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⁸ Layer Formation on K-feldspar in ⁹ Fluidized Bed Combustion and ¹⁰ Gasification with bark and chicken ¹¹ manure

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28

29 Abstract

The layer formation on bed materials in fluidized bed applications is an often-studied phenomenon where most work has focused on combustion but some studies on gasification exists, and direct comparisons of layer formation in combustion and gasification have been

performed occasionally. The present work provides a thorough comparison of layer formation 33 during combustion and gasification with K-feldspar as bed material using different 34 feedstocks, namely Ca-rich bark; Ca- and P-rich chicken manure; and an admixture of 35 chicken manure with bark. The feedstocks are tested in a 5 kW bubbling fluidized bed 36 combustor and a 100 kW_{th} dual fluidized bed steam gasifier. A reference bed material sample 37 38 from the industrial biomass combined heat and power plant (CHP) in Senden is used as example for the gasification of bark-rich logging residues. The formed bed particle layers on 39 40 the bed material surface are characterised using combined scanning electron microscopy and energy-dispersive X-ray spectroscopy; area mappings and line scans are carried out for 41 all samples. The obtained data shows no essential influence of operational mode on the 42 layer formation process. During the combustion and gasification of Ca-rich feedstocks a layer 43 rich in Ca formed while K is diffusing out of the layer. The use of Ca- and P-rich feedstocks 44 inhibited the diffusion of K and a layer rich in Ca and also P formed. The addition of P to the 45 feedstock by chicken manure therefore changed the underlying layer formation processes. 46

47 Keywords

48 Fluidized bed, layer formation, K-feldspar, P, combustion, gasification

49 Highlights

- 50 Layer formation on K-feldspar is the same during combustion and gasification
- P-rich chicken manure promotes the formation of phosphates in layers
- P-rich chicken manure hinders diffusion of K out of the K-feldspar particles

53 **1. Introduction**

The Holocene epoch, which already lasts for more than 11,700 years, is the only state of the earth system to be known of supporting contemporary human societies. Human activities since the age of industrialization are strongly influencing the earth system increasing the risk of destabilization, resulting in a state less hospitable to the development of human societies. Nine planetary boundaries that define a safe operating space for human societies have been

59 defined, as displayed in Figure 1. [1]



Figure 1. Current status of seven of nine planetary boundaries [1].

60 The biogeochemical flow of P is one of the planetary boundaries already in a high risk zone.

61 Addressing the further use and possible recovery potential of waste streams containing

relevant amounts of P is therefore of major importance. The use of such P-rich waste
streams as feedstock in thermochemical conversion applications (e.g. combustion,
gasification) is one strategy to address the challenge with biogeochemical flows of P by both
reducing waste and enabling recovery and recycling.

66 Fluidized bed technology is a promising application for such thermochemical conversion of biogenic feedstock. Thermal conversion in fluidized beds allows for utilization of different 67 feedstock [2] and is an industrial established technology. Thermochemical gasification of 68 biogenic feedstock is a promising option to advance the eco-friendly and efficient production 69 of secondary energy carriers, heat and power generation out of the product gas. The dual 70 fluidized bed (DFB) steam gasification of bark-rich logging residues demonstrates a well-71 proven technology to produce nitrogen-free product gas with a heating value of around 72 11-15 MJ Nm⁻³. The basic principle of the process is shown in Figure 2. This process is 73 based on the separation of endothermic gasification and exothermic combustion. Heat, which 74 is necessary for gasification, is provided by the circulating bed material from the combustion 75 to the gasification reactor. Steam is used as gasification agent for the bubbling bed in the 76 gasification reactor. A part of the biomass is combusted to provide the heat necessary for 77 gasification [3]. A comprehensive review on the DFB gasification technology was recently 78 published by Karl and Pröll [4]. 79

Based on this concept the first industrial application using wood as feedstock was commissioned in the early 2000's with the combined heat and power plant Güssing in Austria (8 MW_{th} feedstock capacity). Further plants went into operation in Oberwart/Austria (9 MWfuel capacity), Villach/Austria (15 MW_{th} feedstock capacity), Senden/Germany (14 MW_{th} feedstock capacity), and in Göteborg/Sweden (32 MW_{th} feedstock capacity).



Figure 2. Basic principle of DFB steam gasification [3].

The economic feasibility of biomass projects is highly dependent on the feedstock price. Additionally, biogenic feedstock should not be in competition with food production. To reduce feedstock costs biogenic residues are a promising alternative to woody biomass. One of the challenging issues for the utilization of residues for gasification is the high ash content, which contains various elements. Understanding the ash chemistry in the system is a key factor for further development of the technology [5].

91 Interactions between feedstock ash and bed material particles have been investigated in the 92 past. Ash layer formation has been described on a mechanistic level for combustion of 93 various feedstocks and for gasification of bark-rich logging residues [2,6–8]. Furthermore, 94 positive catalytic effects have been assigned to Ca-rich ash layers in gasification leading to 95 an improvement of the product gas quality compared to fresh olivine [9,10]. A kinetic rate 96 expression was empirically derived for olivine after an ash-rich layer has formed [11].

Berdugo Vilches et al. proposed a first overview of the main transformation reactions 97 98 pathways of tar species when olivine, activated through interaction with ash components, is used as in-bed catalyst [12]. Optimization of the operation of an industrial-scale DFB steam 99 gasification plant based on the activation of the bed material through interaction with 100 feedstock ash was reported by Kuba et al. [13]. Here, already catalytically activated olivine 101 102 bed particles were reused in the process to increase the overall activity of the fluidized bed. Similar results regarding the optimization in industrial-scale were obtained at the DFB steam 103 104 gasifier GoBiGas, where ash components were identified to play a major role in improving the product gas quality [14]. 105

First insights into ash layer formation in both combustion and gasification [15,16] have been 106 reported, indicating that the operational mode has no influence on the layer formation, apart 107 108 from S-rich feedstocks, where the formation of a melt only occurring during combustion enhances the agglomeration tendency of S-rich feedstocks [15]. The influence of P on the 109 layer formation has been studied in combustion [2] and gasification [17] atmosphere, but to 110 the authors' knowledge no study focused on a comparison of P-rich feedstocks in both 111 combustion and gasification atmosphere. Several groups currently focus on the substitution 112 of olivine as bed material in DFB steam gasification [17-26] due to its heavy metal content 113 [8]. K-feldspar was found as impurity in CHP in Senden, where layers rich in Ca developed 114 and thermochemical analysis showed that these layers show a lower tendency towards 115 agglomeration compared to layers formed on quartz particles [8]. Alkali-feldspar (a mixture of 116 K-feldspar and Na-feldspar, with traces of Ca-feldspar) was shown to have a catalytic activity 117 towards tar reforming [19] and was tested as bed material in the Chalmers 2-MW gasifier 118 [18]. No catalytic activity towards the water-gas-shift reaction was detected for pure K-119 feldspar [17,27] but it was possible to activate the K-feldspar by layer formation during the 120 gasification in a 100 kW_{th} DFB reactor at TU Wien with a mixture of bark, straw, and chicken 121 manure as feedstock [17]. 122

Therefore, this paper addresses the influence of P on the layer formation both in fluidized bed combustion and gasification with K-feldspar as bed material. Samples from both fluidized bed combustion as well as DFB steam gasification facilities were evaluated. Furthermore, the influence of P from the feedstock regarding layer formation is addressed. For this, P-lean bark, P-rich chicken manure, and an admixture of chicken manure to bark are compared regarding their layer formation process.

129 **2. Materials and Methods**

130

Bed material samples were collected from fluidized bed combustion as well as gasification and compared regarding their layer formation. The combustion experiments were carried out in a 5 kW bubbling fluidized bed reactor. Bed material samples for gasification were obtained from the CHP (15 MW_{th}) in Senden and from a 100 kW_{th} DFB pilot plant at TU Wien.

135 **2.1. Feedstocks**

The feedstocks used for these investigations were conifer bark during combustion and barkrich logging residues for gasification; a mixture of bark with chicken manure (ratio 7:3 dry mass) during combustion and gasification; and pure chicken manure during combustion and gasification. Table 1 shows relevant data for the feedstocks used. The ash content was

- determined according to DIN 14775 but at a temperature of 550 °C and the lower heatingvalue was determined according to DIN 51900 T2.
- 142Table 1. Ash content and LHV of the used feedstocks. The table also gives an overview of the reactors143that each feedstock was used in.

		Ash content	LHV ^b	
Fuel	Used in	mass	kJ kg⁻¹ (d.b.ª)	
		fraction		
		given in %		
		d.b. ^a		
Bark	5 kW _{th} BFB Combustion	8.1	18180	
Bark-rich	15 MW CHP Sondon	15	17920	
logging residues		1.5		
Bark+chicken	5 kW RER Combustion + 100 kW DER	12.5	16430	
manure (7:3)	5 KW th BFB Compustion + 100 KW th DFB	13.5		
Chicken manure	5 kW _{th} BFB Combustion+ 100 kW _{th} DFB	25.4	13900	

^a dry basis, ^b lower heating value

145 Figure 3 shows the feedstock ash components (fuel fingerprint) of the used feedstocks,

determined using XRF. Displaying the ash composition in mol kg⁻¹ gives a better overview of

the possible interactions taking place in the ash [28]. The used values to obtain Figure 3 are

148 given in the supplementary in Table .



Figure 3. Feedstock ash components in the used feedstocks.

149 **2.2. Bed material**

Feldspar is currently investigated comprehensively as bed material for DFB steam gasification [17–19]. K-feldspar has a mohs' hardness of 6 and its density is 2600 kg m⁻³. Additionally, it is an easily available mineral and therefore a promising bed material especially for gasification.

For the combustion experiments in the 5 kW test rig, K-feldspar was sieved to a particle size 154 of 200 - 250 µm as needed for the bubbling fluidized bed reactor. The K-feldspar studied 155 156 from the CHP in Senden is an "impurity" introduced with the feedstock into the olivine bed, which is currently used in commercial DFB gasifiers. For the gasification test campaigns in 157 the 100 kW DFB pilot plant a mixture of 0.89 kg kg⁻¹ K-feldspar ($d_{SV} = 287 \mu m$) and 0.11 kg 158 kg⁻¹ limestone (d_{SV} =480 µm) was used. The calcite was added to increase the catalytic 159 activity of the bed during start-up, since the pure and unused K-feldspar does not possess 160 any catalytic activity [17,27]. 161

162

2.3. Fluidized bed reactors for experimental investigations

Combustion experiments were conducted in a 5 kW bubbling fluidized bed (BFB) reactor. 164 165 The total height of the reactor is 2 m with an inner diameter of 100 mm at the air distribution 166 plate and 200 mm in the freeboard section. Temperatures and pressures could be monitored continuously. The fluidized bed was maintained with a primary air flow of 50 NL min⁻¹ through 167 the distribution plate below the bed. The primary air velocity was approximately six times the 168 minimum fluidization velocity which translates to about 0.6 m s⁻¹. A secondary air flow of 30 169 NL min⁻¹ was introduced into the reactor above the fluidized bed into the freeboard providing 170 sufficient oxygen to ensure complete combustion of the generated gases. The reactor was 171 equipped with external heaters for heat up and compensation of heat losses. The 172 temperature inside the reactor is regulated by these heaters as well as by the feedstock 173 input. The flue gas is cleaned by a cyclone removing all particles larger than 10 µm. 174 Afterwards the flue gas is further cleaned with a water scrubber. A more detailed description 175 can be found elsewhere [29]. In total, 540 g of the sieved bed material were added to the 176 fluidized bed. The operating temperature during the combustion experiments were around 177 800 °C and feedstock was continuously fed with a rate around 0.7 kg h⁻¹ for 40 hours or until 178 the bed collapsed due to agglomeration of the bed material. Bed material samples were 179 taken after the experiments and were then further analysed regarding layer formation. 180

181 The bed material sample for the gasification of bark-rich logging residues was taken from the 182 CHP in Senden. The studied K-feldspar particles are "impurities" introduced by the 183 feedstock. The data presented in this work is also described in an earlier work [8].

184 Gasification experiments with bark+chicken manure and chicken manure were conducted in a 100 kW_{th} DFB pilot plant at TU Wien. A detailed description on the specific design of the 185 186 reactor system can be found in literature [30]. For the gasification test campaigns the DFB steam gasifier was first heated up with electrical trace heating and later on additionally by 187 188 combusting softwood pellets until the desired temperatures were reached. At that point steam fluidization was started in the gasification reactor until a steady-state operation was 189 achieved. During this gasification test campaigns several feedstocks were tested. At first, a 190 benchmark operation with softwood pellets was carried out, further described elsewhere [20]. 191 Afterwards the test campaign with bark+chicken manure pellets was started, before ending 192 193 with the chicken manure pellets only. Bed material samples were taken before each fuel 194 change from the lower loop seal.

Table 2 summarizes the experiments covered in this work. It gives an overview of the 195 196 average temperatures observed and the operation time when the samples were taken. For 197 the combustion experiments T_{combustion} describes the temperature in the fluidized bed, while for the gasification experiments T_{combustion} describes the temperatures measured in the 198 combustion reactor and T_{gasification} the temperatures in the gasification reactor. The 199 operational times of the compared experiments differ greatly, as can be seen in Table 2. At 200 this point it is worth mentioning that the combustion experiment with chicken manure did not 201 lead to defluidization but was stopped intentionally due to the accumulating ash inside the 202 system. 203

204Table 2. Average temperatures measured during the operation and duration of operation when the sample205was taken.

			Combustion (5 kW)	Gasification			
		Bark	Bark+	Chicken	Bark-rich	Bark+	Chicken	
			chicken	chicken manure		chicken	manure	
			manure		residues	manure	(100	
					(15 MW) [8]	(100 kW)	kW)	
T _{combustion}	°C	826	795	804	884	996	952	
T _{gasification}	°C	n.a. ^a	n.a. ^a	n.a.ª	856	777	766	
t _{operation}	h	36.5	40	10.8	Constant bed	2.9	1.9	
					replacement			

206 ^a not applicable

207 **2.4. Scanning electron microscopy with energy dispersive** 208 **spectroscopy**

For all analyses, the materials were mounted in epoxy and polished to obtain cross sections 209 of bed particles. Combined scanning electron microscope (SEM) and energy-dispersive X-210 ray spectroscopy (EDS) area mappings and line scans were applied to study the bed 211 materials. Layer morphology in the samples was determined with a Zeiss Evo LS-15 at a 212 voltage of 20 kV and a current of 400 pA in backscattered mode; elemental composition was 213 determined using an Oxford X-MaxN 80 EDS detector. Overview images were captured to 214 identify typical bed particles for elemental analysis. In each sample, around 30 line scans 215 distributed over several particles and approximately five area mappings were obtained. 216

3. Results and Discussion

218

Table 3 depicts SEM images and EDS measurements obtained for the samples of the 219 220 experiments. The SEM images show, that an observable layer formed for all experiments. The EDS measurements show, that during all experiments layers rich in Ca were formed. P 221 was only found in the layers if a P-rich feedstock was used. During the combustion 222 experiments with bark+chicken manure and chicken manure S was non-continuously 223 detected in layers as well. The observed composition of these S-containing areas 224 corresponds to analyses done for ash particles found in the bed, which will be the focus of an 225 upcoming work. 226

Figure 4 shows a close-up of a K-feldspar particle obtained from the combustion of bark+chicken manure and Table 4 shows corresponding EDS images. A clear layer formation can be observed in the micrograph. The cracks in the layer probably stem from the preparation of the sample since no differences in elemental composition along the cracks are observable in the EDS images. The EDS images clearly show that Ca is found further into the particle compared to Mg and phosphorous.

233Table 3. SEM and EDS analysis of K-feldspar particles for the experiments with bark, bark+chicken234manure, and chicken manure in combustion and gasification atmosphere.

	Combustion			Gasification				
	Bark	Bark+chicken	Chicken	Bark	Bark+chicken	Chicken		
0514		manure	manure		manure	manure		
SEM- Imag e		×:	1-6		$\mathbf{\Omega}$			
К		Ked	Ktol	K Kal	Kal	K kal		
Na	Na Kel , 2	Na Ko1,2	Na Kel 2	Na Kol. 2	Na Kol , 2	Na Koti, 2		
Ca		Cafel	G kal	Ca Kal	Ca Kal	Ca Kal		
Mg	Mg Kal, 2	Mg kal.2	Mg Kd , 2	Mg Ka1,2	Mg ka 2	Mg kai, 2		
AI	Al fol	Alfol	Al Kol	Al Kal	Alkal	Al Kal		
Si	S Kel	S Kal	S Kal	Sikal	Skal	S Kal		
P	PEal	Pkal	PRoj	P Ka1	PKd	PKal		
S	Skal	S Kal	S Kal	S Kal	S Kal	5kal		



Figure 4. Close-up of K-feldspar obtained after the combustion with bark+chicken manure.







Figure 5 shows exemplary line scans for all experiments. Line scan a) shows the developed 240 line after the combustion of bark. It can be seen that the concentration of Ca is increasing 241 towards the surface, while K is depleted. This can be seen by the deviation of the inherent K-242 feldspar K/AI ratio of 1 to 0.22 in the layers formed. This substitution of K by Ca is typical for 243 woody biomass ash interacting with K-feldspar [8,31]. Apart from Ca and the elements 244 naturally contained in K-feldspar only Mg is found in a relevant amount. The line scan 245 246 measured for K-feldspar found in the sample for the gasification of bark-rich logging residues is depicted in Figure 5 b). Similarly to the results observed for the combustion of bark, an 247 248 enrichment with Ca was detected while K is depleted. The depletion can again be characterized by a K/AI ratio of 0.62. For this sample no Mg was observed in the layer. 249

Even though K-feldspar was only contained as an "impurity" in the olivine bed used for the gasification of bark-rich logging residues at the CHP in Senden, the same layer formation process took place also when no olivine was present. It is therefore possible to study the layer formation on "impurities" and assume that the same process is occurring for a pure bed.



Figure 5. Linescans measured on K-feldspar. The given distance starts at the outside of the particle and points towards the core. a) Combustion of bark b) Gasification of bark-rich logging residues c) Combustion of bark+chicken manure d) Gasification of bark+chicken manure e) Combustion of chicken manure f) Gasification of chicken manure.

The layer formed during the combustion of bark+chicken manure, depicted in Figure 5 c) is mainly dominated by Ca, P, and Mg. As already observed in Table 4 Ca seems to be found further into K-feldspar compared to Mg and P. The same can be said for the layer formed during the gasification of bark+chicken manure, Figure 5 d). Even though the layer is thinner, Ca is again measured further into the particle compared to P and Mg. Apart from these three

elements no other elements could be found in a relevant amount. A similar observation can 260 261 be made for the layers studied after the combustion and gasification of chicken manure, seen in Figure 5 e) and f), respectively. Ca is again found further into the particle, while P and Mg 262 are enriched in the layer at the same location and no K depletion is occurring. The continued 263 use of the bed material after the gasification of bark+chicken manure does not seem to have 264 265 an influence on the formed layer during the gasification of chicken manure. This can be said, 266 since no two separate layers different in composition were observed in the case for chicken 267 manure, but only one layer which is similar in composition to the combustion of chicken 268 manure. For the experiments with bark+chicken manure and pure chicken manure no 269 depletion of K could be detected.

3.1. Layer formation process proposal

A first proposal for a possible layer formation mechanism will be given in the following section based on the data presented throughout this work. To further support the following proposal experiments focusing on long-term operation will be necessary.

274 The layers formed for bark+chicken manure and pure chicken manure are different to the 275 layers formed with bark and bark-rich logging residue but similar to each other. For those experiments, the diffusion of K out of the K-feldspar cannot be detected. This is due to the 276 fact that the high levels of phosphorous for bark+chicken manure and chicken manure shift 277 the reactions into the ash phase to the formation of Ca-rich phosphates. This effect is already 278 observable for an admixture of chicken manure of 0.3 dry mass fraction as studied here. That 279 is due to the fact that chicken manure has a comparably high ash content, see Table 1 and 280 Figure 3, so small admixtures already highly influence the ash chemistry. The often 281 282 overlooked high Ca content of chicken manure is additionally influencing the ash chemistry. 283 This high Ca content is promoting the formation of Ca-rich layers, which are known to be catalytically active for gasification reactions [10], also when phosphorous is present in the 284 285 layers [17].

286 All line scans with bark show that Ca is penetrating further into the particle than P. This is 287 likely due to the formation of an inner and an outer layer. If the ratio of P to Ca is further 288 increased it was previously speculated that the inner layer might be completely inhibited. This is explained in the following. The inner layer is formed by the diffusion of Ca into the 289 particle, while the outer layer is formed by adhesion of ash, resulting in high shares of Ca 290 and P, which form the majority of chicken manure ash. Grimm et al. [2] have observed an 291 292 inhibition of inner layer formation when using P-rich sewage sludge as feedstock and quartz particles as bed material in fluidized bed combustion experiments. The inhibition of the inner 293 layer was explained by phosphate formation within the ash, which further leads to less 294 reactivity of the ash components with the bed particle itself. 295

Figure 6 shows a simple scheme of inner and outer layer formation. Inner layer formation is characterized by a chemical reaction-based interaction between feedstock ash components and the bed particle surface. This interaction can be e.g. alkali-silicate formation, as observed for quartz where K reacts with silicon to form K-silicates [32]. Furthermore, inner layer formation can be based on a substitution reaction, as observed for olivine where Ca^{2+} ions substitute Fe^{2+} and Mg^{2+} ions in the crystal structure of olivine. Therefore, inner layers typically grow inwards into the bed particles [33].

303 Outer layers, on the other hand, are formed through accumulation of ash components on the 304 particle surface and pile up outwards. Woody feedstock typically shows both inner and outer layer formation (Figure 6, a)), whereas P-rich residual feedstock shows a stronger tendencytowards solely outer layer formation (Figure 6, b)).



Figure 6. Simple scheme of layer formation mechanisms; a) Chemical reaction-based layer formation with woody-based feedstock, b) Ash accumulation-based layer formation with P-rich feedstock.

307 Frequently proposed mechanisms for layer formation in the literature [32,33] typically refer to

inner layer formation since outer layers are merely an accumulation of ash components and therefore highly dependent on the feedstock ash content itself.

Inner layer formation has been observed to be an important factor in agglomeration in 310 fluidized beds, as coating- or layer-induced agglomeration is a major issue when quartz 311 particles are used as bed material [34-36]. Since outer layers are typically dominant in Ca 312 the agglomeration tendency decreases once an outer layer - acting as a shell around the 313 314 particle and, if applicable, the inner layer - has been formed. Furthermore, Ca from the outer layer can diffuse to and react with the inner e.g. K-rich layer forming a more Ca-rich inner 315 316 layer with higher melting temperature. Thus, layer formation is of high relevance when it comes to investigation on agglomeration processes. 317

318 **4.** Conclusion

The presented results show that layer formation on K-feldspar is mainly dependent on the 319 used feedstock and findings for BFB combustion and DFB gasification were similar to each 320 other. When feedstocks rich in P are being used, an enrichment of P in the layer could be 321 observed. Due to this it is possible to adapt the observations regarding layer formation 322 collected for combustion to gasification applications. It was furthermore speculated that an 323 increased P content hinders the formation of inner layers by promoting the formation of 324 phosphates in the ash fraction. The formed phosphates then stick to the K-feldspar particles 325 to form an ash-rich layer. This ash-rich layer forms independent of the atmosphere, i.e. 326 327 combustion or gasification.

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340 **References**

- W. Steffen, K. Richardson, J. Rockström, S.E. Cornell, I. Fetzer, E.M. Bennett, R. Biggs, S.R. Carpenter, W. de Vries, C.A. de Wit, C. Folke, D. Gerten, J. Heinke, G.M. Mace, L.M. Persson, V. Ramanathan, B. Reyers, S. Sörlin, Planetary boundaries: Guiding human development on a changing planet, Science. 347 (2015) 1259855. doi:10.1126/science.1259855.
- A. Grimm, N. Skoglund, D. Boström, M. Öhman, Bed Agglomeration Characteristics in Fluidized Quartz Bed Combustion of Phosphorus-Rich Biomass Fuels, Energy Fuels.
 25 (2011) 937–947. doi:10.1021/ef101451e.
- J.C. Schmid, U. Wolfesberger, S. Koppatz, C. Pfeifer, H. Hofbauer, Variation of [3] 349 feedstock in a dual fluidized bed steam gasifier-influence on product gas, tar content, 350 composition, Environ. Prog. Sustain. Energy. 31 351 and (2012) 205–215. doi:10.1002/ep.11607. 352
- 353[4]J. Karl, T. Pröll, Steam gasification of biomass in dual fluidized bed gasifiers: A review,354Renew. Sustain. Energy Rev. 98 (2018) 64–78. doi:10.1016/j.rser.2018.09.010.
- [5] D. Boström, N. Skoglund, A. Grimm, C. Boman, M. Öhman, M. Broström, R. Backman,
 Ash Transformation Chemistry during Combustion of Biomass, Energy Fuels. 26 (2012)
 85–93. doi:10.1021/ef201205b.
- [6] H. He, D. Boström, M. Öhman, Time Dependence of Bed Particle Layer Formation in
 Fluidized Quartz Bed Combustion of Wood-Derived Fuels, Energy Fuels. 28 (2014)
 360 3841–3848. doi:10.1021/ef500386k.
- [7] F. Kirnbauer, H. Hofbauer, Investigations on Bed Material Changes in a Dual Fluidized
 Bed Steam Gasification Plant in Güssing, Austria, Energy Fuels. 25 (2011) 3793–3798.
 doi:10.1021/ef200746c.
- [8] M. Kuba, H. He, F. Kirnbauer, N. Skoglund, D. Boström, M. Öhman, H. Hofbauer, Thermal Stability of Bed Particle Layers on Naturally Occurring Minerals from Dual Fluid Bed Gasification of Woody Biomass, Energy Fuels. 30 (2016) 8277–8285. doi:10.1021/acs.energyfuels.6b01523.
- F. Kirnbauer, V. Wilk, H. Kitzler, S. Kern, H. Hofbauer, The positive effects of bed
 material coating on tar reduction in a dual fluidized bed gasifier, Fuel. 95 (2012) 553–
 562. doi:10.1016/j.fuel.2011.10.066.
- 371[10]M. Kuba, F. Havlik, F. Kirnbauer, H. Hofbauer, Influence of bed material coatings on the
water-gas-shift reaction and steam reforming of toluene as tar model compound of
biomass gasification, Biomass Bioenergy. 89 (2016) 40–49.
doi:10.1016/j.biombioe.2015.11.029.
- [11] J. Kryca, J. Priščák, J. Łojewska, M. Kuba, H. Hofbauer, Apparent kinetics of the water gas-shift reaction in biomass gasification using ash-layered olivine as catalyst, Chem.
 Eng. J. 346 (2018) 113–119. doi:10.1016/j.cej.2018.04.032.
- T. Berdugo Vilches, M.C. Seemann, H. Thunman, Influence of in-bed catalysis by ash coated olivine on tar formation in steam gasification of biomass, Energy Fuels. (2018).
 doi:10.1021/acs.energyfuels.8b02153.
- [13] M. Kuba, S. Kraft, F. Kirnbauer, F. Maierhans, H. Hofbauer, Influence of controlled handling of solid inorganic materials and design changes on the product gas quality in dual fluid bed gasification of woody biomass, Appl. Energy. 210 (2018) 230–240.
 (2018) 384 doi:10.1016/j.apenergy.2017.11.028.
- [14] H. Thunman, M. Seemann, T.B. Vilches, J. Maric, D. Pallares, H. Ström, G. Berndes, P.
 Knutsson, A. Larsson, C. Breitholtz, O. Santos, Advanced biofuel production via
 gasification lessons learned from 200 man-years of research activity with Chalmers'
 research gasifier and the GoBiGas demonstration plant, Energy Sci. Eng. 6 (2018) 6–
 34. doi:10.1002/ese3.188.
- [15] M. Öhman, L. Pommer, A. Nordin, Bed Agglomeration Characteristics and Mechanisms
 during Gasification and Combustion of Biomass Fuels, Energy Fuels. 19 (2005) 1742–
 1748. doi:10.1021/ef040093w.

- [16] Z. He, D.J. Lane, W.L. Saw, P.J. van Eyk, G.J. Nathan, P.J. Ashman, Ash–Bed Material
 Interaction during the Combustion and Steam Gasification of Australian Agricultural
 Residues, Energy Fuels. 32 (2018) 4278–4290. doi:10.1021/acs.energyfuels.7b03129.
- [17] K. Wagner, A.M. Mauerhofer, M. Kuba, H. Hofbauer, Suitability of K-feldspar as
 Alternative Bed Material in Dual Fluidized Bed Steam Gasification in Combination with
 Ash-Rich Feedstocks, in: 23rd Int. Conf. FBC, Seoul, Korea, 2018: pp. 967–976.
- [18] N. Berguerand, T. Berdugo Vilches, Alkali-Feldspar as a Catalyst for Biomass
 Gasification in a 2-MW Indirect Gasifier, Energy Fuels. 31 (2017) 1583–1592.
 doi:10.1021/acs.energyfuels.6b02312.
- [19] N. Berguerand, J. Marinkovic, T. Berdugo Vilches, H. Thunman, Use of alkali-feldspar
 as bed material for upgrading a biomass-derived producer gas from a gasifier, Chem.
 Eng. J. 295 (2016) 80–91. doi:10.1016/j.cej.2016.02.060.
- [20] A.M. Mauerhofer, F. Benedikt, J.C. Schmid, J. Fuchs, S. Müller, H. Hofbauer, Influence
 of different bed material mixtures on dual fluidized bed steam gasification, Energy. 157
 (2018) 957–968. doi:10.1016/j.energy.2018.05.158.
- [21] A. Magdalena Mauerhofer, F. Benedikt, J. Christian Schmid, H. Hofbauer, Mixtures of Silica Sand and Calcite as Bed Material for Dual Fluidized Bed Steam Gasification, in: Proc. SEEP2017, University of Maribor Press, 2017: pp. 253–266. doi:10.18690/978-961-286-048-6.26.
- [22] C. Pfeifer, S. Koppatz, H. Hofbauer, Catalysts for dual fluidised bed biomass
 gasification—an experimental study at the pilot plant scale, Biomass Convers.
 Biorefinery. 1 (2011) 63–74. doi:10.1007/s13399-011-0005-3.
- [23] C. Pfeifer, S. Koppatz, H. Hofbauer, Steam gasification of various feedstocks at a dual
 fluidised bed gasifier: Impacts of operation conditions and bed materials, Biomass
 Convers. Biorefinery. 1 (2011) 39–53. doi:10.1007/s13399-011-0007-1.
- [24] T. Berdugo Vilches, J. Marinkovic, M. Seemann, H. Thunman, Comparing Active Bed
 Materials in a Dual Fluidized Bed Biomass Gasifier: Olivine, Bauxite, Quartz-Sand, and
 Ilmenite, Energy Fuels. 30 (2016) 4848–4857. doi:10.1021/acs.energyfuels.6b00327.
- [25] J. Marinkovic, M. Seemann, G.L. Schwebel, H. Thunman, Impact of Biomass Ash–
 Bauxite Bed Interactions on an Indirect Biomass Gasifier, Energy Fuels. 30 (2016)
 4044–4052. doi:10.1021/acs.energyfuels.6b00157.
- [26] S. Anis, Z.A. Zainal, Tar reduction in biomass producer gas via mechanical, catalytic
 and thermal methods: A review, Renew. Sustain. Energy Rev. 15 (2011) 2355–2377.
 doi:10.1016/j.rser.2011.02.018.
- [27] M. Kuba, F. Kirnbauer, H. Hofbauer, Influence of coated olivine on the conversion of intermediate products from decomposition of biomass tars during gasification, Biomass Convers. Biorefinery. 7 (2017) 11–21. doi:10.1007/s13399-016-0204-z.
- [28] N. Skoglund, Ash chemistry and fuel design focusing on combustion of phosphorus-rich
 biomass, Doctoral Thesis, Department of applied physics and electronics, Umeå
 universitet, 2014.
- [29] M. Öhman, A. Nordin, A New Method for Quantification of Fluidized Bed Agglomeration
 Tendencies: A Sensitivity Analysis, Energy Fuels. 12 (1998) 90–94.
 doi:10.1021/ef970049z.
- [30] J.C. Schmid, Development of a novel dual fluidized bed gasification system for
 increased fuel flexibility, PhD Thesis, Doctoral thesis, Institute of Chemical Engineering,
 Vienna University of Technology, 2014.
- [31] H. He, N. Skoglund, M. Öhman, Time-Dependent Layer Formation on K-Feldspar Bed
 Particles during Fluidized Bed Combustion of Woody Fuels, Energy Fuels. 31 (2017)
 12848–12856. doi:10.1021/acs.energyfuels.7b02386.
- [32] H. He, X. Ji, D. Boström, R. Backman, M. Öhman, Mechanism of Quartz Bed Particle
 Layer Formation in Fluidized Bed Combustion of Wood-Derived Fuels, Energy Fuels. 30
 (2016) 2227–2232. doi:10.1021/acs.energyfuels.5b02891.
- [33] M. Kuba, H. He, F. Kirnbauer, N. Skoglund, D. Boström, M. Öhman, H. Hofbauer, 445 Mechanism of Layer Formation on Olivine Bed Particles in Industrial-Scale Dual Fluid 446 447 Bed Gasification of Wood, Energy Fuels. 30 (2016) 7410–7418. doi:10.1021/acs.energyfuels.6b01522. 448

- [34] H.J.M. Visser, S.C. van Lith, J.H.A. Kiel, Biomass Ash-Bed Material Interactions
 Leading to Agglomeration in FBC, J. Energy Resour. Technol. 130 (2008) 011801.
 doi:10.1115/1.2824247.
- [35] M. Öhman, A. Nordin, B.-J. Skrifvars, R. Backman, M. Hupa, Bed Agglomeration
 Characteristics during Fluidized Bed Combustion of Biomass Fuels, Energy Fuels. 14
 (2000) 169–178. doi:10.1021/ef990107b.
- [36] F. Scala, Particle agglomeration during fluidized bed combustion: Mechanisms, early
 detection and possible countermeasures, Fuel Process. Technol. 171 (2018) 31–38.
 doi:10.1016/j.fuproc.2017.11.001.

458 **Supplementary**

459 Table A.1. Fuel fingerprint data; concentrations given in mol kg⁻¹.

	K	Na	Ca	Mg	Fe	Al	Si	Р	S	CI
Bark	0.10	0.17	0.51	0.25	0.11	0.23	0.89	0.06	0.04	0.02
Bark- rich logging residues	0.06	0.01	0.23	0.03	0.00	0.01	0.05	0.02	0.01	0.00
Bark+ chicken manure	0.24	0.23	1.11	0.45	0.10	0.22	0.81	0.60	0.13	0.12
Chicken manure	0.60	0.60	1.99	1.10	0.04	0.10	0.40	1.92	0.41	0.49