedded pair

$$\mathcal{P}(h, u) = \mathcal{S}(h, u) - \overline{\mathcal{S}}(h, u) = \frac{1}{2}(\mathcal{S}(h, u) - \mathcal{S}^*(h, u)). \quad (4.16)$$



*Palindromic* schemes, or ‘reflected schemes’ first proposed in [9] in the terminology of [3], are characterized by  $b_j = a_{s+1-j}$ ,  $j = 1, \dots, s$ , i.e.,

$$\begin{aligned} & (a_1, b_1, a_2, b_2, \dots, a_{s-1}, b_{s-1}, a_s, b_s) \\ &= (a_1, a_s, a_2, a_{s-1}, \dots, a_{s-1}, a_2, a_s, a_1). \end{aligned} \quad (4.17)$$

Assume a scheme of order  $p$  is given, and consider a single splitting step of the form (2.4). Swapping the roles of  $A$  and  $B$ , i.e., replacing (2.4) by

$$\hat{\mathcal{S}}(h, u) = \hat{\mathcal{S}}_s(h, \hat{\mathcal{S}}_{s-1}(h, \dots, \hat{\mathcal{S}}_1(h, u))), \quad (4.18a)$$

with

$$\hat{\mathcal{S}}_j(h, v) = \mathcal{E}_A(b_j h, \mathcal{E}_B(a_j h, v)), \quad (4.18b)$$

also results in a scheme of order  $p$ , because no special information about the nature of  $A$  or  $B$  enters the order conditions. If  $\mathcal{S}$  is palindromic then

$$\mathcal{S}(-h, \hat{\mathcal{S}}(h, u)) = u, \quad \text{which gives} \quad \hat{\mathcal{S}}(h, u) = \mathcal{S}^*(h, u). \quad (4.19)$$

The computational costs for the local error estimator are the same as for the basic integrator. Palindromic schemes are not only interesting because, as stated in 3.0.1 the number of order condition is lower, but also because [9] discovered that they tend to have minimal LEMs among sets of equally costly schemes. The reason for this is not know, but would be interesting for further investigations.

## 4.4 MilneDevice

Consider two schemes  $(\mathcal{S}, \hat{\mathcal{S}})$  [9], with the same order  $p$  and  $s$  stages. Now let the local errors  $\mathcal{L}, \hat{\mathcal{L}}$  be related via

$$\mathcal{L}(h, u) = C(u)h^{p+1} + \mathcal{O}(h^{p+2}) \quad (4.20a)$$

$$\hat{\mathcal{L}}(h, u) = \gamma C(u)h^{p+1} + \mathcal{O}(h^{p+2}) \quad (4.20b)$$

with  $\gamma \neq 1$ . The additive scheme

$$\overline{\mathcal{S}}(h, u) = -\frac{\gamma}{1-\gamma} \mathcal{S}(h, u) + \frac{1}{1-\gamma} \hat{\mathcal{S}}(h, u) \quad (4.21)$$

is of order  $p+1$ , and a local error estimator is given by

$$\mathcal{P}(h, u) = \mathcal{L}(h, u) - \overline{\mathcal{L}}(h, u) = -\frac{1}{1-\gamma} (\mathcal{L}(h, u) - \hat{\mathcal{L}}(h, u)). \quad (4.22)$$

This is more general than Section 4.3, on the other hand, the construction works in practice only for lower-order schemes, because (4.20b), (4.20b) is a rather restrictive requirement, which corresponds to  $\gamma = -1$

## 4.5 Time-adaptive strategies

After estimating the local error (4.1)  $\mathcal{P}(h, u)$ , it is used to choose the step size  $h$ . Given a local error tolerance TOL, one may want to maximize step size  $h$ . The following formula is used to estimate the optimal step size for the next step (see [15, 22]).

$$h = h_0 \min \left\{ \alpha_{\max}, \max \left\{ \alpha_{\min}, \alpha \left( \frac{\text{TOL}}{\mathcal{P}(h_0, u)} \right)^{\frac{1}{p+1}} \right\} \right\} \quad (4.23)$$

The notation  $h_0$  is used for the step size currently used. The parameters  $\alpha_{\min}$  and  $\alpha_{\max}$  limit the change rate of the step size,  $\alpha$  is a safety factor to reduce overestimating the step size due to numerical errors. If the estimated error is larger than the given tolerance the step is rejected and a new guess is made with the previously estimated error. In the test the parameters were chosen as,

$$\alpha = 0.9, \quad \alpha_{\min} = 0.25, \quad \alpha_{\max} = 4.0. \quad (4.24)$$

More advanced algorithms, e.g. combining the last two step sizes ( $h_0, h_{-1}$ ) and estimated errors (4.25) to predict the step size have been investigated but did not show a significant change in efficiency or number of rejected steps.

$$h = h_0 \min \left\{ \alpha_{\max}, \max \left\{ \alpha_{\min}, \alpha \left( \frac{\text{TOL}}{\mathcal{P}(h_0, u)} \right)^{\frac{\beta_1}{p+1}} \left( \frac{\text{TOL}}{\mathcal{P}(h_{-1}, u)} \right)^{\frac{\beta_2}{p+1}} \left( \frac{h_0}{h_{-1}} \right)^{-\alpha_1} \right\} \right\} \quad (4.25)$$

with

$$\alpha = 1.0, \quad \alpha_{\min} = 0.25, \quad \alpha_{\max} = 4.0 \quad \text{and} \quad \alpha_1 = \beta_1 = \beta_2 = 0.25. \quad (4.26)$$

# Chapter 5

## Commutator free exponential Time propagators / Magnus

For a non-autonomous linear system of differential equations

$$\frac{d}{dt}u(t) = A(t)u(t), \quad t \in [t_0, t_{end}], \quad u(t_0) = u_0 \text{ given}, \quad (5.1)$$

the formal representation of the solution is given by the Magnus expansion [14],

$$u(t_n + \tau_n) = e^{\Omega(t_n + \tau_n)}u(t_n), \quad t_n, t_n + \tau_n \in [t_0, t_{end}] \quad (5.2)$$

$$\begin{aligned} \Omega(t_n + \tau_n) = & \int_{t_n}^{t_n + \tau_n} A(\sigma) d\sigma + \frac{1}{2} \int_{t_n}^{t_n + \tau_n} \int_{t_n}^{\sigma_1} [A(\sigma_1), A(\sigma_2)] d\sigma_2 d\sigma_1 + \\ & \frac{1}{6} \int_{t_n}^{t_n + \tau_n} \int_{t_n}^{\sigma_1} \int_{t_n}^{\sigma_2} [[A(\sigma_1), A(\sigma_2)], A(\sigma_3)] + [A(\sigma_1), [A(\sigma_2), A(\sigma_3)]] d\sigma_3 d\sigma_2 d\sigma_1 + \dots \end{aligned} \quad (5.3)$$

This has been extensively studied in the literature.

### 5.1 Magnus-type integrators

Truncation of the infinite sum (5.3) and suitable quadrature of the integrals gives the class of Magnus-type integrators,

$$e^{\Omega(t_n + \tau_n)} \approx e^{\Omega_n}. \quad (5.4)$$

**Second-order Magnus-type integrator (exponential midpoint scheme)**

$$\Omega_n \approx \tau_n A\left(t_n + \frac{\tau_n}{2}\right) \quad (5.5)$$

### Fourth-order Magnus-type integrator

$$\Omega_n \approx \frac{1}{6} \tau_n \left( A(\tau_n) + 4A\left(t_n + \frac{\tau_n}{2}\right) + A(t_n + \tau_n) \right) - \frac{1}{12} \tau_n^2 [A(t_n), A(t_n + \tau_n)] \quad (5.6)$$

For higher order one gets nasty commutators expressions which may alter the structure of the matrix. This leads to the following alternative approach.

## 5.2 Commutator free Magnus integrators

To avoid the computational costs of the commutators, commutator free exponential time integrators were proposed [1, 2]. They are constructed as compositions of matrix exponentials of linear combinations of  $A$  evaluated at certain times. The scheme is characterized by the order  $p$ , the number of evaluation points (nodes)  $K$  of  $A$  and the number of matrix exponentials  $J$ . Therefore we have the vector

$$c = \begin{pmatrix} c_1 \\ \vdots \\ c_K \end{pmatrix} \in \mathbb{R}^K \text{ of evaluation points and the matrix } a = \begin{pmatrix} a_{11} & \dots & a_{1K} \\ \vdots & \ddots & \vdots \\ a_{J1} & \dots & a_{JK} \end{pmatrix} \in \mathbb{R}^{J \times K}$$

with the corresponding coefficients.

One step with Magnus form  $u_n \approx u(t_n)$  to  $u_{n+1}$  with stepsize  $\tau_n$

$$\begin{aligned} u_{n+1} &= \mathcal{S}_{t_n}(\tau) u_n \\ \mathcal{S}_{t_n}(\tau) &= e^{\Omega_n} = e^{\tau B_J(t_n, \tau)} \dots e^{\tau B_1(t_n, \tau)} \\ B_j(t_n, \tau) &= a_{j1} A(t_n + c_1 \tau) + \dots + a_{jK} A(t_n + c_K \tau), \quad j \in \{1, \dots, J\} \end{aligned}$$

From now on assume  $t_n = 0$ , to shorten the notation.

### 5.2.1 Local error and defect. Order conditions and defect based local error estimate

The main idea is the same as for splitting, see also (2.5) for the local error, (4.2) for the defect and (4.8) for the local error estimator. The local error and defect are now defined by,

$$\mathcal{L}(\tau) = \mathcal{S}(\tau) - \mathcal{E}(\tau), \quad (5.7)$$

$$\mathcal{D}(\tau) = \frac{d}{d\tau} \mathcal{S}(\tau) - A(t_0 + \tau) \mathcal{S}(\tau), \quad (5.8)$$

with the exact flow  $\mathcal{E}$  associated with the given equation (5.1). The local error satisfies

$$\frac{d}{d\tau} \mathcal{L}(\tau) = A(\tau) \mathcal{L}(\tau) + \mathcal{D}(\tau), \quad (5.9)$$

and

$$\mathcal{L}(\tau) = \int_0^\tau \Pi(\tau, \sigma) \mathcal{D}(\sigma) d\sigma, \quad \text{with} \quad \Pi(\tau, \sigma) = \mathcal{E}(\tau) \mathcal{E}(-\sigma). \quad (5.10)$$

A scheme of order  $p$  is characterized by the property as stated before in (3.5)  $\mathcal{L}(\tau) = \mathcal{O}(\tau^{p+1})$ , or equivalently  $\mathcal{L}(0) = 0$  and

$$\frac{d^q}{d\tau^q} \mathcal{L}(\tau) \Big|_{\tau=0} = 0, \quad q = 1, \dots, p. \quad (5.11a)$$

Since from (3.7) and (5.8) we inductively obtain

$$\frac{d^q}{d\tau^q} \mathcal{L}(\tau) = \sum_{k=0}^{q-1} \binom{q-1}{k} \frac{d^{q-1-k}}{d\tau^{q-1-k}} A(\tau) \frac{d^k}{d\tau^k} \mathcal{L}^{(k)}(\tau) + \frac{d^{q-1}}{d\tau^{q-1}} \mathcal{D}(\tau),$$

and as for the splitting case order conditions (5.11a) are equivalent to

$$\frac{d^{q-1}}{d\tau^{q-1}} \mathcal{D}(\tau) \Big|_{\tau=0} = 0, \quad q = 1, \dots, p, \quad (5.11b)$$

and a scheme of order  $p$  is characterized by

$$\mathcal{D}(\tau) = \mathcal{O}(\tau^p). \quad (5.11c)$$

To compute the defect (5.8) for this step one must be able to evaluate

$$\frac{d}{d\tau} \mathcal{S}(\tau) = \left( \frac{d}{d\tau} e^{\tau B_j(\tau)} \right) e^{\tau B_{j-1}(\tau)} \dots e^{\tau B_1(\tau)} + \dots + \quad (5.12)$$

$$+ e^{\tau B_j(\tau)} \dots e^{\tau B_2(\tau)} \left( \frac{d}{d\tau} e^{\tau B_1(\tau)} \right) \quad (5.13)$$

$$\frac{d}{d\tau} e^{\tau B_j(\tau)} = \sum_{m=0}^{\infty} \frac{1}{(m+1)!} ad_{\Omega_j(\tau)}^m (\Omega'_j(\tau)) e^{\tau B_j(\tau)}. \quad (5.14)$$

with the notation

$$\Omega_j(\tau) = \tau B_j(\tau),$$

$$\Omega'_j(\tau) = B_j(\tau) + \tau B'_j(\tau),$$

$$B'_j(\tau) = a_{j1} c_1 A'(c_1 \tau) + \dots + a_{jK} c_K A'(c_K \tau),$$

$$ad_{\Omega}^j(X) = [\Omega, ad_{\Omega}^{j-1}(X)], \quad j \geq 1, \quad (5.15)$$

$$ad_{\Omega}^0(X) = X. \quad (5.16)$$

It is not possible to compute the infinite sum (5.14), since we only consider a method of order  $p$ , the sum is truncated,

$$\frac{d}{d\tau} e^{\tau B_1(\tau)} \approx \sum_{m=0}^{p-1} \frac{1}{(m+1)!} ad_{\Omega_1(\tau)}^m (\Omega'_1(\tau)) e^{\tau B_1(\tau)}. \quad (5.17)$$

## 5.2.2 Efficient evaluation of the defect

For commutator free Magnus integrators it is also possible to evaluate the defect parallel to the propagation of the basic solution see 4.1.1 for the splitting case. The notation stays the same,  $d = \mathcal{D}(\tau)$ . The main computational effort is the evaluation of the matrix exponentials in (5.20) and (5.21).

$$\text{for } j = 1 : J$$

$$B = \sum_{k=1}^K a_{j,k} A(c_k \tau) \quad (5.18)$$

$$B_t = \sum_{k=1}^K c_k a_{j,k} A_t(c_k \tau) \quad (5.19)$$

$$u = e^{\tau B} u \quad (5.20)$$

$$d = \begin{cases} \sum_{m=1}^{p-1} \frac{1}{(m+1)!} \text{ad}_{\tau B}^m (B + \tau B_t) u, & j = 1 \\ d + e^{\tau B} d + \sum_{m=1}^{p-1} \frac{1}{(m+1)!} \text{ad}_{\tau B}^m (B + \tau B_t) u, & j > 1 \end{cases} \quad (5.21)$$

**end**

$$d = d - A(\tau) u \quad (5.22)$$

Define  $A_t := \frac{d}{dt} A(t)$ . The sum over the commutators (5.15) in the update of the defect is implemented using only matrix vector multiplications. There might be some potential to optimize it, since commutators may be bad for numeric evaluation.

## 5.3 Splitting off the time variable “freezing”

To remove the time dependence of the system matrix  $A(t)$  from (5.1), one can also use a splitting approach. A new variable  $v$  is introduced, which will represent time and giving the autonomous system,

$$\frac{d}{dt} u(t) = A(v) u(t), \quad (5.23a)$$

$$\frac{d}{dt} v(t) = 1, \quad (5.23b)$$

or equivalently,

$$\frac{d}{dt} \begin{pmatrix} u(t) \\ v(t) \end{pmatrix} = \underbrace{\begin{pmatrix} A(v) & 0 \\ 0 & 0 \end{pmatrix}}_{\mathcal{B}} \begin{pmatrix} u(t) \\ v(t) \end{pmatrix} + \underbrace{\begin{pmatrix} 0 \\ 1 \end{pmatrix}}_{\mathcal{A}}, \quad (5.24)$$

with initial condition  $(u_0, t_0)^T$ ). The splitting operators in this section will be written as  $\mathcal{A}, \mathcal{B}$  as  $A$  is already used for the system matrix. Splitting the right hand side in  $\mathcal{A}(u, v) = (0, 1)^T$  and  $\mathcal{B}(u, v) = (A(v)u, 0)^T$  simplifies the computation, because now the matrix for the exponential is time independent. For this kind of splitting where one of the operators is simple like  $\mathcal{A}$  it might be interesting to find optimized schemes, which exploit the special structure of  $\mathcal{A}$ .

Every splitting scheme with  $s$  stages applied to (5.1), may also be interpreted as a commutator free Magnus integrator (CFMI) from Section 5.2 with  $s = K = J$  and

$$c = \left( a_1, a_1 + a_2, \dots, \sum_{i=0}^s a_i \right)^T \text{ and } a = \text{diag}(b_1, \dots, b_s). \quad (5.25)$$

As an example for the splitting scheme Strang  $p = s = 2$  with coefficients  $a_1 = a_2 = \frac{1}{2}$  and  $b_1 = 1, b_2 = 0$  (5.25) yields

$$c = \left( \frac{1}{2}, 1 \right)^T \text{ and } a = \text{diag}(1, 0). \quad (5.26)$$

This simplifies to  $c = (\frac{1}{2})$  and  $a = (1)$ , which is the same as exponential midpoint rule in (5.5) further named Magnus2. To proof that one can always interpret a CFMI as a splitting scheme may be more difficult. This is an interesting question for further investigations.

### 5.3.1 Solution

We note the initial value of  $(u, v)^T = (u_0, v_0)^T$ . For operator  $\mathcal{A}$  the exact solution is

$$\begin{pmatrix} u(t) \\ v(t) \end{pmatrix} = \begin{pmatrix} u_0 \\ v_0 + t \end{pmatrix}, \quad (5.27)$$

therefore for the evaluation of the defect based error estimator from Section 4.1 one needs,

$$\partial_2 \mathcal{E}_{\mathcal{A}} \left( t, \begin{pmatrix} u \\ v \end{pmatrix} \right) = Id. \quad (5.28)$$

For operator  $\mathcal{B}$  the solution is

$$\begin{pmatrix} u(t) \\ v(t) \end{pmatrix} = \exp \left( t \begin{pmatrix} A(v) & 0 \\ 0 & 0 \end{pmatrix} \right) \begin{pmatrix} u_0 \\ v_0 \end{pmatrix} = \begin{pmatrix} \exp(tA(v))u_0 \\ v_0 \end{pmatrix}, \quad (5.29)$$

and for the defect based error estimator

$$\partial_2 \mathcal{E}_{\mathcal{B}} \left( t, \begin{pmatrix} u \\ v \end{pmatrix} \right) = \begin{pmatrix} \exp(tA(v)) & \frac{\partial}{\partial v} \exp(tA(v))u \\ 0 & 1 \end{pmatrix}, \quad (5.30)$$

with differential of the matrix exponential

$$\frac{\partial}{\partial v} \exp(tA(v))u = \sum_{m=0}^{\infty} \frac{1}{(m+1)!} \text{ad}_{tA(v)}^m \left( t \frac{\partial}{\partial v} A(v) \right) \exp(tA(v))u. \quad (5.31)$$

The infinite sum will be approximated as in (5.17) by a partial sum up to  $m = p - 1$  if  $p$  is the order of the scheme.



# Chapter 6

## Examples and Results

### 6.1 Methods used

#### 6.1.1 Magnus

The Magnus schemes are named Magnus where as the first number afterwards gives the order of the scheme. Magnus2 Magnus4 are schemes with the minimal number of matrix exponentials for their order. For the Magnus4Optimized scheme, the local error constant is smaller at cost of an additional matrix exponential, The coefficients for this three are taken from [2]. The two sixth order schemes Magnus6\_4 and Magnus6\_6 which were also considered, are taken from [1]. The number of matrix exponentials can be found in Table 6.3.

#### 6.1.2 Splitting

The splitting schemes used in the comparisons are all from [5] as mentioned earlier in Section 2. Embedded splitting pairs of order  $p$  are named with the pattern “EMB  $p+1/p$  . . . ”. Similar Palindromic schemes are named in the manner of “PP  $p/p+1$  . . . ” and Milne pairs have some where the string “milne ” inside the name. If the coefficients are complex “ c ” will be the last character in the name. The additional tag “ D ” is added when the defect based error estimator from Section 4.1 is used with the splitting scheme.

#### 6.1.3 Hardware

The computations were done on a PC running Ubuntu 16.04 with an Intel(R) Core(TM) i7-2600 CPU @3.4 GHz (4 cores) and 16 GB ram. The Julia language is still in development, the provided code was written in Julia version v0.5 .

## 6.2 Solar cells: Application of splitting and Magnus-type integrators

Modeling oxide solar cells physicist get a time-dependent Hermitian matrix

$$H: \mathbb{R} \rightarrow \mathbb{C}^{d \times d} \quad (6.1)$$

to describe the movement and interaction of electrons within a Hubbard-type model in solid state physics. The explicit time-dependency originates from an external electric field associated with a photon. The matrix  $H$  is Hermitian, though formulating the equation like 5.1 we get

$$\frac{d}{dt}u(t) = A(t)u(t) = -iH(t)u(t), \quad t \in [t_0, t_{end}], \quad u(t_0) = u_0 \text{ given}, \quad (6.2)$$

with  $A(t)$  is anti-Hermitian, which means  $a_{ij} = -\overline{a_{ji}}$ .

Section 6.2.3 discusses the simple case with 2 electrons, and Section 6.2.4 the more complex case with 8 electrons in a line.

### 6.2.1 Implementation

The implementation is done in Julia [11] a high-level, high-performance dynamic programming language for technical computing. In Julia you are able to call Python and C code directly, which enables you to access lots of software libraries directly. The code is setup in such a way that one can easily change the scheme. The main computational effort lies in the evaluation of the matrix exponentials.

### 6.2.2 Matrix exponential

The system Matrix in 6.2.3 has only dimension 4, for which the native implementation in Julia is used. In the physically interesting cases, the system matrix  $A(t)$  is a large sparse matrix. The system in 6.2.4 roughly about 0.2% of the  $4900^2$  elements are non zero. Expokit [24] is used to compute the matrix exponential. Expokit evaluates  $e^{tA}u$  without computing the exponential itself. Expokit is written in FORTRAN, that means a wrapper for the code is needed. H. Hofstätter provided the interface to call Expokit directly from Julia. We choose Expokit over the native implementation, because its enormous performance increase for sparse matrices of about 5700 compared to the native implementation of `expm` in Julia, see Table 6.2. This allows to complete the computations in an adequate time. Also in the full case the performance increase is significant as Table 6.1 reports. In those Tables "time" means the time to compute the matrix exponential of either a random matrix in  $\mathbb{C}^{4900 \times 4900}$  or (6.6) and apply it to a vector in  $\mathbb{C}^{4900}$  measured in

seconds. "err" is the  $L_2$  norm of the difference between initial data and computing one step forward and backward with step size  $h = 0.1$ . The native implementation in Julia relies on the scaling and squaring algorithm from [16] to compute first the exponential and then uses a matrix vector multiplication.

	time	error
Julia's expm	95.965	1.711e-15
Expokit	1.022	2.984e-08

Table 6.1: full matrix ( $n = 4900$ )

	time	error
Julia's expm	130.001	2.002e-15
Expokit	0.022	2.184e-09

Table 6.2: sparse matrix ( $n = 4900$ )

From Tables 6.1 and Table 6.2 one can easily see the major disadvantage of Expokit, it is that it can only guarantee accuracy of  $\sqrt{\epsilon ps}$ , where  $\epsilon ps \approx 1e - 16$  is the machine epsilon. This demands further investigations to improve this.

As stated before in 6.2.1 the main computational effort goes into the computation of the matrix exponentials. That means for the splitting schemes  $A$  and  $B$  are chosen that the number of matrix exponentials is minimal. Following Table 6.3 shows how many times the matrix exponential has to be computed per step. The Magnus schemes are from [1, 2] and the others from [5]. The error estimator for Magnus schemes is always the defect based one, which generally takes  $2s - 1$  evaluations. One may determine that for embedded schemes the additional evaluations for the error estimator are smaller than for the defect based ones.

### 6.2.3 Results (2 electrons)

In this simple case, for 2 electrons and 2 states the Hamiltonian  $H \in \mathbb{C}^{4 \times 4}$  reads,

$$H(t) = \begin{pmatrix} v_{11} + v_{22} & -v_{12}(t) & -v_{21}(t) & 0 \\ -v_{12}(t)^* & 2v_{11} + U & 0 & v_{21}(t) \\ -v_{21}(t)^* & 0 & 2v_{22} + U & v_{12}(t) \\ 0 & v_{21}(t)^* & v_{12}(t)^* & v_{11} + v_{22} \end{pmatrix} * \dots \text{complex conjungate.}$$

Method	# matrix exponentials without errorestimator	# matrix exponentials with errorestimator
Magnus2	1	1
Magnus4	2	3
Magnus4Optimized	3	5
Magnus6_4	4	7
Magnus6_6	6	11
BM 11-6 PRK D	10	19
A 10-6 D	9	17
Symm-Milne-32	2	4
EMB 4/3 AK p	5	8
EMB 4/3 M/AK	5	7
EMB 5/4 AK (ii)	8	11
EMB 4/3 AK s	5	7
PP 3/4 A	3	6
PP 5/6 A	8	16

Table 6.3: Number of matrix exponential computed per step.

The initial condition is chosen  $u_0 = (1, 0, 0, 0)^T$  and the other parameters are given by,

$$v_{11} = 0, \quad v_{22} = 1, \quad v_{12}(t) = e^{i\omega(t)}, \quad v_{21}(t) = e^{-i\omega(t)}, \quad (6.3a)$$

$$\omega(t) = \frac{1}{10} e^{-\frac{1}{6}(t-6)^2} \cos\left(\frac{7\pi}{4}(t-6)\right) \quad \text{and } U = 3. \quad (6.3b)$$

The interesting time for this simulation is between  $t_0 = 0.0$  and  $t_{end} = 8.0$ .

### Reference solution

Starting with a step size of  $t_0 - t_{end}$  the step size is halved every iteration, as long as the distance between the solution at  $t_{end}$  and the one computed with the previous step size is decreasing. For this purpose PP 3/4 A was used. It took 15 refinements to the final step size,  $2.441e - 04$  with the minimal distance of  $1.735e - 12$  to the previously computed one. Also the values of the solution at  $t_0 + (t_{end} - t_0) \cdot 2^{-i}, i \in 1, 2, \dots, 15$  are computed to be used as a reference solution for estimating the local error and its orders. The following tables show the results.

## Tables

First we present some tables to show general, that the schemes have the predicted order. Then second order methods are compared to determine their efficiency and later on 4-th order methods are compared.

- Tables 6.4 and 6.5 show the global error at the end of the integration interval. The used step size is in the column  $h$ ,  $err$  is the  $L_2$  norm of the error and  $p$  is the experimental order, which is computed by the logarithm of the quotient from the error of two consecutive step sizes.

	$h$	$err$	$p$
1	$8.000e+00$	$1.030e-01$	
2	$4.000e+00$	$1.328e-01$	-0.37
3	$2.000e+00$	$1.179e-01$	0.17
4	$1.000e+00$	$8.571e-02$	0.46
5	$5.000e-01$	$3.764e-02$	1.19
6	$2.500e-01$	$8.160e-03$	2.21
7	$1.250e-01$	$2.065e-03$	1.98
8	$6.250e-02$	$5.180e-04$	2.00
9	$3.125e-02$	$1.296e-04$	2.00
10	$1.563e-02$	$3.241e-05$	2.00
11	$7.813e-03$	$8.103e-06$	2.00
12	$3.906e-03$	$2.026e-06$	2.00
13	$1.953e-03$	$5.064e-07$	2.00
14	$9.766e-04$	$1.266e-07$	2.00
15	$4.883e-04$	$3.165e-08$	2.00
16	$2.441e-04$	$7.914e-09$	2.00

Table 6.4: Global Error at  $t = 8.0$ ; Magnus2

	h	err	p
1	$8.000e+00$	$9.939e-02$	
2	$4.000e+00$	$1.209e-01$	-0.28
3	$2.000e+00$	$1.043e-01$	0.21
4	$1.000e+00$	$4.252e-02$	1.29
5	$5.000e-01$	$7.685e-03$	2.47
6	$2.500e-01$	$2.362e-03$	1.70
7	$1.250e-01$	$5.951e-04$	1.99
8	$6.250e-02$	$1.490e-04$	2.00
9	$3.125e-02$	$3.728e-05$	2.00
10	$1.563e-02$	$9.320e-06$	2.00
11	$7.813e-03$	$2.330e-06$	2.00
12	$3.906e-03$	$5.825e-07$	2.00
13	$1.953e-03$	$1.456e-07$	2.00
14	$9.766e-04$	$3.641e-08$	2.00
15	$4.883e-04$	$9.103e-09$	2.00
16	$2.441e-04$	$2.277e-09$	2.00

Table 6.5: Global Error at  $t = 8.0$ ; Symm-Milne-32

- In Table 6.6 the properties of the local error can be seen. Column err1 shows the local error in  $L_2$  norm and err2 the error of the defect based error estimator also in the  $L_2$  norm, which is the same as the error of the by the error estimator corrected solution. The orders are the ones one would expect for Strang  $p = 2, p + 1$  and  $p + 2$ .

	h	err1	p1	err2	p2
1	$8.000e+00$	$1.030e-01$		$5.653e+01$	
2	$4.000e+00$	$2.357e-02$	2.13	$2.407e-01$	7.88
3	$2.000e+00$	$2.372e-03$	3.31	$1.601e-02$	3.91
4	$1.000e+00$	$4.896e-04$	2.28	$1.313e-03$	3.61
5	$5.000e-01$	$6.205e-05$	2.98	$8.883e-05$	3.89
6	$2.500e-01$	$9.476e-06$	2.71	$7.760e-06$	3.52
7	$1.250e-01$	$1.202e-06$	2.98	$4.605e-07$	4.07
8	$6.250e-02$	$1.495e-07$	3.01	$2.654e-08$	4.12
9	$3.125e-02$	$1.856e-08$	3.01	$1.572e-09$	4.08
10	$1.563e-02$	$2.307e-09$	3.01	$9.534e-11$	4.04
11	$7.813e-03$	$2.875e-10$	3.00	$5.865e-12$	4.02
12	$3.906e-03$	$3.588e-11$	3.00	$3.636e-13$	4.01
13	$1.953e-03$	$4.481e-12$	3.00	$2.273e-14$	4.00
14	$9.766e-04$	$5.599e-13$	3.00	$1.516e-15$	3.91
15	$4.883e-04$	$6.998e-14$	3.00	$1.415e-16$	3.42
16	$2.441e-04$	$8.749e-15$	3.00	$2.221e-16$	-0.65
17	$1.221e-04$	$1.099e-15$	2.99	$1.110e-16$	1.00

Table 6.6: Local error and error of the defect based error estimator for Magnus2

- In Table 6.7 the Methods Magnus2 and Magnus2 are compared, using equidistant time stepping for different step sizes. It is shown that Magnus2 is approximately twice as fast as Symm-Milne-32, because as stated in 6.3 the number of matrix exponentials is twice. The time is averaged over 100 runs and the unit is in seconds. The error for Symm-Milne-32 is much smaller for the same step size, because of a much smaller local error constant, Symm-Milne-32 has 0.05 and Magnus2 has 0.6.

Method	h	err	time
Magnus2	$1e-01$	$1.324e-03$	0.005
Symm-Milne-32	$1e-01$	$3.812e-04$	0.004
Magnus2	$1e-02$	$1.328e-05$	0.015
Symm-Milne-32	$1e-02$	$3.818e-06$	0.029
Magnus2	$1e-03$	$1.328e-07$	0.141
Symm-Milne-32	$1e-03$	$3.818e-08$	0.277
Magnus2	$1e-04$	$1.335e-09$	1.383
Symm-Milne-32	$1e-04$	$3.889e-10$	2.785

Table 6.7: Global error at  $t = 8.0$  for equidistant time-stepping, various stepsizes

- The costs for the error estimator vary significantly as Table 6.8 shows. For Magnus2 there is no additional matrix exponential to be evaluated, whereas the error estimator for Symm-Milne-32 is as expensive as the basic integrator.

Method	10000 steps without err est	10000 steps with err est
Magnus2	0.175	0.300
Symm-Milne-32	0.345	0.728

Table 6.8: Effort for the error estimator

- To determine if adaptive step size selection is faster than without, Table 6.9 shows that for Magnus2 it is a draw, but for Symm-Milne-32 it is definitely not. It uses about half the steps as needed for Magnus2. The columns "# steps adap" and "# steps equ" give the number of computed time steps, for the adaptive time stepping and the equidistant time stepping. The last two columns "time adap" and "time equ" show the computation time measured in seconds for both variants.



Method	# steps adap	# steps equi	time adap	time equi
TOL = $10^{-8}$				
Magnus2	1613	2487	0.046	0.046
Symm-Milne-32	757	1195	0.059	0.044
TOL = $10^{-10}$				
Magnus2	7490	11544	0.204	0.204
Symm-Milne-32	3515	5523	0.259	0.194
TOL = $10^{-12}$				
Magnus2	34772	53581	0.947	0.986
Symm-Milne-32	16322	25637	1.189	1.036

Table 6.9: Comparison of the efficiency of Strang (Magnus2) and Symm-Milne-32. The tolerances were  $10^{-8}$  (top),  $10^{-10}$  (middle) and  $10^{-12}$  (bottom), respectively. For equidistant time the minimal stepsize was used

- In Table 6.10 it is shown that Magnus4Optimized has the lowest error constant and Magnus4 is the fastest. Step sizes for this methods smaller than  $10^{-3}$  seem not to be beneficial as the global error increases again due to the effect of rounding error.

Method	h	err	time
Magnus4	$1e-01$	$3.300e-06$	0.004
Magnus4Optimized	$1e-01$	$1.525e-07$	0.006
EMB 4/3 AK s	$1e-01$	$3.395e-06$	0.009
EMB 4/3 M/AK	$1e-01$	$8.947e-07$	0.010
Magnus4	$1e-02$	$3.336e-10$	0.035
Magnus4Optimized	$1e-02$	$1.478e-11$	0.057
EMB 4/3 AK s	$1e-02$	$3.424e-10$	0.075
EMB 4/3 M/AK	$1e-02$	$9.100e-11$	0.079
Magnus4	$1e-03$	$3.317e-12$	0.369
Magnus4Optimized	$1e-03$	$3.125e-12$	0.609
EMB 4/3 AK s	$1e-03$	$7.132e-12$	0.663
EMB 4/3 M/AK	$1e-03$	$4.356e-12$	0.840
Magnus4	$1e-04$	$9.105e-12$	3.832
Magnus4Optimized	$1e-04$	$2.192e-11$	5.944
EMB 4/3 AK s	$1e-04$	$3.859e-11$	5.734
EMB 4/3 M/AK	$1e-04$	$2.683e-11$	7.007

Table 6.10: Global error at  $t = 8.0$  for equidistant time-stepping, various stepsizes

- To compare the efficiency of the error estimator look at Tabel 6.11, where you can see that the defect based error estimator for the Magnus schemes cost more than the basic integrator itself, for the embedded splitting scheme the cost for the error estimator are only 40% of the basic integrator.

Method	10000 steps without err est	10000 steps with err est
Magnus4	0.384	0.842
Magnus4Optimized	0.616	1.579
EMB 5/4 AK (ii)	1.369	1.911

Table 6.11: Effort for the error estimator

- Table 6.12 shows that for all Magnus schemes the adaptive time step selection is slower than computing with a fixed step size. The EMB 5/4 AK (ii) is for larger tolerances slightly better, and for smaller tolerances it could be called a tie. The fastest method over all is the Magnus4Optimized, which also needs fewest steps. The number of rejected steps (not displayed) is up to 4 because in the beginning the initial step size given was to big.

Method	# steps adap	# steps equi	time adap	time equi
TOL = $10^{-8}$				
Magnus4	175	233	0.045	0.020
Magnus4Optimized	74	99	0.036	0.008
EMB 5/4 AK (ii)	93	128	0.024	0.033
TOL = $10^{-10}$				
Magnus4	440	585	0.086	0.023
Magnus4Optimized	172	240	0.033	0.014
EMB 5/4 AK (ii)	227	321	0.053	0.045
TOL = $10^{-12}$				
Magnus4	1105	1469	0.098	0.057
Magnus4Optimized	422	599	0.070	0.037
EMB 5/4 AK (ii)	562	807	0.115	0.112

Table 6.12: Comparison of the efficiency of Magnus4, Magnus4Optimized and Emb 5/4 AK (ii) The tolerances were  $10^{-8}$  (top),  $10^{-10}$  (middle) and  $10^{-12}$  (bottom), respectively. For equidistant time the minimal stepsize was used

## 6.2.4 Results (8 electrons)

Now for 8 electrons in a line the system matrix  $H \in \mathbb{C}^{4900 \times 4900}$  is given by following definition,

$$f(t) = \cos \left( ae \left( \frac{-(t-t_0)^2}{2\sigma^2} \right) (\cos(\omega(t-t_0)) - \cos(\omega(-t_0))) \right) - 1 \quad (6.4)$$

$$g(t) = \sin \left( ae \left( \frac{-(t-t_0)^2}{2\sigma^2} \right) (\cos(\omega(t-t_0)) - \cos(\omega(-t_0))) \right) \quad (6.5)$$

$$H(t) = H_{\text{diag}} + H_{\text{off}_1} + f(t) \cdot H_{\text{off}_1} + i \cdot g(t) \cdot H_{\text{off}_2} \quad (6.6)$$

where  $H_{\text{diag}}$  is a diagonal matrix  $H_{\text{off}_1}$  is symmetric and  $H_{\text{off}_2}$  is skew symmetric. As a result  $H(t)$  is also hermitian. The scalar parameters for  $f$  and  $g$  are given by,

$$U = 5, \quad a = 2, \quad \omega = 7, \quad t_0 = 2, \quad \sigma = 1. \quad (6.7)$$

### Reference Solution

Starting with a step size of  $t_0 - t_{\text{end}}$  the step size is halved every iteration, as long as the distance between the solution at  $t_{\text{end}}$  and the one computed with the previous step size is decreasing. In this case PP 56 A was used. It took 11 refinements

to the final step size,  $7.813e - 3$  with the minimal distance of  $1.870e - 8$  to the previously computed one. Also the values of the solution at  $t_0 + (t_{end} - t_0) \cdot 2^{-i}, i \in 1, 2, \dots, 11$  are computed to be used as a reference solution for estimating the local error and its orders.

## Tables

The tables in this section are similar to them shown in 6.2.3, but for a much larger system. First there are some tables to show general that the splitting works, eq that the schemes have the predicted order, than second order methods are compared to determine their efficiency and later on 4-th order methods are compared.

- Tables 6.13, 6.14 and 6.15 show the global error, with respect to the reference solution at the end of the integration interval. The used step size is in the column h, err is the error and  $p$  is the experimental order, which is computed by the logarithm of the quotient from the error of two consecutive step sizes. For Emb 5/4 A k (ii) the global order is barely visibly because the step size region before the numerical rounding errors is very small.

	h	err	p
1	$8.000e + 00$	$1.058e + 00$	
2	$4.000e + 00$	$1.358e + 00$	-0.36
3	$2.000e + 00$	$1.167e + 00$	0.22
4	$1.000e + 00$	$1.407e + 00$	-0.27
5	$5.000e - 01$	$1.380e + 00$	0.03
6	$2.500e - 01$	$6.350e - 01$	1.12
7	$1.250e - 01$	$1.894e - 01$	1.75
8	$6.250e - 02$	$4.847e - 02$	1.97
9	$3.125e - 02$	$1.217e - 02$	1.99
10	$1.563e - 02$	$3.044e - 03$	2.00
11	$7.813e - 03$	$7.593e - 04$	2.00
12	$3.906e - 03$	$1.881e - 04$	2.01

Table 6.13: Global Error at  $t = 8.0$ ; Magnus2

	h	err	p
1	$8.000e+00$	$1.417e+00$	
2	$4.000e+00$	$1.276e+00$	0.15
3	$2.000e+00$	$1.405e+00$	-0.14
4	$1.000e+00$	$1.383e+00$	0.02
5	$5.000e-01$	$9.244e-01$	0.58
6	$2.500e-01$	$3.767e-01$	1.30
7	$1.250e-01$	$5.665e-02$	2.73
8	$6.250e-02$	$1.423e-02$	1.99
9	$3.125e-02$	$3.560e-03$	2.00
10	$1.563e-02$	$8.885e-04$	2.00
11	$7.813e-03$	$2.203e-04$	2.01
12	$3.906e-03$	$5.328e-05$	2.05

Table 6.14: Global Error at  $t = 8.0$ ; Symm-Milne-32

	h	err	p
1	$8.000e+00$	$1.082e+00$	
2	$4.000e+00$	$1.458e+00$	-0.43
3	$2.000e+00$	$1.367e+00$	0.09
4	$1.000e+00$	$1.257e+00$	0.12
5	$5.000e-01$	$5.125e-01$	1.29
6	$2.500e-01$	$5.653e-02$	3.18
7	$1.250e-01$	$4.152e-04$	7.09
8	$6.250e-02$	$3.194e-05$	3.70
9	$3.125e-02$	$8.233e-06$	1.96
10	$1.563e-02$	$6.869e-06$	0.26
11	$7.813e-03$	$6.798e-06$	0.02
12	$3.906e-03$	$6.789e-06$	0.00

Table 6.15: Global Error at  $t = 8.0$ ; EMB 5/4 AK (ii)

- In Table 6.16 the properties of the local error can be seen. Column err1 shows the local error and err2 the error of the defect based error estimator, which is the error of the by the error estimator corrected solution. The orders are the ones one would expect for Strang  $p = 2$ ,  $p + 1$  and  $p + 2$ .

	h	err1	p1	err2	p2
1	$8.000e+00$	$1.058e+00$		$1.666e+03$	
2	$4.000e+00$	$1.368e+00$	-0.37	$1.007e+01$	7.37
3	$2.000e+00$	$1.379e+00$	-0.01	$8.609e+01$	-3.10
4	$1.000e+00$	$9.787e-01$	0.49	$9.053e+00$	3.25
5	$5.000e-01$	$2.639e-01$	1.89	$4.638e-01$	4.29
6	$2.500e-01$	$4.377e-02$	2.59	$5.061e-02$	3.20
7	$1.250e-01$	$6.941e-03$	2.66	$3.533e-03$	3.84
8	$6.250e-02$	$8.973e-04$	2.95	$2.139e-04$	4.05
9	$3.125e-02$	$1.110e-04$	3.02	$1.299e-05$	4.04
10	$1.563e-02$	$1.370e-05$	3.02	$7.990e-07$	4.02
11	$7.813e-03$	$1.699e-06$	3.01	$5.003e-08$	4.00
12	$3.906e-03$	$2.111e-07$	3.01	$3.971e-09$	3.66

Table 6.16: Local error and error of the defect based error estimator for Magnus2

- In the Table 6.17 it is shown that Magnus2 is approximately twice as fast as Symm-Milne-32, because as stated in 6.3 the number of matrix exponentials is twice. The error for Symm-Milne-32 is much smaller for the same step size.

Method	h	error	time
Magnus2	$1e-01$	$1.228e-01$	1.931
Symm-Milne-32	$1e-01$	$3.630e-02$	3.741
Magnus2	$1e-02$	$1.244e-03$	18.223
Symm-Milne-32	$1e-02$	$3.607e-04$	36.254
Magnus2	$1e-03$	$1.393e-05$	184.817
Symm-Milne-32	$1e-03$	$5.180e-06$	363.343

Table 6.17: Global error at  $t = 8.0$  for equidistant time-stepping, various stepsizes

- The costs for the error estimator vary dramatically as Table 6.18 shows. For Magnus2 there is no additional matrix exponential to be evaluated, whereas the error estimator for Symm-Milne-32 is as expensive as the basic integrator.

Method	1000 steps without err est	1000 steps with err est
Magnus2	22.762	27.459
Symm-Milne-32	46.037	90.545

Table 6.18: Effort for the error estimator

- The main question is if the computation with error estimating and adaptive step size selection is faster than without. Table 6.19 gives the answer for Magnus2 this is correct with a speed up of a factor 2, but for Symm-Milne-32 it is not. It uses about half the steps as needed for Magnus2.

Method	# steps adap	# steps equi	time adap	time equi
TOL = $10^{-4}$				
Magnus2	275	705	7.928	16.335
Symm-Milne-32	147	360	15.300	16.505
TOL = $10^{-6}$				
Magnus2	1263	3269	35.013	74.313
Symm-Milne-32	618	1637	57.627	74.398
TOL = $10^{-8}$				
Magnus2	5846	15166	161.191	345.653
Symm-Milne-32	2917	7701	280.121	352.199

Table 6.19: Comparison of the efficiency of Strang (Magnus2) and Symm-Milne-32 The tolerances were  $10^{-4}$  (top),  $10^{-6}$  (middle) and  $10^{-8}$  (bottom), respectively. For equidistant time the minimal stepsize was used

- Figure 6.1 shows the adaptive chosen step size for Magnus2. If the step size is chosen too small, in this case five orders of magnitude wrong, the adaptive selection algorithm nearly instantly corrects this. The wrong initial step size gives you a total of additional 9 steps to compute. The minimal step size occurs around  $t = 2$ , because there the changes of the matrix are the strongest in time.

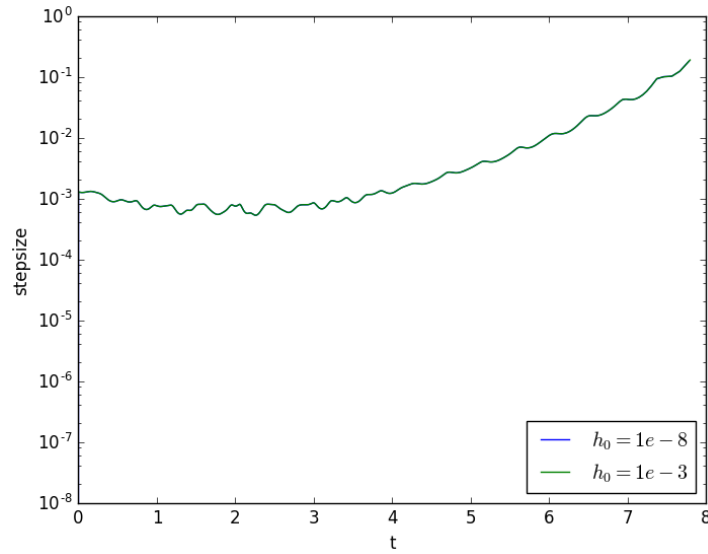


Figure 6.1: Step size over time for Magnus2 with  $TOL = 10^{-8}$  with different initial step sizes.

- In the Table 6.20 it is shown that Magnus4Optimized has the lowest error constant and Magnus4 is the fastest, but due to the numerical inaccuracy all compared methods have the same error for step sizes smaller than 0.01.

Method	h	err	time
Magnus4	$1e-01$	$5.469e-04$	4.165
Magnus4Optimized	$1e-01$	$4.153e-05$	6.669
EMB 4/3 AK s	$1e-01$	$4.626e-04$	8.165
EMB 4/3 M/AK	$1e-01$	$1.236e-04$	9.376
Magnus4	$1e-02$	$4.730e-06$	40.363
Magnus4Optimized	$1e-02$	$4.731e-06$	66.643
EMB 4/3 AK s	$1e-02$	$4.736e-06$	74.517
EMB 4/3 M/AK	$1e-02$	$4.774e-06$	91.337
Magnus4	$1e-03$	$1.587e-06$	428.143
Magnus4Optimized	$1e-03$	$1.638e-06$	699.416
EMB 4/3 AK s	$1e-03$	$1.582e-06$	728.632
EMB 4/3 M/AK	$1e-03$	$6.338e-06$	909.764

Table 6.20: Global error at  $t = 8.0$  for equidistant time-stepping, various stepsizes.



- Table 6.21 shows that for the Magnus-type schemes the evaluation of the sum of commutators already has not negligible costs. The embedded scheme proves again the the costs of the error estimator are cheap compared to the other methods.

Method	1000 steps without err est	1000 steps with err est
Magnus4	51.934	102.975
Magnus4Optimized	85.633	200.748
EMB 5/4 AK (ii)	177.413	244.238

Table 6.21: Effort for the error estimator

- Table 6.22 shows that for Magnus4 and EMB 5/4 AK (ii) it is a tie or doing adaptive time stepping is slightly better. Though the fastest method over all is the Magnus4Optimized. Also worth while to mention is that for tolerance  $10^{-8}$  the number of steps used in EMB 5/4 AK (ii) is significant higher than before, this is probably the result that the error estimator is the difference of two solution, which are limited in their accuracy by  $\sqrt{e\bar{p}s}$ . This leads to many rejections of steps. For the both Magnus schemes the defect error estimator which is scaled by the step size still gives an accurate estimate.

Method	# steps adap	# steps equi	time adap	time equi
TOL = $10^{-4}$				
Magnus4	70	148	8.138	7.425
Magnus4Optimized	39	77	10.639	6.365
EMB 5/4 AK (ii)	35	67	15.556	13.181
TOL = $10^{-6}$				
Magnus4	172	375	18.017	18.930
Magnus4Optimized	76	156	17.634	13.325
EMB 5/4 AK (ii)	84	167	27.678	29.217
TOL = $10^{-8}$				
Magnus4	430	952	43.826	47.752
Magnus4Optimized	169	345	33.952	28.826
EMB 5/4 AK (ii)	658	1382	224.973	245.597

Table 6.22: Comparison of the efficiency of Magnus4, Magnus4Optimized and Emb 5/4 AK (ii) The tolerances were  $10^{-4}$  (top),  $10^{-6}$  (middle) and  $10^{-8}$  (bottom), respectively. For equidistant time the minimal stepsize was used. Note that for TOL= $10^{-8}$  the accuracy of the matrix exponential is the limiting factor.

### 6.3 Gray-Scott equation

As a parabolic example, we study the Gray-Scott system (see [13]) modeling a two-component reaction-diffusion process, in two,  $\mathbf{x} \in \mathbb{R}^2$ , or three,  $\mathbf{x} \in \mathbb{R}^3$ , dimensions

$$\partial_t u(\mathbf{x}, t) = c_u \Delta u(\mathbf{x}, t) - u(\mathbf{x}, t) v^2(\mathbf{x}, t) + \alpha(1 - u(\mathbf{x}, t)), \quad (6.8a)$$

$$\partial_t v(\mathbf{x}, t) = c_v \Delta v(\mathbf{x}, t) + u(\mathbf{x}, t) v^2(\mathbf{x}, t) - \beta v(\mathbf{x}, t). \quad (6.8b)$$

The nonlinear term describes the reaction  $u + 2v \rightarrow 3v$  of two chemical components which are described by  $(u(\mathbf{x}, t), v(\mathbf{x}, t))$ .  $\alpha$  is the rate of fresh  $u$  added and  $\beta$  is the amount of  $v$  removed. This has been discussed in [10]. For this model it is natural to have periodic boundary conditions. The system is a model for pattern formation with dynamical behavior. Splitting only in two components (6.9) will not allow to solve the nonlinear term  $B$  exactly,

$$\underbrace{\begin{pmatrix} c_u \Delta - \alpha & 0 \\ 0 & c_v \Delta - \beta \end{pmatrix} U(\mathbf{x}, t) + \begin{pmatrix} \alpha \\ 0 \end{pmatrix}}_{=A} + \underbrace{\begin{pmatrix} -u(\mathbf{x}, t) v^2(\mathbf{x}, t) \\ u(\mathbf{x}, t) v^2(\mathbf{x}, t) \end{pmatrix}}_{=B}. \quad (6.9)$$

The implementation solves this by using numerical integration for, example a Runge–Kutta integrator. In Table 6.23 the global error and experimental order

for Strang is shown.

	h	err	p
1	1.000e+00	1.831e-03	1.77
2	5.000e-01	5.363e-04	1.94
3	2.500e-01	1.393e-04	1.98
4	1.250e-01	3.518e-05	1.99
5	6.250e-02	8.817e-06	1.99
6	3.125e-02	2.205e-06	1.99
7	1.563e-02	5.515e-07	1.99
8	7.813e-03	1.378e-07	2.00
9	3.906e-03	3.446e-08	2.00
10	1.953e-03	8.613e-09	2.00
11	9.765e-04	2.145e-09	2.04

Table 6.23: Global error at  $t = 1.0$ ; Strang

Though splitting into 3 operators according to

$$\underbrace{\begin{pmatrix} c_u \Delta - \alpha & 0 \\ 0 & c_v \Delta - \beta \end{pmatrix} U(\mathbf{x}, t) + \begin{pmatrix} \alpha \\ 0 \end{pmatrix}}_{=A} + \underbrace{\begin{pmatrix} 0 \\ u(\mathbf{x}, t)v^2(\mathbf{x}, t) \end{pmatrix}}_{=B} - \underbrace{\begin{pmatrix} u(\mathbf{x}, t)v^2(\mathbf{x}, t) \\ 0 \end{pmatrix}}_{=C}.$$

allows all the subflows to be integrated exactly, but the computation time is higher [10]. For example compare Table 6.23 with 6.24, this shows that the error for the same step size is approximately twice as big. This also corresponds to the computed LEM see [5] for both of this schemes, the value of the LEM for Strang is 0.6 and Strang ABC has LEM 1.5.

	h	err	p
1	$1.000e+00$	$3.401e-03$	2.00
2	$5.000e-01$	$8.502e-04$	2.00
3	$2.500e-01$	$2.125e-04$	2.00
4	$1.250e-01$	$5.313e-05$	2.00
5	$6.250e-02$	$1.328e-05$	2.00
6	$3.125e-02$	$3.321e-06$	1.99
7	$1.563e-02$	$8.302e-07$	1.99
8	$7.813e-03$	$2.075e-07$	1.99
9	$3.906e-03$	$5.189e-08$	1.99
10	$1.953e-03$	$1.297e-08$	1.99
11	$9.766e-04$	$3.250e-09$	1.97

Table 6.24: Global error at  $t = 1.0$ ; Strang ABC

See Table 6.25 where PP 3/4 A 3 c is the only ABC-splitting scheme. This table also shows that a second order scheme needs a lot more steps than a third order scheme. The fewest steps were made by the ABC-splitting scheme. The fastest for the larger tolerance was the equidistant Emb 4/3 A c and for the smaller tolerance equidistant PP 3/4 A c. Time adaptivity is of no use in this simulation as the solution has rapid changes all the time on different places, which will not allow larger bigger step sizes in time.

Method	# steps adap	# steps equi	time adap	time equi
TOL = $10^{-5}$				
Milne 2/2 c (i),	406	486	57.04	28.21
Emb 4/3 A c,	67	79	17.72	11.46
PP 3/4 A c,	116	135	23.02	12.99
PP 3/4 A 3 c,	65	67	26.74	13.23
TOL = $10^{-8}$				
Milne 2/2 c (i),	4691	5625	878.72	503.93
Emb 4/3 A c,	516	612	174.30	128.19
PP 3/4 A c,	929	1107	195.87	106.79
PP 3/4 A 3 c,	555	645	244.41	138.38

Table 6.25: Comparison of the efficiency of Milne 2/2 c (i), Emb 4/3 A c, PP 3/4 A c and PP 3/4 A 3 c for (6.8). The tolerances were  $10^{-5}$  (top) and  $10^{-8}$  (bottom), respectively.

For parabolic equations it is essential that the splitting coefficients have non-negative real part. This leads for higher order schemes  $p > 2$  to complex coefficients. Coefficients from [5] can be identified to have complex entries by “ c ” at the end of their name. The full error analysis was done in [10].

### 6.3.1 Implementation

The code is written in FORTRAN, using MPI library and 2DECOMP&FFT [21], a library to distribute the data efficient to multiple nodes (computers) and compute the FFT. This allows the code to be run on large clusters as the Vienna Scientific Cluster (VSC) [27].

This high performance computing (hpc) system has 1314 nodes with 2 AMD Opteron “Magny Cours 6132HE” with 8 cores each running at 2,2 GHz. The memory of one node is 8 x 4 GB ECC DDR3 RAM and an 16 GB SSD. The system is connected by 2 x Gigabit Ethernet LAN and 1 x Infiniband-QDR. The operating system is Scientific Linux 6.0 with Intel MPI and Open MPI. Figure 6.2 shows that if double the number of cores where used to run the simulation the time is nearly halved, which would be the ideal case, dotted line. See section 6.3.2 for the 3-dimensional case to get the used parameters.

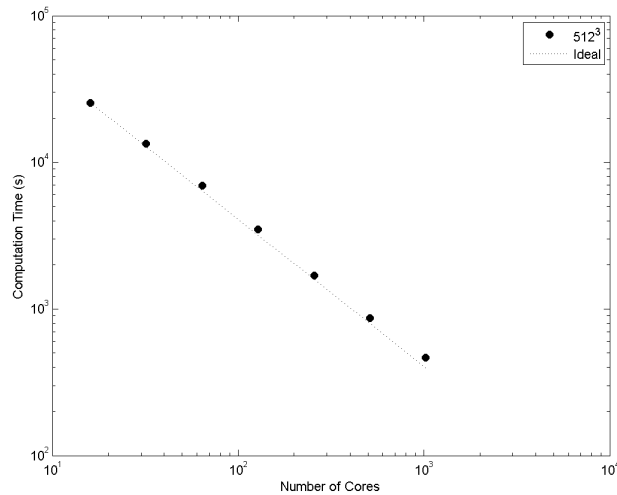


Figure 6.2: Scaling the number of cores.

To generate the pictures shown in 6.3.2 ParaView 4.1 [25] was used. This is a multi functional software to analyze and generate pictures from scientific data.

With this tool it is possible to use co-processing to render the visualization in situ without the need to write the raw data to disc, which can be very time consuming.

### 6.3.2 Visual results

The free parameters in (6.8) are chosen as

$$c_u = 0.04, \quad c_v = 0.005, \quad \alpha = 0.038, \quad \beta = 0.076. \quad (6.10)$$

#### 2 dimensions

In 2-dimension  $\mathbf{x} = (x, y) \in [-4\pi, 4\pi]^2$  we prescribe the initial condition as

$$u(x, y, 0) = 0.5 + \exp(-1 - (x^2 + y^2)), \quad v(x, y, 0) = 0.1 + \exp(-1 - (x^2 + y^2)). \quad (6.11)$$

A visualization of the solution component  $v$  at  $t = 0$ , 2000 and 4000 is shown in Figure 6.3.



Figure 6.3: Solution component  $v$  at  $t = 0$  (left),  $t = 2000$  (middle) and  $t = 4000$  (right) for (6.8).

#### 3 dimensions

In 3 spatial dimensions  $\mathbf{x} = (x, y, z) \in [-4\pi, 4\pi]^3$  we prescribe the initial condition

$$u(x, y, z, 0) = 0.5 + \exp(-1 - (x^2 + y^2 + z^2)), \quad (6.12)$$

$$v(x, y, z, 0) = 0.1 + \exp(-1 - (x^2 + y^2 + z^2)). \quad (6.13)$$

In Figure 6.4 we show the component  $v$  computed by a complex embedded 4/3 splitting pair from [19] with an underlying spatial discretization with  $512^3$  basis functions and a tolerance of  $10^{-5}$ . The solution is plotted at times  $t = 2500$ ,  $t = 3000$ ,  $t = 4000$ , and  $t = 5000$ .

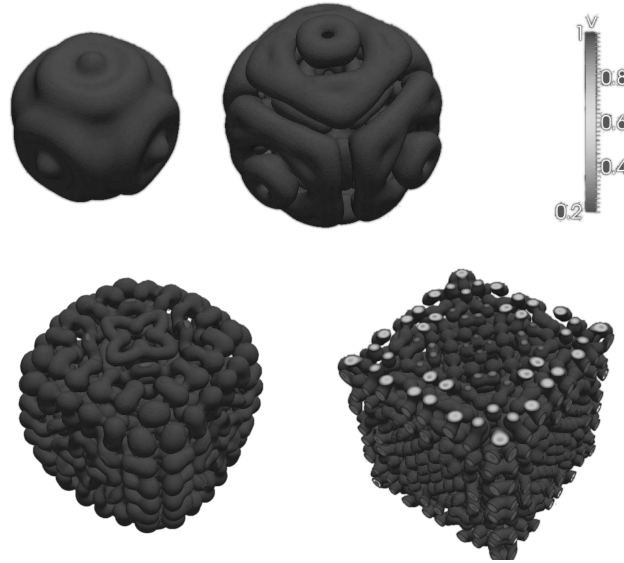


Figure 6.4: Solution component  $v$  for (6.8) in 3D at times  $t = 2500, 3000, 4000, 5000$ .

## 6.4 Schrödinger Equations

Splitting also works for wave equations, though one should choose only schemes with real coefficients. The standard form of the non relativistic Schrödinger equation for a single particle moving in an electric field is given by,

$$i\hbar\partial_t\psi(\mathbf{x},t) = \left(-\frac{\hbar^2}{2m}\Delta + V(\mathbf{x},t)\right)\psi(\mathbf{x},t) \quad (6.14)$$

with  $\hbar$  the Planck constant,  $m$  the particle's mass and  $V$  the potential energy. The notation for the unknown function is changed from  $u$  to  $\psi$ , because it is standard in literature about Schrödinger equations. There are two examples considered first the cubic nonlinear Schrödinger (NLS) equation 6.4.1 and a semi classical example in 6.4.2 with an time dependent potential.

### 6.4.1 The cubic NLS

The cubic nonlinear Schrödinger equation [26] is given by

$$i\partial_t\psi(\mathbf{x},t) = -\frac{1}{2}\Delta\psi(\mathbf{x},t) + \kappa|\psi(\mathbf{x},t)|^2\psi(\mathbf{x},t), \quad (6.15a)$$

$$\psi(\mathbf{x},0) = \psi_0(\mathbf{x}), \quad \mathbf{x} \in \mathbb{R}^n, \quad t > 0, \quad (6.15b)$$

where we set  $\kappa = -1$ . To reduce computing complexity and because all interesting effects are available, the 1-dimensional case is considered  $\mathbf{x} = x \in \mathbb{R}$  with the initial condition chosen as the sum of two solitons,

$$\psi_0(x) = \sum_{j=1}^2 \frac{a_j e^{-ib_j x}}{\cosh(a_j(2x - c_j))}, \quad x \in [-16, 16]. \quad (6.15c)$$

with  $a_1 = 2.0$ ,  $a_2 = 2.0$ ,  $b_1 = 1.0$ ,  $b_2 = 3.0$ ,  $c_1 = 5.0$ ,  $c_2 = -5.0$ .

The cubic NLS has been treated earlier in [4], a theoretical analysis is given in [20]. The two solitons which eventually cross [18], posing a challenge for an adaptive step-size selection algorithm. The two solitons cross approximately at  $t = 2.3$  as Figure 6.5 shows. The step size drops by a factor of 5 during the collision and afterwards regains to previous level. This kind of behaviour for the solution is necessary that the adaptive algorithms are faster than using an equidistant time integrator to achieve the same global error at  $t_{end}$  as Table 6.26 shows.

The last column in Table 6.26, ladled with err, shows that the global error strongly correlates with the prescribed tolerance. The scheme PP 5/6 A is the best for low tolerances and it beats the equidistant step size solution every time. The schemes with the defect based error estimator often fail to beat the equidistant step size solution.

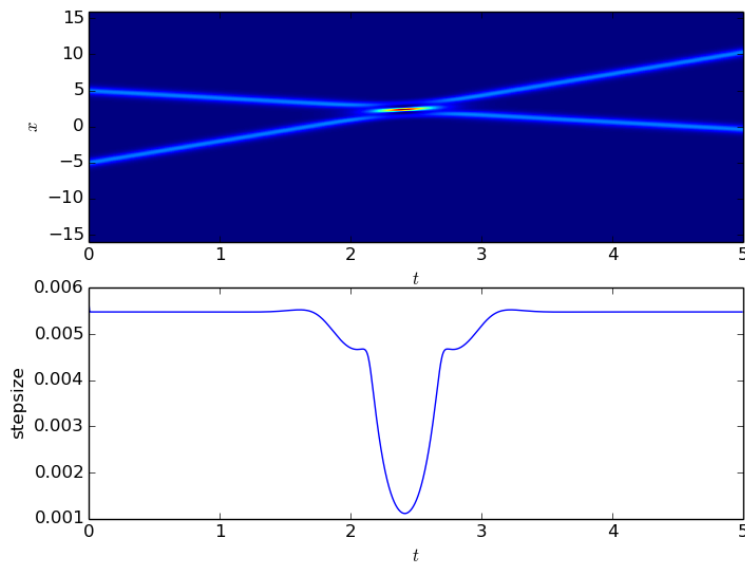


Figure 6.5: Solution of (6.15) (top), and stepsizes generated by an adaptive procedure based on PP 5/6 A with tolerance  $10^{-10}$  (bottom).



Method	# steps adap	# steps equi	time adap	time equi	err
TOL = $10^{-5}$					
Emb 4/3 AK p	275	586	0.123	0.130	$6.646e-05$
PP 3/4 A	438	772	0.150	0.106	$7.608e-05$
PP 5/6 A	154	394	0.136	0.149	$3.447e-04$
Emb 4/3 AK p D	265	469	0.131	0.103	$1.848e-04$
PP 3/4 A D	438	776	0.185	0.126	$7.526e-05$
PP 5/6 A D	188	581	0.188	0.263	$3.945e-05$
TOL = $10^{-8}$					
Emb 4/3 AK p	1536	3159	0.655	0.617	$6.971e-08$
PP 3/4 A	2478	2858	0.758	0.427	$3.719e-07$
PP 5/6 A	503	1292	0.392	0.477	$1.114e-07$
Emb 4/3 AK p D	1495	1619	0.647	0.316	$9.817e-07$
PP 3/4 A D	2478	2865	0.924	0.438	$3.717e-07$
PP 5/6 A D	567	1391	0.449	0.561	$6.386e-08$
TOL = $10^{-10}$					
Emb 4/3 AK p	4854	10382	1.975	2.091	$6.609e-10$
PP 3/4 A	7837	6766	2.406	1.060	$1.174e-08$
PP 5/6 A	1136	2433	0.945	0.975	$1.786e-09$
Emb 4/3 AK p D	4728	3870	2.163	0.862	$3.089e-08$
PP 3/4 A D	7837	6766	2.506	1.069	$1.174e-08$
PP 5/6 A D	1174	2491	1.122	1.074	$1.553e-09$

Table 6.26: Comparison of the efficiency of Emb 4/3 AK p, PP 3/4 A, and PP 5/6 A and their corresponding defect based error estimators for Nonlinear Schroedinger. The tolerances were  $10^{-5}$  (top),  $10^{-8}$  (middle) and  $10^{-10}$  (bottom), respectively. For equidistant time the optimal stepsize to get the same up to a 1% margin global error at  $t_{end} = 5.0$  was used.

In Figure 6.6 the Table 6.26 is used to generate a work precision diagram. On the x-axis the computation time in seconds is drawn and on the y-axis the  $L_2$  norm of the global error at  $t_{end}$ . Lines of the same color belong to same scheme, full lines are with adaptive time integration and the dashed ones for equidistant time integration. Strang scheme is added to show off the superiority of the other schemes. The Emb 4/3 AK p is the best third order scheme, the adaptive algorithm is also faster than the equidistant strategy.

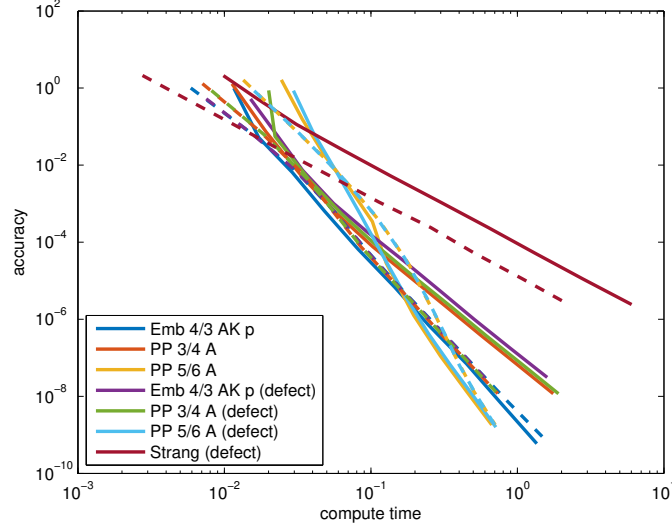


Figure 6.6: Work precision diagram of (6.15).

## 6.4.2 Quantum control

A model of quantum control of atomic systems discussed in [17] introduces a potential which explicitly depends on time to control the permeability:

$$i \partial_t \psi(\mathbf{x}, t) = \varepsilon \Delta \psi(\mathbf{x}, t) + \varepsilon^{-1} V(\mathbf{x}, t) \psi(\mathbf{x}, t), \quad (6.16a)$$

$$\psi(\mathbf{x}, 0) = \psi_0(\mathbf{x}), \quad \mathbf{x} \in \mathbb{R}^n, \quad t > 0, \quad (6.16b)$$

with potential  $V(\mathbf{x}, t)$ . The potential is the sum of an time independent and a time dependent one, which effects permeability. For this example it is also chosen the 1-dimensional case, where  $\mathbf{x} = x \in \mathbb{R}$ . The initial state and potential are given by

$$\begin{aligned} \psi_0(x) &= (\delta \pi)^{-\frac{1}{4}} e^{\frac{ik_0(x-x_0)}{\delta} - \frac{(x-x_0)^2}{2\delta}} \\ V(x, t) &= V_0(x) + \underbrace{\rho(3t-1)\rho(\sin(2\pi(x-t)))}_{=:E(x,t)} \\ V_0(x) &= \rho(4x) \sin(20\pi x) \\ \rho(x) &= \begin{cases} e^{\frac{-1}{1-x^2}}, & |x| < 1 \\ 0, & \text{otherwise,} \end{cases} \end{aligned}$$

where  $x_0 = -0.3$ ,  $k_0 = 0.1$ ,  $\delta = 10^{-3}$  and  $\varepsilon = 2^{-8}$ . The space was discretized with 2048 points on the interval  $(-1, 1)$ , with periodic boundary conditions.

It is clearly visible by comparing Figure 6.7 and Figure 6.8 that the time dependent potential allows larger amounts to pass through. This shows that the anticipated effect can be reached.

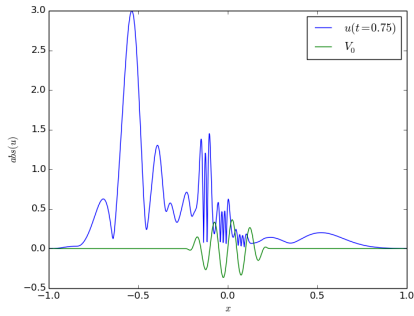


Figure 6.7:  $V(x,t) = V_0(x)$

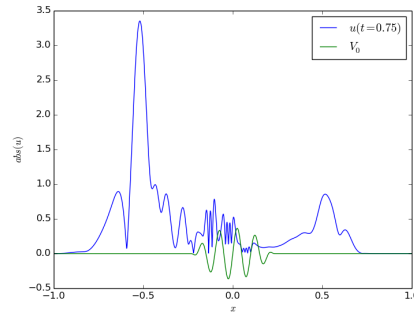


Figure 6.8:  $V(x,t) = V_0(x) + E(x,t)$

Figure 6.9 shows the space time plot of the solution with the time dependent potential. It shows that during the interaction of the soliton and the barrier the step size decreases and in the end increases again. Changing the semiclassical

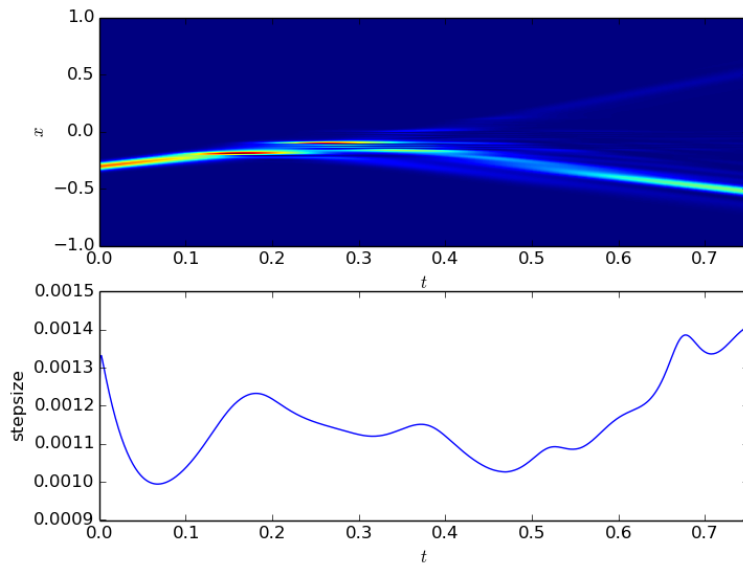


Figure 6.9: Solution (top) and step sizes (bottom) generated for (6.16) with  $\varepsilon = 2^{-8}$  for PP 5/6 A and tolerance  $10^{-10}$ .

parameter  $\varepsilon$  to  $10^{-5}$  gives after an initial drop by factor 10 oscillating step sizes,

see Figure 6.10. This results lead to further investigation on the parameter  $\varepsilon$  and the step size selection strategy.

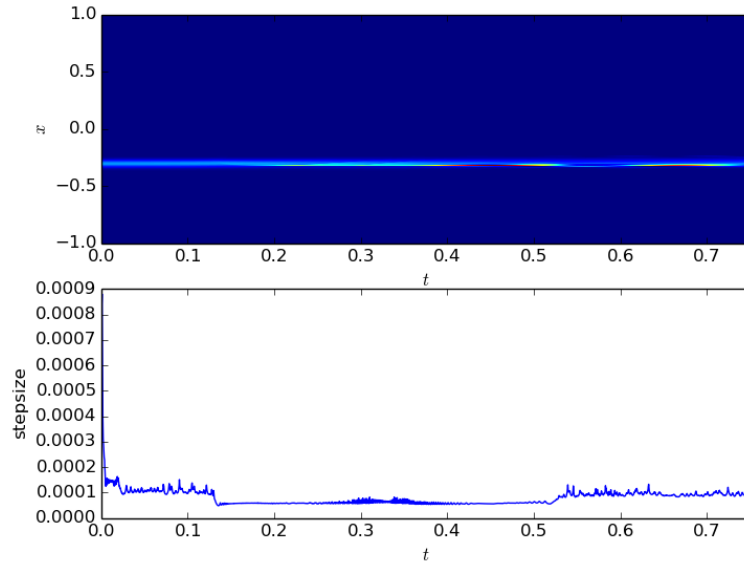


Figure 6.10: Solution (top) and step sizes (bottom) generated for (6.16) with  $\varepsilon = 10^{-5}$  for PP 5/6 A and tolerance  $10^{-10}$ .

To compare the step size selection strategies from 4.5 the change ratio is plotted in Figure 6.11, where ‘Simple’ refers to (4.23) and ‘2 Steps’ to (4.25). The change ratio in the first step is the highest because the algorithm needs to find the suitable stepsize. The 2 Step algorithm seems to have a smoother sequence of step sizes, especially in the case with small  $\varepsilon$ . Table 6.27 shows that the simple step size selection algorithm 4.23 is better than 4.25 in this situation. When forced to

Selection strategy	$\varepsilon$	steps	rejected steps	rejections per steps
Simple	$3.91e-03$	655	5	0.0076
	$1.00e-05$	10386	12	0.0012
2 Steps	$3.91e-03$	662	16	0.0242
	$1.00e-05$	10489	101	0.0096

Table 6.27: Comparing different step size selection methods PP 5/6 A

reach the given local error tolerance  $10^{-10}$  by a relative tolerance of  $10^{-1}$ ,

$$\text{err} < \text{TOL} \quad \text{and} \quad \frac{\text{err}}{\text{TOL}} - 1 < \text{reltol} \quad (6.17)$$

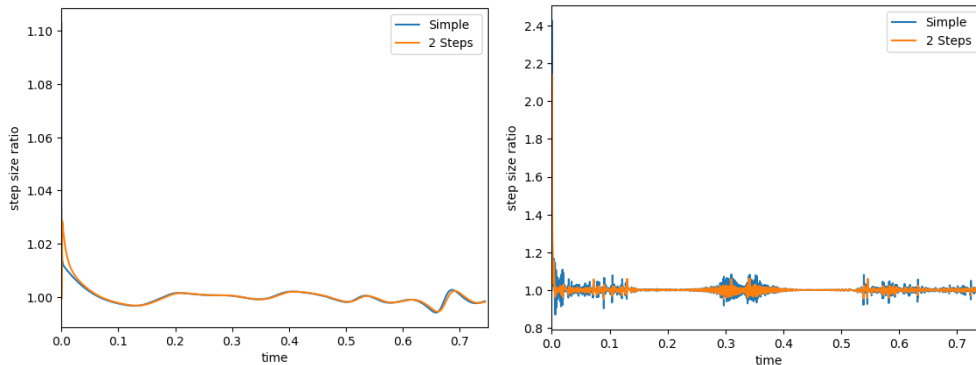


Figure 6.11: Comparing selection strategies for PP 5/6 A with tolerance  $10^{-10}$ . Left  $\varepsilon = 2^{-8}$  and right  $\varepsilon = 10^{-5}$ .

the number of rejected steps increases, as Table 6.28 shows. The two-step step size selection algorithm performs now better. But for the smaller value of  $\varepsilon$  both strategies fail, because they end up in an cycle of insufficient step sizes. Decreasing

Selection strategy	$\varepsilon$	steps	rejected steps	rejections per steps
Simple	$3.91e-03$	587	1408	2.3986
	$1.00e-05$	$\infty$	$\infty$	—
2 Steps	$3.91e-03$	591	989	1.6734
	$1.00e-05$	$\infty$	$\infty$	—

Table 6.28: Comparing different step size selection methods PP 5/6 A forced relative tolerance  $10^{-1}$ .

ing the relative tolerance to  $10^{-2}$  drastically deteriorates the number of rejected steps for the two-step step size selection strategy, see Table 6.29

Selection strategy	$\varepsilon$	steps	rejected steps	rejections per steps
Simple	$3.91e-03$	586	1538	2.6246
	$1.00e-05$	$\infty$	$\infty$	—
2 Steps	$3.91e-03$	586	4605	7.8584
	$1.00e-05$	$\infty$	$\infty$	—

Table 6.29: Comparing different step size selection methods PP 5/6 A forced relative tolerance  $10^{-2}$ .

### Investigating small $\varepsilon$

Table 6.30 and 6.31 show for different values of  $\varepsilon$ , how the error estimator and the size of the first step correlate. For a given  $\varepsilon$  and given tolerance  $10^{-10}$  the adaptive step size selecting strategy has been applied 100 times, for the step starting from  $t_0 = 0$ . The result of this procedure is seen in the column labeled  $h$ . The column to the right tries to measure if the step size converged to a specific value or oscillates by giving the ratio of  $h$  and the previously step size  $h_{-1}$ , 1.0 is the value for convergence. The last two columns give the by the error estimator estimated error and the exact error to the reference solution computed by  $\frac{h}{100}$  with PP 5/6 A. The error estimator is in the range of the exact error. Though the error estimator for small epsilon sometimes leads to too large step sizes and errors but the number of rejected steps is only slightly higher than in cases with larger  $\varepsilon$ .

$\varepsilon$	$h$	$h/h_{-1}$	err est	err
$3.91e-03$	$1.347e-03$	$1.000e+00$	$5.314e-11$	$5.698e-11$
$1.00e-05$	$4.165e-03$	$4.000e+00$	$2.177e-07$	$3.894e-07$

Table 6.30: 1 step PP 5/6 A

$\varepsilon$	$h$	$h/h_{-1}$	err est	err
$3.91e-03$	$1.334e-03$	$1.000e+00$	$5.053e-11$	$5.414e-11$
$1.00e-05$	$3.906e-03$	$4.000e+00$	$1.774e-07$	$3.130e-07$

Table 6.31: 1 step PP 5/6 A D

Further investigations on the parameter  $\varepsilon$  yielded that for some values of  $\varepsilon$  the step size selection leads to oscillations. The step size change is limited by a factor of 4, see 4.5 and Figure 6.12. The instant change from  $\frac{1}{4}$  to 4 and back are the result of swapping from the too large step size to the smaller one or vice versa. The defect based error estimator has more problems with small  $\varepsilon$ . Reducing the change rate to 2 gives Figure 6.13. Comparing both Figures shows that the problem is not solved by this measure.

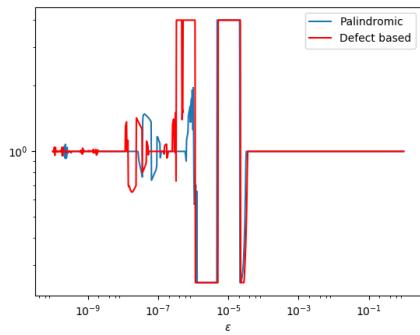


Figure 6.12: Comparing  $h/h_{-1}$  for PP 5/6 A and PP 5/6 A D with tolerance  $10^{-10}$  and changerate limited by 4.

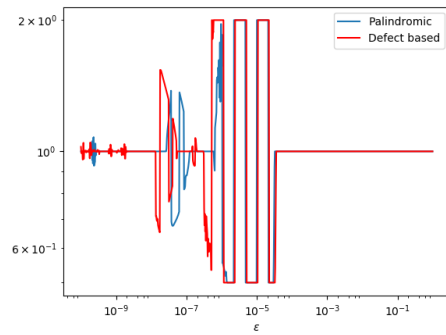


Figure 6.13: Comparing  $h/h_{-1}$  for PP 5/6 A and PP 5/6 A D with tolerance  $10^{-10}$  and changerate limited by 2.

# Chapter 7

## Spectral Method

The spectral method is used to solve partial differential equations, by representing the solution using global ansatz functions. Typical ansatz function are sin and cos for periodic boundary conditions or Chebyshev polynomials else.

Consider the NLS equation (6.15). The spacial dimension is set to 1 for simplicity. In higher dimensions the arguments follow the same. Since the  $L^2$ -function  $\psi$  can be assumed to be negligible outside an interval which can be scaled down to  $[-\pi, \pi]$ , without restriction of generality,

$$i \partial_t \psi(x, t) = -\frac{1}{2} \Delta \psi(x, t) + \kappa |\psi(x, t)|^2 \psi(x, t), \quad (7.1)$$

$$\psi(x, 0) = \psi_0(x), \quad x \in [-\pi, \pi], \quad t > 0, \quad (7.2)$$

$$u(-\pi, t) = u(\pi, t), \quad t \in [0, t_{end}] \quad (7.3)$$

**Trigonometric Interpolation** First the desired function is semidiscretized in space, by using an cut of Fourier series.

$$\psi(x, t) \approx \psi_k(x, t) = \sum_{j=-\frac{k}{2}}^{\frac{k}{2}-1} c_j(t) e^{ijx}, \quad x \in [-\pi, \pi], \quad k \text{ even} \quad (7.4)$$

The  $c_j(t)$  satisfy,

$$c_j(t) = \int_{-\pi}^{\pi} \psi(x, t) e^{ijx} dx. \quad (7.5)$$

In this case, we consider collocation on an equidistant grid

$$x_j = j \frac{2\pi}{k}, \quad j = -\frac{k}{2}, -\frac{k-1}{2}, \dots, \frac{k}{2} - 1, \quad (7.6)$$

which yields the set of equations,

$$i \partial_t \psi_k(x_j, t) = -\frac{1}{2} \Delta \psi_k(x_j, t) + \kappa |\psi_k(x_j, t)|^2 \psi_k(x_j, t), \quad j = -\frac{k}{2}, -\frac{k-1}{2}, \dots, \frac{k}{2} - 1. \quad (7.7)$$



**Discrete Fourier Transform** Let  $\mathcal{F}_k : \mathbb{C}^k \rightarrow \mathbb{C}^k$  denote the discrete Fourier transform of length  $k$ ,

$$\hat{\phi} = \mathcal{F}_k \phi \text{ with } \hat{\phi}_l = \sum_{j=-\frac{k}{2}}^{\frac{k}{2}-1} e^{-ilj2\frac{\pi}{k}} \phi_j, \quad l = -\frac{k}{2}, -\frac{k-1}{2}, \dots, \frac{k}{2}-1. \quad (7.8)$$

The inverse transform  $\mathcal{F}_k^{-1}$  is given by

$$\phi = \mathcal{F}_k^{-1} \hat{\phi} \text{ with } \phi_l = \frac{1}{k} \sum_{j=-\frac{k}{2}}^{\frac{k}{2}-1} e^{ilj2\frac{\pi}{k}} \hat{\phi}_j, \quad l = -\frac{k}{2}, -\frac{k-1}{2}, \dots, \frac{k}{2}-1. \quad (7.9)$$

Though mathematicians like it more if  $\mathcal{F} = \mathcal{F}^{-1}$ , but this is computational extensive because than you would have to scale the data twice with a factor  $\frac{1}{\sqrt{k}}$  instead once with  $\frac{1}{k}$ . Both of the transforms can be implemented with computational complexity  $\mathcal{O}(k \log k)$  via the fast Fourier transform (FFT) [12]. For the Fourier transform generally holds,

$$\mathcal{F} \frac{\partial}{\partial x} \phi(x) = ix \mathcal{F} \phi(x) \quad (7.10)$$

The derivative in  $x$  direction in the problem is changed to a multiplication after the Fourier transformation. This changes the PDE to an ODE, in  $t$

$$i \partial_t \psi_k = -\frac{1}{2} \mathcal{F}_k^{-1} (ix)^2 \mathcal{F}_k \psi_k + |\psi_k|^2 \psi_k \quad (7.11)$$

The approximation error at  $t = 0$  for any  $s \in \mathbb{N}^+$  is bounded by

$$\|\psi - \psi_k\|_{L_2} \leq Ck^{-s} \|\partial_x^s \psi\|_{L_2} \quad (7.12)$$

if  $\partial_x^s \psi(\cdot, 0) \in L_2$ , which can be shown by Parseval's formula and partial integration. The error bounds for all  $t > 0$  is given by,

$$\|\psi(t) - \psi_k(t)\|_{L_2} \leq Ck^{-s} (1+t) \max_{\tau \in [0, t]} \|\partial_x^s \psi(\tau)\|_{L_2} \quad (7.13)$$

if the exact solution fulfills  $\partial_x^{s+2} \psi(\cdot, t) \in L_2$ .

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